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ELECTRICAL PROPERTIES OF ANNEALED AND COATED BORON NITRIDE UNDER ELECTRON BEAM IRRADIATION

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ABSTRACT

The charging and relaxation kinetics of pyrolytic boron nitride (BN) substrates, BN with an aluminium oxide (BN/Al₂O₃) coating, and thermally-annealed alumina-coated boron nitride (an-BN/Al₂O₃) were investigated under low power electron irradiation $(5 < E_0 < 20 \text{ keV}, J_i = 10 \text{ nA.cm}^{-2} \text{ at room temperature})$ in the CEDRE facility at ONERA (Toulouse, France). Surface potentials of each ceramics configuration were measured over time using the Kelvin probe method. The influence of coating and annealing treatments to limit charging is discussed in this paper. A thorough study of a an-BN/Al₂O₃ sample was carried out under a critical electron flux ($E_0 = 20 \text{ keV}$, $J_i = 750 \text{ nA.cm}^{-2}$) in order to assess the degradation kinetics of the material's electrical properties. The characterisations of an-BN/Al₂O₃ samples were performed before and after electrical aging at CIRIMAT (Toulouse, France) to identify the structural and chemical evolution which would explain this degradation. A chemical deterioration of coating and some contaminants were evidenced after the critical irradiation.

Keywords: Electron irradiation, electrical conductivity, secondary emission, charging, aging, annealing, coating, ceramics

1. INTRODUCTION

Many technical ceramics have been developed in recent decades for use in satellites due to their remarkable electrical. mechanical and thermal properties. Boron nitride (BN), is one such high valueadded ceramic. It is a synthetic dielectric ceramics [1] [2] of group III-Nitride [3]. BN and especially the pyrolytic BN (pBN) [3] is used in spacecraft applications or in electron devices [4] because of its high anisotropic thermal conductivity and electrical insulating nature. This insulator is often subjected to extreme conditions due to the plasma environment intrinsic to electronic applications. In fact, when pBN substrates are irradiated by electrons with high incident energies < 20 keV, that can lead to trapping of many charged particles in the ceramic's bulk [5] [6]. Consequently, charging and discharging phenomena can occur after prolonged exposure which can deteriorate the efficiency of electronic applications.

Thus, an experimental study of the influence of an alumina coating and thermal annealing (under vacuum) on the charging and relaxation kinetics of these different systems was carried out. The purpose of this work was to assess the efficiency of these surface and thermal treatments to limit charging and the surface potential of these industrial ceramics with pBN substrates under electron irradiation.

A parametric study on charging and relaxation kinetics of BN, BN/Al₂O₃ and an-BN/Al₂O₃ samples under electron irradiation was performed. The energy and flux of incident particles have been adjusted in this parametric study. Observed differences in electrical behaviour under electron beam are emphasised. The intrinsic (or dark) conductivities of these materials were determined using an experimental method [7], the Constant Voltage Conductivity (CVC) methods. Due to the very low absolute equilibrium surface potential of an-BN/Al₂O₃ compared to that of BN and BN/Al₂O₃ when they were irradiated using the same experimental conditions, a thorough study of accelerated aging was also carried out. The different charging kinetics under critical irradiation as a function of time, as well as the chemical evolution of this sample, are described in the last part of this paper.

2. EXPERIMENTATION

2.1. CEDRE facility and method

The versatile irradiation test chamber CEDRE at ONERA (Toulouse, France) (see Fig. 1) can be easily adjusted to characterize the surface potential (V_s) of dielectrics under electron beam irradiation representative of diverse space conditions [9]. The experimental method usually applied in CEDRE to study the charges transport in dielectrics is to implant incident electrons with calibrated flux and energy in order to measure the surface potential built up on the sample with a Kelvin Probe [10] (KP - Monroe Electronics Inc., Model 175, ±20 kV). Charge is implanted with a mono-energetic beam electron gun (Kimball, Model EGPS-4212B), which provides reproducible irradiation conditions spread ≈ 0.5 eV and energy stability of ± 0.01 % during one hour) over an energy range of 1 keV to 20 keV. Typically, a continuous beam was used, with flux ranging from 0.05 nA.cm $^{-2}$ to 100 $\mu A.cm^{-2}$. The continuous beam is focused ($\varphi < 3$ mm) or defocused (3 mm $< \varphi < 50$ mm) in order to study the different conduction mechanisms (intrinsic or surface radiation induced conductivity). The distance between samples surface and the KP is $\sim\!\!3$ mm to obtain the desired spatial resolution and to limit measurement uncertainty.

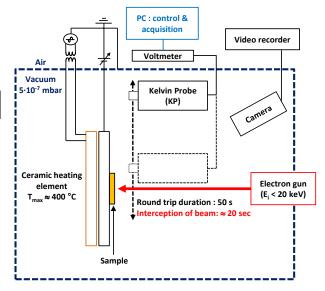


Fig. 1. Schematic of CEDRE instrumentation and the Kelvin probe translation during surface potential measurements

Data processing, instrumentation and the Kelvin probe are computer controlled, using GPIB interfacing and a DAQ card under LabVIEWTM control. A chamber vacuum level of ~5.10⁻⁷ mbar was achieved using a dry pump group to minimize contamination. A floating or grounded sample holder assembly developed at ONERA uses a ceramic heating element to sustain controlled temperatures between 20 °C and 400 °C to assess the temperature dependence of conductivity; it also allows outgassing of samples before the irradiation tests and has been used to discharge the samples after the irradiation test. The sample holder assembly is installed on one of four faces of a rotating cube. A Faraday cup installed on another cube face can quickly measure the electron flux before tests. A CCD camera is used to calibrate flux and visually check other phenomena during the tests.

2.2. CVC Chamber and method

Constant voltage conductivity tests were made in the CVC chamber of Materials Physics Group at Utah State University. The CVC chamber and instrumental have been meticulously described in [11], [12] and [13]. The <u>Fig. 2</u> shows the principle of this method using electrode charge injection in a parallel-plate geometry [14].

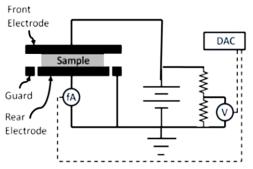


Fig. 2. Schematic representation of the CVC chamber experimental method [13]

The dark conductivity was determined with the CVC method using

$$\sigma^{CVC}(t) = \frac{I(t) \times d}{S \times V},$$
 (1)

where I is the measured current at equilibrium [A], d is the sample thickness [m], S the sample surface in contact with the measurement electrode [m²] and V is the applied voltage [V].

2.3. Samples

The dimensions (L x 1 x d) of BN, BN/Al $_2$ O $_3$ and an–BN/Al $_2$ O $_3$ samples characterised in CEDRE and the CVC chamber were 50 x 3 x 3 mm and ~10 x \lesssim 1 x \lesssim 1 mm, respectively. Commercial BN was coated with alumina (300 nm thickness) using an industrial PVD-RF method. The industrial annealing treatment was carried out under vacuum.

3. RESULTS AND DISCUSSION

3.1. Charges transport in BN, BN/Al $_2O_3$ and an-BN/Al $_2O_3$

The surface potentials of BN, BN/Al $_2$ O $_3$ and an–BN/Al $_2$ O $_3$ were measured under electron irradiation subject to the same experimental conditions (10 nA.cm $^{-2}$, T $^{\circ}$ C $_{room}$, defocused beam). Ten minutes after the irradiation beginning, a stable equilibrium surface potential (V_s eq) was reached for these samples. Fig. 3 represents the evolution of V_s eq as a function of the incident energy (E_0 = 5, 8 and 11 keV).

At low incident energy ($E_0 = 5 \text{ keV}$), $V_s^{\ \ eq}$ for BN is about 5 times greater than for both BN/Al₂O₃ and an–BN/Al₂O₃. When the beam energy (E_0) increases, a significant non-linear increase of the equilibrium surface potential of BN and BN/Al₂O₃ is observed unlike for an–BN/Al₂O₃. The charging of BN/Al₂O₃ and an–BN/Al₂O₃ is governed and limited by the secondary electron emission mechanism at low non-penetrating energies. In fact, the electron penetration depth is less than the coating thickness (300 nm) at low energies, $E_0 \le 6.4 \text{ keV}$ (determined through the Casino software based on Monte-Carlo model [15]).

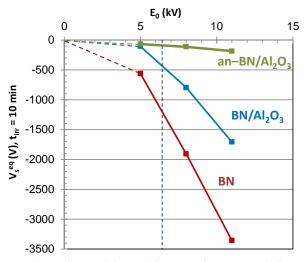


Fig. 3. Evolution of the equilibrium surface potential of BN, BN/Al_2O_3 and $an-BN/Al_2O_3$, as a function of the incident energy, after 10 min under electron irradiation (10 nA.cm⁻², $T^{\circ C}_{room}$ defocused beam)

Consequently, even if the alumina coating is heterogeneous due to the high roughness of the boron nitride substrate, the great majority of incident charges are implanted in the Al_2O_3 coating which has a higher secondary electron yield [16] than BN [4] [17]. When the incident energy increases ($E_0 \geq 6.4$ keV), the electron range increasingly moves into the BN substrate. Thus, the equilibrium surface potential is expected to abruptly increase when $E_0 > 8$ keV. However, the observed increase of $V_s^{\text{éq}}$ for an–BN/Al₂O₃ is very low even beyond 8 keV. This would be expected if the annealing treatment (under vacuum) increases the total conductivity relative to that of BN/Al₂O₃.

In an effort to assess their ability to empty trapped charges, the relative relaxation kinetics of each sample has been measured. The normalised surface potential at ten minutes after the irradiation ceases, $V_{s(10 \, min)}^{norm} = (V_{s(10)}/V_{s(0)})$, or equivalently the fraction of retained charge after 10 min relaxation, $(Q_{s(10)}/Q_{s(0)})$, is shown in Fig. 4 for BN, BN/Al₂O₃ and an-BN/Al₂O₃ as a function of the incident energy E₀ used during the irradiation phase. Very few charge carriers have been detrapped and evacuated from the surface or the bulk of untreated BN substrate after 10 min relaxation, irrespective of the incident energy. The coated BN samples both had higher relaxation rates. For a non-penetrating beam at 5 keV, the surface potential of BN decreased by ~3% after 10 min relaxation, BN/Al_2O_3 by ~22 %, and an– BN/Al_2O_3 by ~84%. The relaxation rates for all samples decrease as incident energy used during the irradiation phase increases (i.e., the relaxation rates are roughly inversely proportional to penetration depth). At 5 keV all incident electrons of the coated samples are implanted in the alumina, which has an intrinsic conductivity higher than that of BN substrate.

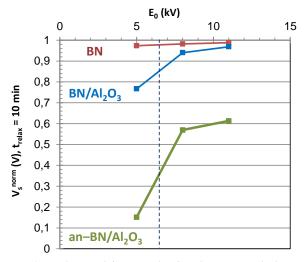


Fig. 4. Evolution of the normalised surface potential of BN, BN/Al₂O₃ and an–BN/Al₂O₃, as a function of the incident energy, during relaxation after 10 min without electron irradiation (10 nA.cm⁻², T^{°C}_{room}, defocused beam)

Even though the surface potential of an–BN/Al $_2$ O $_3$ was much lower than the other materials upon discontinuation of irradiation at $E_0 \geq 8$ keV (see **Fig. 3**), a significant decrease of its surface potential was measured (at least ~ 40 %) after ten minutes of relaxation. Consequently, the annealing thermal treatment under vacuum improves the charges transport in BN substrate and especially in the alumina coating. Annealing under vacuum (reducing atmosphere) relaxes the residual structural constraints in the sample; this is likely to increase the concentration of point defects such as oxygen vacancies and impurities, which favour charge conduction and recombination processes [6].

The total intrinsic conductivity of BN, BN/Al₂O₃ an-BN/Al₂O₃ was determined in order to emphasise the electrical behaviour as a function of the elaboration treatment (see **Table 1**). The values determined in the CVC chamber average < 50%. BN and BN/Al₂O₃ show similar total conductivities (surface, interfaces and bulk). Alternately, an-BN/Al₂O₃ has about 25 to 30 times higher total conductivity than BN and BN/Al₂O₃. These quantitative conductivity results are consistent with the lower charging level (Fig. 3) and faster relaxation rate (Fig. 4) of this annealed coated sample at all incident energies. Further, the significantly higher secondary electron emission yield (δ_{SEE}) of crystalline alumina [16] [18] compared with that of BN [17] can also explain the observed low level of equilibrium surface potential for an-BN/Al₂O₃ compared to BN. Nonetheless, the δ_{SEE} as well as the σ of an–BN/Al₂O₃ are too low to explain its small equilibrium surface potential and especially under high incident energy. Another surface electrical phenomenon such as partial discharges unmeasurable through the Kelvin probe could explain this charging regulation of this heterogeneous rough sample irradiated under high energy and flux.

Table 1. Intrinsic conductivity (S.m⁻¹) value of each samples determined in the CVC chamber

BN	BN/Al ₂ O ₃	an-BN/Al ₂ O ₃	an-BN/Al ₂ O ₃ (aged)
$(0,5\pm0,1).10^{-15}$	$(0,2\pm0,1).10^{-15}$	$(8 \pm 1).10^{-15}$	< (2 ± 3).10 ⁻¹⁵

3.2. Electrical aging of an-BN/Al₂O₃

An accelerated aging test of an–BN/Al₂O₃ was performed to determinate if its conductivity and electron yield evolve as a function of dose. The temporal evolution of the surface potential of an–BN/Al₂O₃ irradiated under high electron flux (750 nA.cm⁻²) and high energy (20 keV) is shown in **Fig. 5**.

Three main charging regimes are conspicuous in **Fig. 5.** First is a temporary equilibrium regime. A low near-equilibrium surface potential is measured at short irradiation times (t < 50 min); this behaviour was corroborated with measurements at lower incident electron energies and flux. Second is a transient regime, from ~50 min to $t_c \approx 134$ min. The charging rate of this material slowly increases (slope $\propto 1/\alpha$) up to a critical time $t_c \approx 134$ min. Last is a critical regime; a consistent high charging rate is observed beyond t_c . A critical surface potential equals to -2800 V is suddenly reached 2 hr after the critical time ($\Delta V = -2400$ V) whereas a small increase of -400 V was observed after the first two hours (between 0 and ~ t_c).

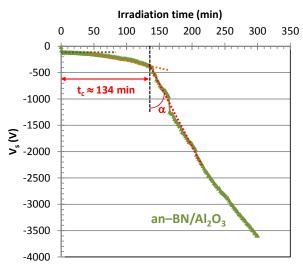


Fig. 5. Temporal evolution of the surface potential of an–BN/Al₂O₃ under critical irradiation (20 keV, 750 nA.cm⁻², T^{C}_{room} , focused beam)

This electrical aging behaviour can be explained by a progressive degradation of the coated boron nitride surface. The critical dose (D_c [J.kg⁻¹ \equiv Gy]) at the onset of degradation which corresponds to the abrupt decrease of α at t_c , that is

$$D_{c(x)} = \frac{J_i}{q_e} \times \frac{t_c}{\rho_m} \times \frac{E_i}{R(E_i)}$$
 (2)

where q_e is the electron charge [C], ρ_m is the mass density of Al_2O_3 or BN [kg.cm 3] and $R(E_i)$ the is energy-dependent penetration depth [m] into the material. The critical doses injected into the alumina coating and in the BN substrate during the aging test were ~ 7,4.10 7 Gy and ~ 1,3.10 8 Gy, respectively.

Chemical characterisation of the irradiated surface of an-BN/Al₂O₃ was done with RAMAN and XPS methods. Chemical degradation of the Al₂O₃ coating due to irradiation was evidenced by an observed decrease of impurities (Cr3+) and chemical bonds of compounds Al(2p) and O(1s). O vacancies, which are known to be produced in a reducing (vacuum) environment [21] and by electron irradiation [22], have been associated with luminescence attributed to one electron (F⁺ emission) or two electron (F emission) trapping process [21]. Increased trapping can lead to decreased conductivity and increased equilibrium surface voltage. As corroborating evidence, another sample of an-BN/Al₂O₃ aged in somewhat different conditions (5 keV and 500 nA.cm⁻², for 24 hr) was characterised in the CVC chamber. The results showed at least a four-fold decrease of intrinsic conductivity but the standard deviation of this measurement is high (see Table 1).

Chemical characterisation also showed an increase of contaminant concentration (especially C) at the irradiated area. High oxygen vacancy concentration has been noted in C-doped Al_2O_3 materials [22]. Prolonged exposure to electron beams has been shown to form graphitic C contamination layers, which reduced the electron emission from technical Al/Al_2O_3 surfaces since the secondary electron yield of graphitic C is very low [20]. Reduced electron emission of such contaminated materials will reduce negative surface charging at incident energies above the second crossover energy (~ 500 eV to 1000 eV for graphitic C). This study suggested that both the total conductivity and secondary electron emission [19] [20] of this sample decreased over irradiation time and dose.

4. CONCLUSION

In summary, the parametric study of charge transport in BN, BN/Al₂O₃ and an–BN/Al₂O₃ described herein has shown that the alumina coating and especially the annealing thermal treatment under vacuum result in a reduced surface potential of the BN substrate. Despite a heterogeneous alumina coating on the rough substrate, the secondary electron yield is higher. The intrinsic conductivity is higher for an–BN/Al₂O₃ sample, compared to BN and BN/Al₂O₃. It is suggested that the annealing treatment probably generated higher density of physical and chemical defects—especially near the surface—which resulted in increased total conductivity of an–BN/Al₂O₃. Nonetheless, another physical mechanism such as surface partial discharges seems to regulate the surface

potential of an–BN/ Al_2O_3 sample. Indeed, its surface potential is very low whatever the used high energies and flux of incident electrons. However this fast phenomenon could not be measured with the KP method (but has been brought into evidence in another study).

An important electrical aging test of an–BN/Al $_2O_3$ was performed. The intrinsic conductivity of this an–BN/Al $_2O_3$ has decreased with dose. Chemical degradation of the alumina coating, as well as increased contaminant (notably C) concentrations were observed. The carbon contamination causes a decrease of secondary electron emission of the heterogeneous surface composed of alumina and boron nitride. The charging rate of an–BN/Al $_2O_3$ slowly increased over an initial exposure time during the accelerated aging test, and suddenly increased at a characteristic critical dose which seems to depend on the incident flux. More experiments should be carried out in order to assess the influence of incident current on this critical dose and the incident electron energy on α .

In conclusion, several steps of the elaboration process, such as coating and annealing treatment, can be applied to limit the charging of an insulator used on satellites. However, these treatments and the elaboration parameters have to be optimised in order to increase the life time of these technical ceramics irradiated in critical conditions.

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