

Utah State University

DigitalCommons@USU

Reports

Utah Water Research Laboratory

January 1970

A Hydrologic Model of the Bear River Basin

Robert W. Hill

Eugene K. Israelsen

A. Leon Huber

J. Paul Riley

Follow this and additional works at: https://digitalcommons.usu.edu/water_rep



Part of the [Civil and Environmental Engineering Commons](#), and the [Water Resource Management Commons](#)

Recommended Citation

Hill, Robert W.; Israelsen, Eugene K.; Huber, A. Leon; and Riley, J. Paul, "A Hydrologic Model of the Bear River Basin" (1970). *Reports*. Paper 416.

https://digitalcommons.usu.edu/water_rep/416

This Report is brought to you for free and open access by the Utah Water Research Laboratory at DigitalCommons@USU. It has been accepted for inclusion in Reports by an authorized administrator of DigitalCommons@USU. For more information, please contact digitalcommons@usu.edu.



Utah State University

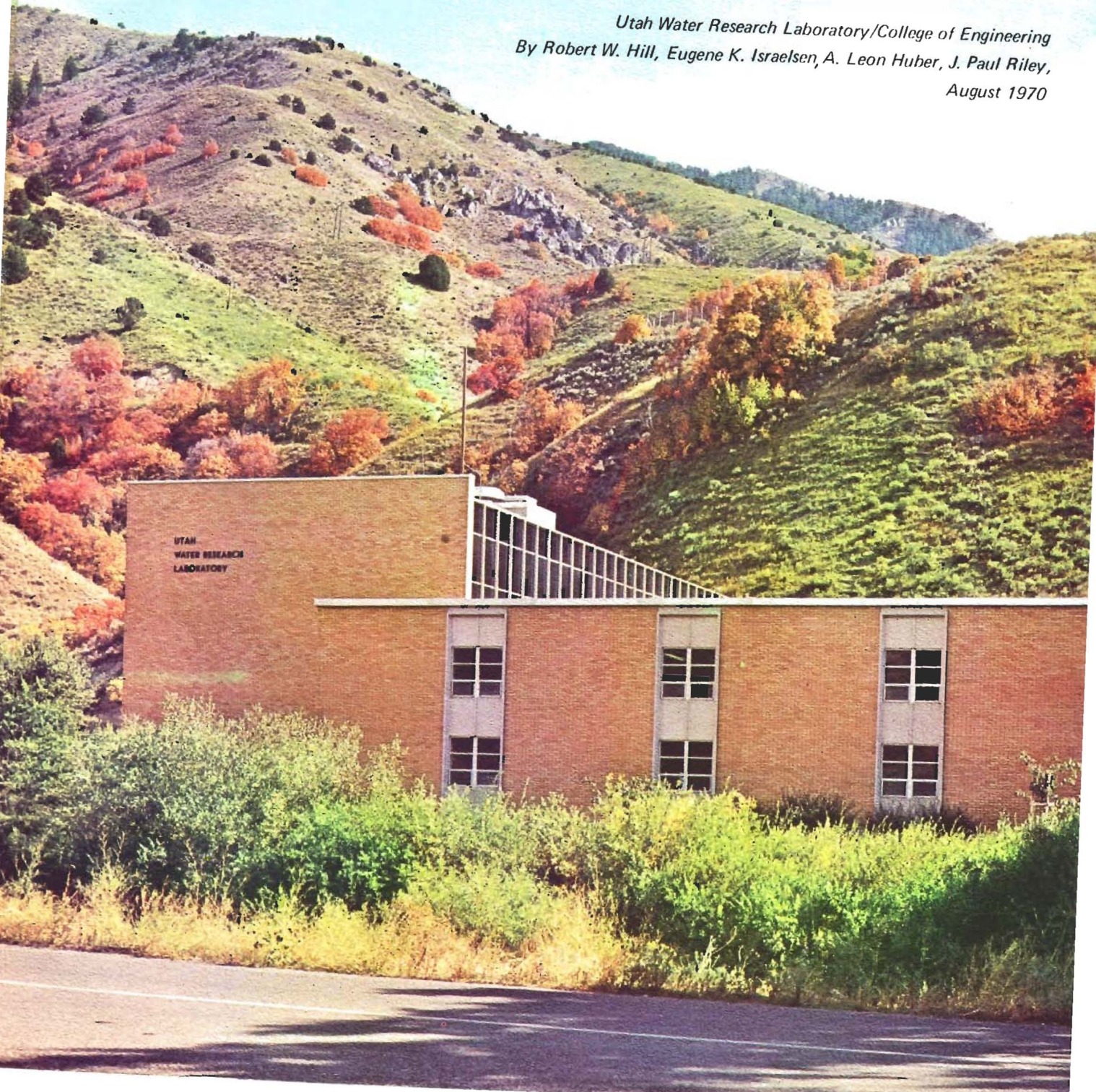
PRWG72-1



Logan, Utah 84321

A Hydrologic Model of the Bear River Basin

*Utah Water Research Laboratory/College of Engineering
By Robert W. Hill, Eugene K. Israelsen, A. Leon Huber, J. Paul Riley,
August 1970*



A HYDROLOGIC MODEL OF THE BEAR RIVER BASIN

by

Robert W. Hill
Eugene K. Israelsen
A. Leon Huber
J. Paul Riley

The work reported by this project completion report was supported
in part with funds provided by the Department of the Interior,
Office of Water Resources Research under P. L. 88-379,
Project Number-B-028-Utah, Agreement Number-
14-01-0001-1955, Investigation Period-July 1,
1968 to June 30, 1970

Utah Water Research Laboratory
College of Engineering
Utah State University
Logan, Utah

August 1970

PRWG72-1

•

•

•

•

•

•

ABSTRACT

A HYDROLOGIC MODEL OF THE BEAR RIVER BASIN

As demands upon available water supplies increase, there is an accompanying increase in the need to assess the downstream consequences resulting from changes at specific locations within a hydrologic system. The problem is approached in this study by hybrid computer simulation of the hydrologic system. Modeling concepts are based upon the development of basic relationships which describe the various hydrologic processes. Within a system these relationships are linked by the continuity-of-mass principle which requires a hydrologic balance at all points. Spatial resolution is achieved by considering the modeled area as a series of subbasins. The time increment adopted for the model is one month, so that time varying quantities are expressed in terms of mean monthly values. The model is general in nature and is applied to a particular hydrologic system through a programmed verification procedure whereby model coefficients are evaluated for the particular system.

In this study the model was synthesized on a hybrid computer and applied to the Bear River basin of western Wyoming, southern Idaho, and northern Utah. Comparisons between observed and computed outflow hydrographs for each subbasin are shown. The utility of the model for predicting the effects of various possible water resource management alternatives is demonstrated for the number 1, or Evanston subbasin. The hybrid computer is very efficient for model development, and the verified model can be readily programmed on the all-digital computer.

Hill, Robert W. ; Israelsen, Eugene K. ; Huber, A. Leon; and Riley, J. Paul.

A HYDROLOGIC MODEL OF THE BEAR RIVER BASIN

Research Project Technical Completion Report to the Office of Water Resources Research, Department of the Interior, August 1970, Washington, D. C. , 85 p.

KEYWORDS--*hydrologic models/*hydrologic simulation/*computer simulation/*simulation/groundwater/*watershed studies/snowmelt/evapotranspiration/deep percolation/water yields/*hydrologic relationship/*hydrologic research/*hydrology/hydrologic data/water yield improvement/soil moisture/*water resource planning and management/*hybrid computer

ACKNOWLEDGMENTS

This publication represents the final report of a project which was supported in part with funds provided by the Office of Water Resources Research of the United States Department of the Interior as authorized under the Water Resources Research Act of 1964, Public Law 88-379. The work was accomplished by personnel of the Utah Water Research Laboratory in accordance with a research proposal which was submitted to the Office of Water Resources Research through the Utah Center for Water Resources Research at Utah State University. This University is the institution designated to administer the programs of the Office of Water Resources Research in Utah.

The authors express gratitude to all others who contributed to the success of this study. In particular, special thanks are extended to Mr. Daniel F. Lawrence, Director of the Division of Water Resources, Utah Department of Natural Resources. The Division supplied substantial financial support for the study, and in addition, Mr. Lawrence and his staff provided valuable suggestions and direction throughout the entire project. In this respect, special acknowledgment is due to Dr. Norman E. Stauffer, Jr. of the Division of Water Resources who made substantial contributions during the model verification phase of the study. Appreciation is also expressed to Dr. Robert R. Lee, Director of the Idaho Water Resources Board, and to Mr. Floyd A. Bishop, Wyoming State Engineer. Dr. Lee and Mr. Bishop and several members of their staffs were most helpful in providing needed data and constructive comments at various times during the course of the study.

Sincere thanks are also extended to Dr. Jay M. Bagley, Director of the Utah Water Research Laboratory, and to Mr. Frank W. Haws, a Research Engineer at the laboratory. On the basis of their broad experience with the hydrologic system of the Bear River basin, these colleagues were able to provide valuable advice and direction throughout the entire project.

Robert W. Hill
Eugene K. Israelsen
A. Leon Huber
J. Paul Riley

TABLE OF CONTENTS

Chapter I		Available soil moisture quantities . . .	17
INTRODUCTION	1	Infiltration	17
General	1	Evapotranspiration	17
Scope of Study	1	Effects of soil moisture on evapotranspiration	19
Objectives	1	Effects of slope and elevation on evapotranspiration	19
Procedures	2	Deep Percolation	20
Discussion	2	River Outflow	20
Chapter II		Chapter IV	
THE BEAR RIVER BASIN	3	THE COMPUTER MODEL	23
Description of the Study Area	3	Chapter V	
Climate	5	APPLICATION OF THE HYDROLOGIC MODEL TO THE BEAR RIVER BASIN	27
Soil Materials	5	Verification	27
Surface Flows	5	Sensitivity Analysis	28
Land Use	5	Management Opportunities	28
Subbasins	6	Case 1	30
Chapter III		Cases 2 and 3	37
THE HYDROLOGIC MODEL	7	Chapter VI	
Formulation of a Hydrologic Model	7	SUMMARY AND CONCLUSIONS	39
Model Requirements	7	BIBLIOGRAPHY	41
The Conceptual Model	7	APPENDIX A: Subbasin Input Data	43
The Hydrologic Balance	8	APPENDIX B: Computer Program	47
Time and Space Increments	8	APPENDIX C: Modified Input Data, Model Coefficients, and Output Data	67
System processes	10	APPENDIX D: Management Opportunities	79
Surface Inflows	10		
Interflow	12		
Groundwater Inflow	12		
Total Inflow	13		
Precipitation	13		
Temperature	14		
Snowmelt	14		
Canal Diversions	15		
Available Soil Moisture	16		

LIST OF FIGURES

Figure		Page	Figure		Page
2.1	The Bear River basin and subbasins	4	5.8	Computed and observed monthly outflow from Cache Valley subbasin 1954, 1955, and 1956	34
3.1	Development process of a hydrologic model	9	5.9	Computed and observed monthly outflow from Tremonton subbasin 1954, 1955, and 1956	35
3.2	Flow diagram for a typical hydrologic model using large time increments	9	5.10	Management of Evanston subbasin, Case 1	35
4.1	Two views of the hybrid computer facility at the Utah Water Research Laboratory	24	5.11	Management of Evanston subbasin, Case 2	36
4.2	General view of the program control structure	25	5.12	Management of Evanston subbasin, Case 3	36
4.3	A flow diagram of the subroutine interaction for program OPVER	26	B.1	Flow chart of hydrologic simulation program OPVER	49
5.1	Computed and observed monthly outflow from Evanston subbasin 1954, 1955, and 1956	31	B.2	Schematic diagram of operating procedures for OPVER	50
5.2	Computer and observed monthly outflow from Randolph subbasin 1954, 1955, and 1956	31	B.3	Deck setup for typical OPVER run	51
5.3	Computer and observed monthly outflow from Cokeville subbasin 1954, 1955, and 1956	32	B.4	List of typical input data for OPVER	56
5.4	Computed and observed monthly outflow from Thomas Fork subbasin 1954, 1955, and 1956	32	B.5	Analog computer program for use with OPVER	57
5.5	Computed and observed monthly outflow from Bear Lake subbasin 1954, 1955, and 1956	33	B.6	List of digital computer program OPVER with all subroutines	58
5.6	Computed and observed monthly outflow from Soda subbasin 1954, 1955, and 1956	33	B.7	Flow chart of subroutine HYDSM	63
5.7	Computed and observed monthly outflow from Oneida subbasin 1954, 1955, and 1956	34	B.8	Flow chart of subroutine BASIC	64
			B.9	Flow chart of subroutine SUBDAT	65
			B.10	Flow chart of subroutine RESRV	66

LIST OF TABLES

Table	Page	Table	Page
2.1	6	B.2	52
Summary of water related land use in the Bear River basin (all units in acres).		Preparation instructions for BASIC data - group 2 cards	
5.1	29	B.3	53
Sensitivity of Evanston subbasin variables		Preparation of subbasin data cards - group 3 cards	
5.2	30	B.4	54
Computer printout showing summary of calibration process		Preparation instructions for pattern search specification	
B.1	52	B.5	54
Preparation instructions for OPVER option control cards - group 1 cards		Notation for OPVER and its subroutines	



CHAPTER I
INTRODUCTION

General

Of the total precipitation falling on watersheds throughout the world, an average of approximately 85 percent returns directly to the atmosphere through evaporation and use by mountain vegetation. The remaining 15 percent moves from the watersheds as runoff and becomes available in the valleys to be used by man for irrigation, industry, recreation, and many other requirements. The very rapid growth of these requirements in recent years has led to an increasing need for additional usable water resources.

Several grandiose and costly schemes have been suggested to supplement existing water resources in the western United States. The enormity of the engineering, social, and legal aspects of implementing one of these schemes certainly shifts the realization of the proposed resource supplement well into the future. However, the need for additional water resources protrudes from immediate future requirements and refuses to disappear even though ignored. Alternative methods must then be identified in order to satisfy or appease the immediate future requirements.

Alternate methods of supplementing water resources must be almost immediately applicable, relatively inexpensive, and effective. Some of the methods proposed to fill the immediate need include groundwater mining, conjunctive use of ground and surface water, and more efficient use of existing supplies. The research work described in this report has focused on the efficient use of existing supplies.

Efficient use of water in a dynamic system implies that the system be described with sufficient accuracy to quantitatively predict depletions resulting from water use in the system. The next step is to realistically alter the system parameters

and points of use to determine system configurations which produce increased benefits and/or decreased water use. The ultimate result of this method is to determine the system configuration which maximizes the benefits per unit of water resource depletion. Water use includes the consumptive use of water and the addition of undesirable elements to the water. This report, however, deals with the hydrology and consumptive use of water in the Bear River basin.

System simulation is a tool currently employed by many researchers to increase the definition of dynamic systems. Since hydrologic systems, like the Bear River basin, are certainly dynamic, the tool of simulation modeling was employed to gain increased system definition. The various processes within the model are linked by the continuity of mass principle, which requires a hydrologic balance at all points. The computer is essential for the solution of the time-dependent differential equations of the model and for the selection of coefficients required during calibration and testing.

Scope of Study

The scope of this study is limited to describing the hydrology of the Bear River basin and demonstrating the possibility of increased efficiency of water use through selection of proper management alternatives.

Objectives. The objectives of this research project were as follows:

1. To simulate the complex hydrologic flow system of the Bear River basin.
2. To demonstrate the applicability of the simulation model to efficient water resources planning in the Bear River basin by evaluating various alternative management possibilities subject to selected constraints.

Procedure

To meet the objectives of this study the following procedure was followed:

1. Basic hydrologic data for the Bear River basin were assembled and analyzed.
2. The Bear River basin was divided into ten subbasins based upon the available hydrologic data and the physical characteristics of the basin.
3. A simulation model was verified for each subbasin. These subbasin models were then linked together to form the model of the entire basin.
4. Three management alternatives were applied to a single subbasin (Evanston) to demonstrate the use of the model in selecting management alternatives.

Discussion

Several problems were encountered during the modeling of the ten subbasins. These problems stemmed from the lack of adequate data required to verify proposed model configurations. Determination of ungaged surface and subsurface flows always presents a problem, but this problem can usually be solved if other data requirements are satisfied. Correlation techniques provide satisfactory estimates of temporal and spatial distribution of ungaged flows. Records of water diversion for irrigation use were lacking in all of the subbasins. Irrigation diversions are important because they alter the hydrologic system, and thus affect stream depletions, groundwater inputs, evapotranspiration losses, and irrigation delivery efficiencies. Records for other required inputs were adequate for formulating satisfactory models.

The Bear Lake and Malad subbasins presented the largest problem in the verification process. The Bear Lake subbasin seems to have a large amount of ungaged inflow and evaporation losses from the lake surface are high. Flow records, diversion records, and data for correlation are lacking for the Malad subbasin. Because of this

problem the Malad model could not be satisfactorily verified. Fortunately, however, the subbasin does not include any of the main stem of the Bear River, and inflows of the Malad River to the Bear River are gaged. All other subbasins could be satisfactorily verified. Until sufficient data are available, the Malad subbasin will be deleted from management studies.

Management applications were demonstrated in the four upper subbasins by changing land use patterns. Perhaps the most significant change in land use would be the complete removal of phreatophytes and this alternative was demonstrated in one of the management runs. Other possible management schemes, not yet tested by the model, might involve the construction of additional reservoirs, enlargement of existing reservoirs, alteration of reservoir operating rules, and various combinations of reservoir operation and land use patterns. Export of water from the basin could be studied though, at present, there are no facilities to perform sizable exports. The management schemes shown are to demonstrate the capability of the model to predict system responses to proposed or desired changes within the system.

CHAPTER II THE BEAR RIVER BASIN

Description of the Study Area

The boundaries and subbasins of the Bear River basin are shown in Figure 2.1, which also indicates the location of the existing streamflow measuring stations.

The Bear River (USBR, 1970) originates in Utah but flows through parts of Wyoming, Idaho, and Utah before entering the Great Salt Lake. This interstate river is the largest stream in the Western Hemisphere which terminates before reaching the ocean. The river winds and twists about 500 miles in a U-shaped course to cover the 90 airline miles from its origin to its mouth. Included in the Bear River basin are 7,465 square miles of mountain and valley lands.

From its Utah origin the river flows for 20 miles down the north slopes of the Uinta Mountains, Utah's east-west mountain range. Near the Wyoming border the river enters the Bear River Valley, the first of five major valleys. The valleys are separated by narrow canyons or gorges which form ideal locations for hydroelectric power generation.

The Bear River Valley is the highest and longest valley in the Bear River basin. The valley is narrow, five miles or less in width, and extends for nearly 100 miles along the western border of Wyoming. However, a significant portion of the valley lies in Utah and Idaho.

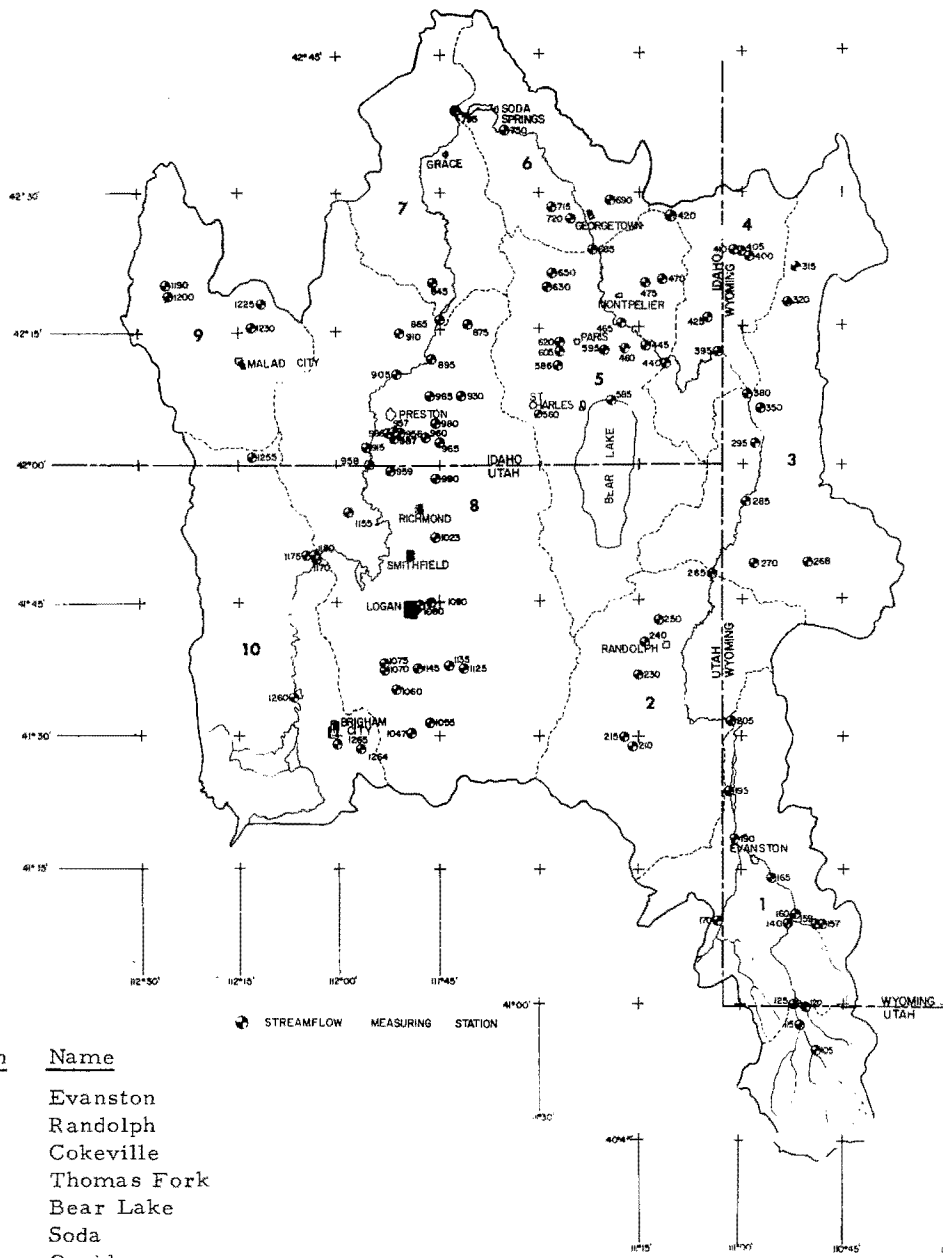
Near the Idaho border the river flows westward to enter the Bear Lake Valley which is about 50 miles long and 12 miles wide. The south end of Bear Lake valley is occupied mostly by Bear Lake and Mud Lake. Bear Lake is about 20 miles long and averages seven miles in width, while Mud Lake, at the north end of Bear Lake, is about three miles in diameter. Bear River did not naturally flow into Bear Lake, but inlet and outlet canals have been constructed north of

the lakes to facilitate hydroelectric power generation. A combined active storage of these two lakes of about 1,450,000 acre-feet provides a complete control of the flow in Bear River at that location.

The river flows northwest from the Bear Lake Valley through several miles of hilly and broken grazing lands and through a narrow channel near Soda Springs, Idaho, into Gem Valley. In the narrow lava channel are located the Soda Reservoir and hydroelectric power plant. Gem Valley is a broad agricultural area which was formed in the northern and central portions by a lava flow plain. Originally, the Bear River flowed north through Gem Valley to the Snake River. However, lava flows eventually turned the course of Bear River south toward the Great Salt Lake. Gem Valley south of the lava flow is about 500 feet lower than the central portion. This drop is used for power generation. The southern portion of Gem Valley is also called Gentile and Mound Valley. At the south end of Gem Valley the river enters the Oneida Narrows, a canyon about 11 miles long, which forms another power generation location.

From Oneida Narrows the Bear River enters Cache Valley, one of the more highly developed valleys in the Bear River basin. The river enters Cache Valley from the northeast, meanders southward, and leaves the valley through a gorge into the Lower Bear River Valley. Cache Valley is about 45 miles long and 10 miles wide. Several tributaries enter Cache Valley and combine with Bear River prior to leaving the valley. The gorge followed by the river in leaving Cache Valley forms a good location for power generation.

The Bear River continues through the Lower Bear River Valley and into the Great Salt Lake. The Lower Bear River Valley is part of the generally flat



Subbasin	Name
1	Evanston
2	Randolph
3	Cokeville
4	Thomas Fork
5	Bear Lake
6	Soda
7	Oneida
8	Cache Valley
9	Malad
10	Tremonton

Figure 2.1. The Bear River basin and subbasins.

Salt Lake Valley that drains toward the Bear River. The Malad River enters the Bear River in the Lower Bear River Valley from an origin some 50 miles to the north.

Valley elevations range from 7,800 feet near Evanston, Wyoming, in the Bear River Valley to 4,200 feet at the Bear River Bay in the Lower Bear River Valley.

Climate

Wide seasonal and diurnal temperature variations characterize the typical mountain continental climate of the Bear River basin. The high valleys have long hard winters and short cool summers. The climate of the lower valleys is generally more moderate. The average frost-free season varies from about 30-days in the higher valleys to over 150 days in the Lower Bear River Valley. Precipitation is heaviest in the mountain sections with the majority of precipitation coming as snow. About one-third of the annual precipitation occurs during the growing season which results in the irrigation water demand on the Bear River and its tributaries.

Soil Materials

Soils in the Bear River basin have been deposited by winds, lakes, and streams. The parent materials are quartzites and sandstones in the upper valleys; limestone, dolomites, and sandstone in the central valleys; and tuffaceous sediments, limestone, shale, and basalts in the lower valley.

Surface Flows

The maximum annual flows normally occur during the snowmelt period in May or June, but can also appear in April or July. The maximum discharge at the Utah-Wyoming border of 2,860 cfs occurred on June 12, 1965. The maximum discharge recorded at the Harer station near the lower end of the Upper Bear River Valley was 4,440 cfs on May 7, 1952. The maximum flow in the Lower Bear

River Valley near Corinne was 7,200 cfs on May 3, 1952. The maximum flows result from melting snow and spring rainstorms. After the snow has melted, the river flow drops to a low level and remains fairly constant through the remainder of the year. Minimum flows have occurred in April, September, October, and November. Local, high intensity, summer thundershowers cause high flows in tributaries but seldom cause record setting flows in the main stem.

Diversion of water from the main stem of the Bear River and its tributaries has increased since about 1860. The consumptive use associated with the increased diversions has affected river flows throughout the entire basin. The average flow near the upper part of the river near the Utah-Wyoming state line is about 135,000 acre-feet per year. The average annual flow at the Harer station east of Dingle, Idaho, is about 367,000 acre-feet. Near Corinne, Utah, the average annual flow of the Bear River is nearly 1,174,000 acre-feet. The length of records used to obtain these estimates is not equal, and the flows are partly controlled; but the comparison does portray the relative magnitudes of flow at successive downstream points along the course of the Bear River.

The quantity of water used consumptively by irrigated crops is usually much less than the total quantity applied. Water used consumptively by evaporation and plant transpiration is lost to the basin. Part of the water applied, but not used consumptively, either percolates to the water table or returns directly to the stream as overland flow. These waters become available for reuse.

Land Use

The land use in the Bear River system ranges from pasture and meadow hay in the upper reaches through pasture, alfalfa, and grains in the middle reaches to potatoes, sugar beets, and small truck garden items in the lower reaches. Pasture, alfalfa, and grains are also grown in certain areas of the

lower subbasins. In addition, lakes, rivers, and marshes occupy significant areas within the Bear River basin. The water-loving vegetation which borders these water bodies is classified into the general category of phreatophytes. Because phreatophytes deplete the water supplies they were considered in the model. Municipalities and dwellings cover many acres in the basin. Land use statistics are summarized in Table 2.1.

Subbasins

In developing a hydrologic model, spatial resolution is achieved by dividing the total area into specific spatial increments or subbasins. Increasing the number of subbasins within a particular area increases the spatial resolution of the model, and there-

fore, its general utility. However, this trend also increases model complexity, so that data and computer requirements are also usually substantially increased. The selection of the appropriate spatial increment is, therefore, an important phase of hydrologic modeling, and is based upon many considerations, the most important of which is data availability, land and water use patterns, and the resolution required in answering questions relating to basin planning and management problems. In this study the Bear River basin was divided into 10 subbasins, and each of these is outlined in Figure 2.1. Only the valley floor was included in the hydrologic model of each subbasin with surface and subsurface flows to this area being included as inputs to the model.

Table 2.1. Summary of water related land use in the Bear River basin (all units in acres).

Crops	Subbasins	Evanston	Randolph	Conrad	Thomas	Bear	Soda	Oneida	Cache	Malad	Tremonton
		01	02	03	Fork 04	Lake 05	06	07	Valley 08	09	10
Alfalfa	1	2599	1916	577	425	8959	2677	11873	52429	8006	17803
Pasture	2	8823	5518	9076	7435	12347	3703	5381	27563	7254	13750
Other hay	3	19835	40025	18982	13064	20121	6098	2367	6058	753	1158
Small grains	4	314	1213	510	319	10098	3022	7927	50020	5064	16645
Corn	5					42		36	9469	182	6513
Sugar beets	6							1471	4827	137	8612
Potatoes	7							1363	289	91	72
Orchard	8								392		2093
Peas	9								0		0
Tomatoes	10								3		507
Small truck	11					46		466	683		217
Idle	12								0		0
Beans	13								275		217
Total		31571	48672	29145	21243	51613	15500	30884	152008	21487	67587
Open water	B	632	884	0	291	21283	848	597	7515	1172	934
Marshes, tules, cattails	C1	609	2145	68	720	7307	0	0	15863	1758	3092
Grasses, willows, cottonwoods	C2	3523	765	1344	199	3100	2886	1233	15771	2930	4525
Grasses & med. density trees	C3	261	608	15	0	2636	0	0	5776	0	2698
Low water table, light density	C4	2434	2073	803	924	8030	1890	1005	7775	163	9506
Total		7459	6475	2230	2134	42356	5624	2835	52700	6023	20755

CHAPTER III THE HYDROLOGIC MODEL

Simulation is a technique for investigating the behavior or response of a dynamic system subject to particular constraints and input functions. This technique has been applied by means of both physical and electronic models. Physical models and analog models consisting of electrical resistor-capacitor networks have been used to investigate hydraulic and hydrologic phenomena for many years. However, simulation by means of high-speed electronic computers is a relatively new technique.

The advantages of simulation include the following:

1. The system can be non-destructively tested, which is of practical interest in the hydrologic design of structures such as large dams and flood control works in a river basin.
2. Proposed modifications of existing systems can be tested for improved performance. This is especially desirable if the original system is in operation, since operation time will not be lost during testing.
3. Hypothetical system designs may be verified at minimum expense, thus paying large dividends if the proposed system turns out to be inefficient.
4. Simulation provides insight into the system being studied and is thus a powerful teaching device.

Formulation of a Hydrologic Model

Model Requirements

The fundamental requirements of a computer model of a hydrologic system are:

1. It simulates on a continuous basis all important processes and relationships within the system it represents.
2. It is non-unique with respect to space.

This implies that it can be easily applied to different geographic areas with existing hydrologic data.

3. It is capable of answering questions concerning perturbations in the system or of accurately predicting outputs resulting from varying input and process parameters.

The general research philosophy involved in the development of a simulation model of a dynamic system, such as a hydrologic unit, is shown by the flow diagram of Figure 3.1. In addition to predicting system responses to particular input functions and parameter changes, the process of model development provides for improvement of system relationships.

The Conceptual Model

The hydrologic model utilized in this study is a modified version of that developed in earlier studies involving the computer simulation of a complete watershed unit (Riley et al., 1966 and 1967). Simplification was achieved by including only the valley bottom lands of each subbasin.

The basis of the hydrologic model is a fundamental and logical mathematical representation of the various hydrologic processes and routing functions. These physical processes are not specific to any particular geography, but rather are applicable to any hydrologic unit, including all of the subbasins located within the Bear River basin. Experimental and analytical results were used whenever possible to assist in testing and establishing some of the mathematical relationships included within the model. Under a model verification procedure, equation constants are established which calibrate or fit the model for a particular drainage area. Average values of hydrologic quantities needed for model verification were estimated in one of three ways:

(1) From available data, (2) by statistical correlation techniques, and (3) through verification of the model.

A flow diagram of the hydrologic system is shown by Figure 3.2. As this flow chart indicates, the total input to a subbasin is the combination of surface and subsurface inflows of water obtained by summing river and tributary inflows, precipitation, and imports from other basins. Depletions from the subbasins occur through evapotranspiration, municipal and industrial consumption, and exports. The residual quantity is a combination of surface and subsurface outflow of water from the area. Subsurface flows may undergo various time delays as they move through the system. Each parameter and process depicted by Figure 3.2 is discussed in some detail in the following sections.

The Hydrologic Balance

A dynamic system consists of three basic components, namely the medium or media acted upon, a set of constraints, and an energy supply or driving force. In a hydrologic system, water in any one of its three physical states is the medium of interest. The constraints are applied by the physical nature of the hydrologic basin, and the driving forces are supplied by direct solar energy, gravity, and capillary potential fields. The various functions and operations of the different parts of the system are interrelated by the concepts of continuity of mass and momentum. Unless relatively high velocities are encountered, such as in channel flow, the effects of momentum are negligible, and the continuity of mass becomes the only link between the various processes within the system.

Continuity of mass is expressed by the general equation:

$$\text{Input} = \text{Output} \pm \text{Change in storage}$$

A hydrologic balance is the application of this equation to achieve an accounting of physical, hydrologic measurements within a particular unit. Through this means and the application of appropriate translation or routing functions, it is possible to predict the movement of water within a system in terms of its occurrence in space and time.

The concept of the hydrologic balance is pictured by the block diagram in Figure 3.2. The inputs to the system are precipitation and surface and groundwater inflow, while the output quantity is divided among surface outflow, groundwater outflow, and evapotranspiration. As water passes through this system, storage changes occur on the land surface, in the soil moisture zone, in the groundwater zone, and in the stream channels. These changes occur rapidly in surface locations and more slowly in the subsurface zones.

In the course of model development, each of the system processes must be described mathematically as completely as possible. The flow chart of Figure 3.2 is a schematic representation of the system processes and storage locations and their relationship to each other. In the model each box and connecting line is represented by a mathematical expression.

Time and Space Increments

Practical data limitations and problem constraints require that increments of time and space be considered during model design. Data, such as temperature and precipitation readings, are usually available as point measurements in terms of time

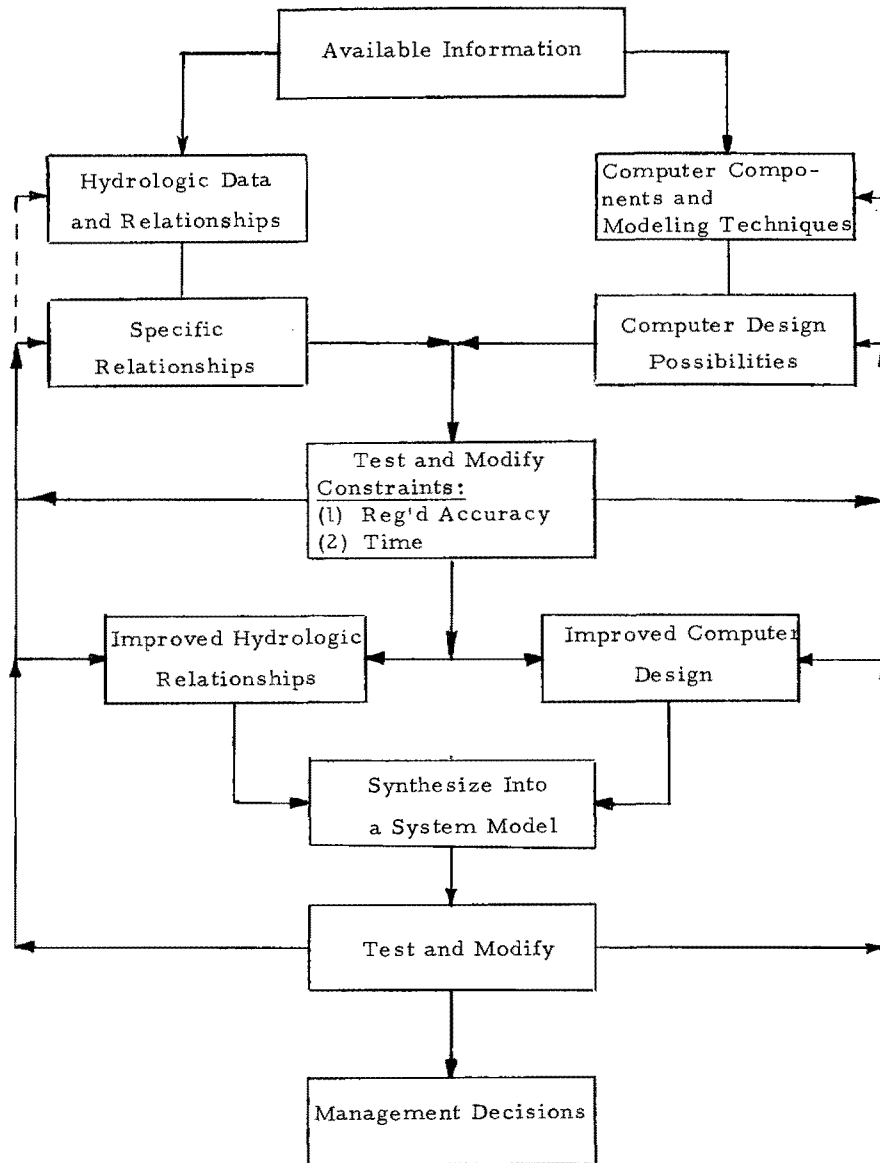


Figure 3.1. Development process of a hydrologic model.

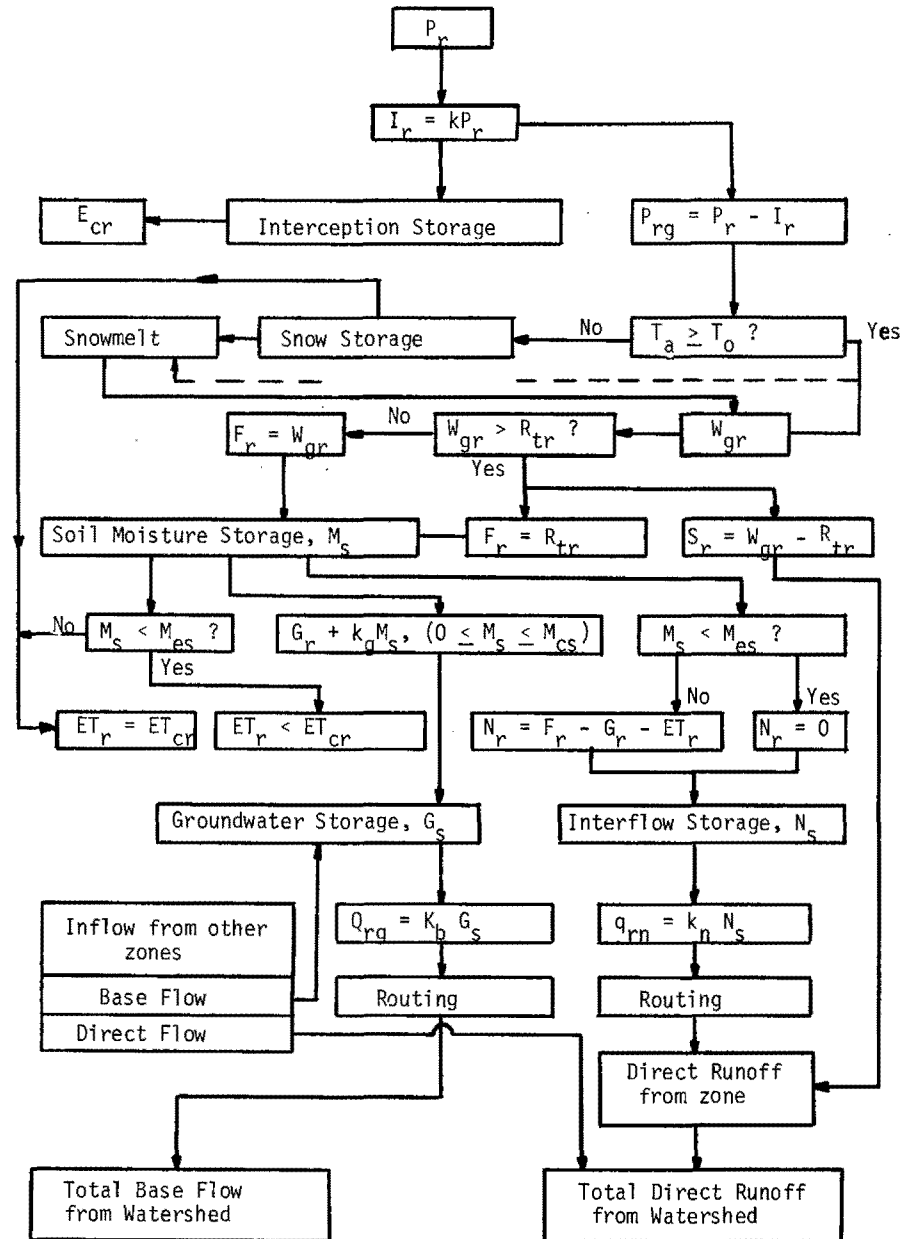


Figure 3.2 Flow diagram for a typical hydrologic model using large time increments.

and space; and integration in both dimensions is usually accomplished by the method of finite increments.

The complexity of a model designed to represent a hydrologic system largely depends upon the magnitude of the time and spatial increments utilized in the model. In particular, when large increments are applied, the scale magnitude is such that the effect of phenomena which change over relatively small increments of space and time is insignificant. For instance, on a monthly time increment, interception rates and changing snowpack temperatures are neglected. In addition, the time increment chosen might coincide with the period of cyclic changes in certain hydrologic phenomena. In this event net changes in these phenomena during the time interval are usually negligible. For example, on an annual basis, storage changes within a hydrologic system are often insignificant, whereas on a monthly basis, the magnitude of these changes are frequently appreciable and need to be considered. As time and spatial increments decrease, improved definition of the hydrologic processes is required. No longer can short-term transient effects or appreciable variations in space be neglected, and the mathematical model, therefore, becomes increasingly more complex with an accompanying increase in the requirements of computer capacity and capability.

For the study of the Upper Bear River basin discussed by this report, a monthly time increment and large space units (subbasins) were adopted. Selection of the subbasins was based on hydrologic boundaries and points of data collection. It was felt that the selection of the subbasins and the monthly time increment would satisfy the requirements of a general planning-management model for the basin.

System Processes

Surface Inflows

The basic inflow or input of water into any hydrologic system originates as a form of precipitation. However, for simulation models of valley floor areas, direct precipitation input to the system is greatly overshadowed by river and tributary inflows.

Streamflow is defined as that portion of the precipitation which appears in streams and rivers as the net or residual flow collected from all or a portion of a watershed. When unaffected by the activities of man, such runoff is referred to as "natural or virgin" flow. Except in headwater reaches, no streams in the Bear River basin now carry natural flows. Artificial diversions and regulatory action in lakes and reservoirs affect the regimes of every stream within the basin.

The surface water inflow component consists of flow traveling over the ground surface and through channels to enter a stream. At the stream, surface runoff usually combines with other flow components to form the total surface runoff hydrograph. Within the runoff cycle (Chow, 1964), surface runoff begins to occur when the capacities of vegetative interception, infiltration, and surface retention are reached. Continued precipitation beyond this point serves as a source for surface runoff. Small basins have different runoff characteristics than do large watersheds, and the characteristics peculiar to each basin must be evaluated on an individual basis.

For each subbasin in the Bear River basin, a limiting rate of surface runoff exists for any particular time period. Surface runoff is assumed to occur when the threshold or limiting rate of surface water supply, consisting of snowmelt, rainfall,

canal diversions, or any combination of these, is exceeded.

This concept of surface runoff is particularly important when precipitation is considered as the initial water input to the watershed. Riley and Chadwick (1966) indicate that for particular conditions there exists a limiting or threshold rate of surface supply, R_{tr} , at which surface runoff, S_r , begins to occur. This relationship can be written:

$$S_{wr} = W_{gr} - R_{tr}, \quad (S_{wr} \geq 0) \quad (3.1)$$

in which

- S_{wr} = rate of surface runoff during a particular time
- W_{gr} = rate at which water is available at the soil surface
- R_{tr} = limiting or threshold rate of surface water supply at which surface runoff begins to occur

When considered for a model time increment of one month, an average value of the threshold surface runoff rate, R_{tr} , is probabilistic in nature, depending essentially upon soil surface conditions, soil moisture, storm characteristics, and rate of available water, W_{gr} .

In this study only the valley bottom lands are considered in the model, and it is assumed that no surface runoff from precipitation occurs from these relatively flat areas. Under this assumption, the rate at which precipitation is available at the soil surface at no time exceeds the threshold rate for surface runoff to occur. Thus,

$$S_{wr} = 0, \quad (W_{gr} \leq R_{tr}) \quad (3.2)$$

The model does provide for surface runoff from agricultural lands due to irrigation application rates which exceed soil infiltration rates. This runoff quantity constitutes a portion of the irrigation return flow.

Surface runoff from the surrounding watershed areas is concentrated in stream channels, and therefore enters the model (valley bottom) as tributary flow. That part of the inflow rate which is measured or gaged is designated as $Q_{is}(m)$.

Unmeasured surface inflows to the model are estimated by a correlation technique which considers three hydrologic parameters, namely a gaged tributary inflow rate, precipitation rate, and snowmelt rate. Thus, in functional form:

$$Q_{is}(u) = f[q_{is}(m), P_r, W_{sr}] \quad (3.3)$$

in which

- $Q_{is}(u)$ = estimated rate of unmeasured surface inflow
- $q_{is}(m)$ = measured rate of surface inflow from a particular tributary area
- P_r = gaged precipitation rate in the form of rain on the valley floor
- W_{sr} = estimated snowmelt rate in terms of water equivalent

If empirical correlation factors are included in the preceding equation, the expression becomes:

$$Q_{is}(u) = k_u q_{is}(m) + k_a P_r + k_b W_{sr} \quad (3.4)$$

in which k_u , k_a , and k_b are correlation factors relating ungaged surface inflow rate to, respectively, a gaged surface inflow rate, precipitation rate, and snowmelt rate. Each of these factors is established through the model verification process for a particular subbasin.

With reference to the measured tributary inflow rate, $q_{is}(m)$, used in Equation 3.4, this quantity might refer to either the total measured tributary inflow or a specific stream within the area. The main criterion for selecting the gaged area is that the watershed exhibit the same general runoff characteristics as that of the ungaged area.

The second independent term in Equation 3.4 refers to the rates of precipitation occurring on the valley floor in the form of rain. Because it is assumed that the influence of snow upon the surface runoff is restricted to the melt period, only rainfall is considered by the equation. Generally, a direct plot of rainfall against runoff for individual storms yields a low correlation because of the variable nature of the factors affecting runoff (Chow, 1964). However, when mean monthly values of precipitation and runoff are considered, many of the transient processes are smoothed and reasonably good correlation of runoff with precipitation is achieved.

The third independent term of Equation 3.4 considers the influence of snowmelt upon surface runoff. Snowmelt rates on the valley floor are predicted in the model by Equation 3.9. This process is discussed in further detail later in this chapter.

The total surface inflow rate to the model (valley floor) is estimated by summing the measured rate and estimated ungaged rate from Equation 3.4. Thus,

$$Q_{is} = Q_{is}(m) + Q_{is}(u) \dots \dots \dots (3.5)$$

in which Q_{is} refers to the total surface inflow rate, and the two independent quantities are as previously defined.

Interflow

Interflow is defined as the lateral movement of moisture through the plant root zone. The process is discussed in further detail at a later point in this chapter. Interflow rate, N_r , is not treated as a separate identity in the hydrologic model of the valley bottoms, but is considered as being a part of the surface runoff from irrigation. In most cases, small interflow rates are encountered in flat lands. Furthermore, for a model time increment of one month, interflow usually produces an insufficient delay time to enable this quantity to be distinguished from surface runoff.

Groundwater Inflow

Groundwater or subsurface inflow refers to those waters which enter the model area or valley floor beneath the ground surface. Much of this water is subsequently discharged as effluent flow into the main channel of the valley, and thus provides a "base flow" for the stream. Discharge from the groundwater basin of the valley floor also occurs by way of spring flows, pumped waters, and consumptive use by phreatophytes.

Essentially, all groundwater is constantly in motion though velocities may range from several feet per day to only a few inches per year. This groundwater movement is basically confined to permeable geologic formations called aquifers which serve as transmission conduits. Movement and volume of groundwater runoff may be calculated through application of Darcy's Law, providing adequate data are available. However, subsurface flow data are sparse within the Bear River basin. Time and spatial distribution of groundwater flows in this study were estimated by an empirical approach through the model verification procedure. For the steep watersheds near the headwaters of major drainage divisions, groundwater inflows to the valley floors were usually sufficiently small to be neglected. As the study proceeded downstream to lower subbasins, it generally became apparent through the time distribution of the water inputs to the model in relation to the recorded outflow that groundwater inflow rates were appreciable. Correlation procedures and transport delays were then used to estimate and simulate groundwater movement into the subbasin. This water was then distributed with time through use of long transport delay networks on the computer. The required delay setting of these networks was established during the model verification process. Hence, the rate of groundwater inflow was described as follows:

$$Q_{ig}(u) = k_c q_{is} \dots \dots \dots (3.6)$$

in which

$Q_{ig}(u)$ = rate of total unmeasured inflow to the groundwater system

k_c = coefficient relating the rate of unmeasured groundwater inflow to a measured surface runoff rate

q_{is} = rate of surface runoff (either total measured tributary inflow or measured tributary inflow or measured inflow from a representative tributary)

For some subbasins a subsurface outflow, as groundwater movement under the outflow gage in the streambed alluvium, was determined by the model verification process. The time and spatial distribution of this outflow formed a component of the groundwater inflow or input to the adjacent downstream subbasin.

Total Inflow

Total inflow rate to the valley bottoms consists of the summation of the surface and groundwater flow rates. The surface inflows for the most part have already been summed and are concentrated in stream channels as they enter the valley floor or agricultural areas. Gaged surface inflow rates are available from surface water records published by the U. S. Geological Survey. These records were utilized wherever possible.

The remaining two components of total inflow, namely ungaged surface inflow and groundwater inflow, are estimated from Equation 3.4 and 3.6, respectively. Therefore, the total inflow, Q_i , to a given subbasin within the Bear River basin is given by the following expression:

$$Q_i = Q_{is} + Q_{ig} \dots \dots \dots (3.7)$$

in which the terms Q_{is} and Q_{ig} are given by Equations 3.5 and 3.6, respectively.

Precipitation

The ultimate source of water input to any hydrologic unit is precipitation in one form or another. Precipitation is considered to be any moisture which emanates from the atmosphere and falls to the earth.

Precipitation input to the hydrologic system varies with respect to both time and space and it is therefore necessary to convert point measurements from climatological stations into an integrated or averaged monthly value over a finite area. Common spatial integration techniques include the Thiessen weighting procedures and the isohyetal method (Linsley, Kohler, and Paulhus, 1958). A modified isohyetal technique was used to estimate precipitation as a function of time for each subbasin. Some precipitation data are available for all subbasins adopted in this study.

Two forms of precipitation, rain and snow, are considered in this study. Air temperature is used as the criterion for establishing the occurrence of these two forms. This criterion is not an ideal index for determining the form of precipitation since no one temperature exists below which it always snows and above which it always rains. However, the surface air temperature appears to be the most suitable single index of precipitation form now available.

Based on investigations by the U. S. Army (1956) at a surface air temperature of 35°F, there is a 50 percent chance that precipitation will be as snow, whereas at 32°F the probability is 95 percent of precipitation falling as snow. However, in this study a double standard was used because average monthly temperatures provided the criteria. Snow was assumed to fall below about 35°F, and snowmelt was assumed to occur above about 30°F. This assumption provided for the occurrence of snowfall and snowmelt during the same month. These threshold temperatures varied in the different subbasins.

A part of the precipitation falling on an area is stored on the vegetative cover. Because most of this water later returns to the atmosphere through the evaporation process, vegetative interception is regarded as a loss. Interception losses which occur over a long time period, such as a month, are generally expressed as a fraction of the total precipitation for that period (U. S. Army, 1956). That part of the precipitation which reaches the ground, namely the difference between the total precipitation and the interception losses, is generally labeled as "effective precipitation" for the area.

The magnitude of the interception loss is basically a function of the type and density of the vegetative cover within the area. Interception losses for forested areas may be considerable, while interception losses for sparsely timbered and grass covered areas might be small. Since the model of this study includes only the valley floors, which are essentially flat, agriculturally oriented areas, interception losses are neglected, and all precipitation is assumed to be effective.

Some of the precipitation which reaches the ground is retained in depression storage. This form of storage includes puddles and other depressions in the soil surface. Water leaves depression storage through either direct evaporation or as infiltration into the soil. Thus, for models involving large time increments, such as a month, abstractions to depression storage need not be treated separately but can be assumed to be a part of the total evapotranspiration and infiltration loss from the total precipitation quantity.

Temperature

Air temperature is an important parameter in a hydrologic system because it can be utilized as a criterion for establishing the form of precipitation, and as an index of the energy available for the snowmelt and evapotranspiration processes. Temperature varies according to both time and space. To

obtain average temperature values for the valley floor, or a portion thereof, within a particular subbasin, requires that point measurements be utilized for estimating an effective or average temperature value for an area. One approach to this problem of spatial integration is to construct isothermal lines for particular time periods and to relate these to selected index stations (Riley and Chadwick, 1967). However, in this study average temperatures for a particular area and a given time period (one month) are estimated by an arithmetic average of temperature measurements taken in the subbasin.

Snowmelt

Although rational formulas which include the various factors involved in the snowmelt process have been developed, data limitations often prohibit a strictly analytical approach to the process. Rational models include fundamental processes, such as those which relate to energy transfer, and requirements for input data are high. An additional restriction to the analytical approach for snowmelt computation is a large modeling time increment such as a month. Many of the short-term, transient phenomena which occur within a snowpack cannot be represented in a macroscopic model of this scale. An empirical relationship was, therefore, adopted for this study model.

Riley et al. (1966) proposed a relationship which states that the rate of melt is proportional to the available energy and the quantity of precipitation stored as snow. As a differential equation the relationship is written:

$$\frac{d[W_s(t)]}{dt} = -k_s (T_a - T_b) \frac{RI_s}{RI_h} W_s(t) \quad (3.9)$$

in which the undefined terms are:

$$\begin{aligned} k_s &= \text{a constant} \\ T_a &= \text{surface air temperature in degrees} \\ & \quad \text{F} \end{aligned}$$

- RI_s = the radiation index on a surface possessing a known degree and aspect of slope
- RI_h = the radiation index for a horizontal surface at the same latitude as the particular watershed under study
- W_s = snow storage in terms of water equivalent
- T_b = assumed base temperature in degrees or F at which melt begins to occur.
In this study T_b was taken as being equal to 32°F.

Riley et al. (1966) report reasonable agreement between predicted snowmelt rates from Equation 3.9 and observed values. They used a value of k_s equal to 0.10 based on studies using data from several snow courses in the Rocky Mountain area where average snow depths are high. It has been found, however, that the value of k_s is somewhat inversely dependent upon snowpack depth. In other words, as the snow depth decreases pack melt rates increase for a given energy input. Thus, k_s is relatively larger for areas of shallow snowpack depth and relatively smaller for areas where depths tend to be large. The radiation index parameter allows adjustment to be made for variation of the total insolation with land surface slope and aspect. However, since only the valley floors are included in the modeling area, it is assumed that the topographic surface of the area is essentially horizontal. This assumption simplified Equation 3.9 in that RI_s becomes equal to RI_h and their ratio goes to unity.

The independent variables on the right side of Equation 3.9 can be expressed as either continuous functions of time or as step functions consisting of mean constant values for a given time increment. For this study a time increment was utilized and integration was performed in steps over each successive time period. Hence, the final values of W_s(t) at the end of a particular time period

became the initial value for the integration process over the following period. On this basis, and setting the ratio RI_s/RI_h equal to unity, the differential form of Equation 3.9 becomes:

$$\frac{W_s(1)}{W_s(0)} \int \frac{dW_s}{W_s} = -k_s(T_a - 32) \int_0^1 dt \quad \dots \quad (3.10)$$

$$W_s(1) = W_s(0) \exp[-k_s(T_a - 32)] \quad \dots \quad (3.11)$$

Canal Diversions

Canal diversions profoundly affect the time and spatial distribution of water within an irrigated area. A portion of this diverted water is evaporated directly to the atmosphere, a second part enters the soil profile through canal seepage and infiltration on the irrigated lands, and the remainder returns to the source as overland flow. Some of the water which enters the soil profile is lost through plant consumptive use. The remainder either percolates downward to the groundwater basin or is intercepted by drainage systems. Irrigation practices, therefore, alter the distribution characteristics of a hydrologic system. The irrigation efficiency factor used in this study includes both the conveyance and application efficiencies. Thus, multiplying total diversions by this factor provides an estimate of that quantity of water which returns directly to the stream as overland flow and/or interflow. This composite irrigation efficiency factor is given by the following expression.

$$\text{Eff} = 100 \frac{W_{dr}}{W_{tr}} \quad \dots \quad (3.12)$$

in which

- Eff = water conveyance and application efficiency in percent
- W_{dr} = rate at which diverted water enters the soil through seepage and infiltration

W_{tr} = total rate at which water is diverted from the stream or reservoir

Records of water diversion to the agriculture lands within each subbasin were found to be lacking. Adjustment of these records was necessary in many cases to get a realistic application rate for the irrigated acreage.

As already indicated, a portion of the water diverted for irrigation returns to the streams as overland flow and interflow. Although the large time increment allows this water to be treated in the model as a single identity, it is important to distinguish between the two components. Overland flow (often termed tailwater) is surface return flow or runoff from the end of the field resulting from the application of water to the irrigated land at rates exceeding the infiltration capacity of the soil. Interflow is defined as that part of the soil water which does not enter the groundwater basin, but rather which moves largely in a lateral direction through the upper and more porous portion of the soil profile until it enters a surface or subsurface drainage channel. Both the overland flow and the interflow return to the stream channels in short distances and times consisting of usually only a few days. The distribution of canal diversion within the hydrologic system can now be expressed as follows:

$$OF_r = (1 - \text{Eff}/100) W_{tr} + N_r \quad \dots \quad (3.13)$$

or

$$OF_r = (W_{tr} - W_{dr}) + N_r \quad \dots \quad (3.14)$$

in which

OF_r = total of overland flow (from irrigation applications at rates exceeding infiltration capacity rates and interflow rates)

N_r = interflow rate

All other quantities have been previously defined under Equation 3.12.

It is pointed out that evapotranspiration losses do not appear as such in Equation 3.13 and 3.14.

These losses are, however, considered because they are abstracted from the infiltration quantity represented by W_{dr} . The evapotranspiration process will be further discussed in a subsequent section.

Available Soil Moisture

The usual definition of available soil moisture capacity is the difference between the field capacity and the wilting point of the soil. Water within this range is available for plant use, and is termed available soil moisture. The field capacity is defined as the soil moisture content after gravity drainage has occurred. Most of the gravity water drains rapidly from the soil thus affording plants little opportunity for its use. The wilting point represents the soil moisture content when plants are no longer able to abstract water in sufficient quantities to meet their needs, and permanent wilting occurs. Available soil moisture can be expressed in several units but in this report it carries the unit of depth in inches.

Sources of available water. Basically, moisture in the soil is derived from infiltration, which is the passage of water through the soil surface into the soil profile. The water available for infiltration at the soil surface is derived from three sources, namely, effective precipitation in the form of rain, P_r , snowmelt, W_{sr} , and irrigation water, W_{dr} . As springtime temperatures rise to the point at which melting occurs, all snow cover on the land is assumed to melt and enter the soil mantle through the infiltration process. In the case of irrigated crops, the most important source of available soil moisture is water which is diverted to the agriculture lands. The rate at which water from this source enters the soil profile through canal seepage and infiltration has been designated as W_{dr} . Thus, the total water available for infiltration into the soil, W_{gr} , can be written as:

$$W_{gr} = W_{dr} + P_r + W_{sr} \dots \dots \dots (3.15)$$

in which all quantities are as previously defined.

Available soil moisture quantities. The maximum quantity of water in a soil available for use by plants is a function of the moisture holding capacity of the soil and the average rooting depth or extraction pattern of the plant.

The basic forces involved in the absorption of water by plants are osmotic, imbibitional, metabolic, and transpiration pull (Thorne and Peterson, 1954). These forces basically define the soil moisture tension or "pull" that must be exerted by the plant to remove water from the soil. Of these forces the principal one is the osmotic pressure created within plant root cells. Opposing these forces are those exerted on the moisture by the soil particles. The forces exerted by the plants vary with different plants, soils, and climates, but the average maximum force which plants can exert in obtaining sufficient water for growth is approximately 15 atmospheres of pressure. At field capacity where water is readily available for plant use, the average soil moisture tension is only about 0.1 atmosphere. However, the soil moisture tension or "pull" plants exert in their quest for water is in itself no indication of the amount of available water contained by the soil. The actual amount of water held by the soil at any given tension value is a function of the soil type.

Determination of the soil depth effectively utilized by a plant is based on the average rooting depth or the average moisture extraction pattern. The soil moisture available for extraction depends on the moisture holding capacity of the soil and the extraction pattern. The typical agriculture crop extracts 70 percent of its moisture from the upper 50 percent of the soil penetrated by the plant roots. Average or typical rooting depths for various plants are reported by McCulloch et al. (1967). Illustrative

depths include 4 to 6 feet for alfalfa, 4 feet for grains and corn, and 2 to 3 feet for pasture. The average available soil moisture capacity of the irrigated lands was estimated for each subbasin.

Under normal circumstances, additions to available soil moisture storage occur through the infiltration process, F_r . Abstractions or depletions from available soil moisture storage occur through evapotranspirational losses, ET_r , and deep percolation, G_r . The assumption is made, however, that deep percolation does not occur until the soil moisture capacity is reached. Thus, the soil moisture storage existing at any time, t , can be stated:

$$M_s(t) = (F_r - ET_r - G_r) dt \dots \dots \dots (3.16)$$

Each of the three terms on the right side of this equation is discussed in the following sections.

Infiltration

As already indicated, additions to available soil moisture occur through the process of infiltration, F_r . Factors which influence the infiltration rate include various soil properties and surface characteristics. A moisture gradient induced by the adhesive properties of the soil particles also influences infiltration rate.

In this study, the rate of infiltration into the soil is given by the following equations

$$F_r = W_{gr}, (W_{gr} \leq R_{tr}) \dots \dots \dots (3.17)$$

and

$$F_r = R_{tr}, (W_{gr} > R_{tr}) \dots \dots \dots (3.18)$$

for which all terms were previously defined. The quantity W_{gr} in Equation 3.17 is given by Equation 3.15.

Evapotranspiration

The second term on the right side of Equation 3.16 represents depletion from the soil moisture storage through the evapotranspiration

process, ET_r . Consumptive use, or evapotranspiration, is the sum of all water used and lost by growing vegetation due to transpiration through plant foliage and evaporation from the plant and surrounding environment such as adjacent soil surfaces. Potential evapotranspiration is defined as that rate of consumptive use by actively growing plants which occurs under conditions of complete crop cover and non-limiting soil moisture supply.

The evapotranspiration process depends upon many interrelated factors whose individual effects are difficult to determine. Included among these factors are type and density of crop, soil moisture supply, soil salinity, and climate. Climatological parameters usually considered to influence evapotranspiration rates are precipitation, temperature, daylight hours, solar radiation, humidity, wind velocity, cloud cover, and length of growing season. Numerous relationships have been developed for estimating the potential evapotranspiration rate.

Perhaps one of the most universally applied evapotranspiration equations is that proposed by Blaney and Criddle (1950). This equation is written as follows:

$$U = kf \dots \dots \dots (3.19)$$

in which

- U = monthly crop potential consumptive use in inches
- k = monthly coefficient which varies with type of crop and
- F = monthly consumptive use factor and is given by the following equation:

$$f = \frac{tp}{100} \dots \dots \dots (3.20)$$

in which

- t = mean monthly temperature in degrees F
- p = monthly percentage of daylight hours of the year

A modification to the Blaney-Criddle formula was proposed by Phelan et al. (1962), wherein the monthly coefficient, k, is subdivided into two parts, a crop coefficient, k_c , and a temperature coefficient, k_t . The relationship describing k_t is an empirical one, depending upon only temperature, and is expressed as:

$$k_t = (0.0173T_a - 0.314) \dots \dots \dots (3.21)$$

where T_a is the mean monthly temperature in degrees F. The crop coefficient, k_c , is basically a function of the physiology and stage of growth of the crop. Typical curves which indicate values of k_c throughout the growth cycle of particular crops are shown by Figure 3.3 which is for alfalfa. Similar k_c curves are available for many agriculture crops (Soil Conservation Service, 1964).

Thus, the modified Blaney-Criddle equation for estimating potential evapotranspiration rates is written as follows:

$$ET_{cr} = k_c k_t \frac{T_a p}{100} \dots \dots \dots (3.22)$$

Because of its simplicity, low data requirements (only surface air temperature is needed), and applicability to the irrigated areas of the Western United States, Equation 3.22 was adopted for this study model. Since the time increment selected for use was one month, the variables on the right of Equation 3.22 represent mean monthly values although these parameters could be expressed as continuous functions instead of the indicated step functions. Thus, Equation 3.22 estimates the mean potential evapotranspiration rate during each month.

The growing season was assumed to begin and end when the mean monthly air temperature reached a value of 32°F. Evapotranspiration losses from the agriculture area during the non-cropping season were estimated from Equation 3.22. For many crops it was necessary to extend the k_c curves to include the non-growing season (West,

1959). Because the k_c curve for grass pasture seems to represent a reasonable set of values for native vegetation (Riley et al., 1967), this curve was used as a guide in the development of a similar k_c curve for phreatophytes.

Effects of soil moisture on evapotranspiration.

As was discussed earlier, as the moisture content of a soil is reduced by evapotranspiration, the moisture tension which plants must overcome to obtain sufficient water for growth is increased. It is generally conceded that some reduction in the evapotranspiration rate occurs as the available quantity of water decreases in the plant root zone. Recent studies by the U.S. Salinity Laboratory in California (Gardner and Ehlig, 1963) indicate that transpiration occurs at the full potential rate through approximately the first one-third of the available soil moisture range, and that thereafter the actual evapotranspiration rate lags the potential rate. When this critical point in the available moisture range is reached, the plants begin to wilt because soil moisture becomes a limiting factor. Thereafter, an essentially linear relationship exists between available soil moisture quantity and actual transpiration rate. The actual evapotranspiration rate is expressed by Riley, Chadwick, and Bagley (1966) in accordance with the end conditions which accompany the two following equations:

$$ET_r = ET_{cr}, [M_{es} < M_s(t) \leq M_{cs}] \quad (3.23)$$

and

$$ET_r = ET_{cr} \frac{M_s(t)}{M_{es}}, (0 \leq M_s(t) \leq M_{es}) \quad (3.24)$$

in which

- ET_r = actual evapotranspiration rate
- ET_{cr} = potential evapotranspiration rate
- M_{es} = limiting or threshold content of available water within the root zone below which the actual becomes less than the potential evapotranspiration rate

- $M_s(t)$ = quantity of water available for plant consumption which is stored in the root zone at any instant of time
- M_{cs} = root zone storage capacity of water available to plants

Because they are differential with respect to time, both Equations 3.23 and 3.24 are easily programmed on the computer. In the integrated form Equation 3.24 appears as:

$$M_s(2) = M_s(1) \exp\left[-\frac{ET_{cr}}{M_{es}}(t_2 - t_1)\right] \quad (3.25)$$

in which $M_s(1)$ and $M_s(2)$ are the soil moisture storage values at time t_1 and t_2 , respectively. Hence, when conditions are such that the available soil moisture storage reduces the potential evapotranspiration rate, the actual consumptive use rate can be expressed by combining Equation 3.22 and 3.24 to read:

$$ET_r = \frac{M_s}{M_{es}} k_c k_t \frac{T_a}{100} \quad (3.26)$$

Equation 3.26 is programmed on the computer to estimate actual evapotranspiration rate. The equation reduces to Equation 3.22 when $M_s > M_{es}$ so that $ET_r = ET_{cr}$.

Effects of slope and elevation on evapotranspiration. In that they affect the available energy supply, land slope (degree and aspect) and elevation influence the evapotranspiration process. Riley and Chadwick (1967) considered the effects of slope by introducing a radiation index parameter. These same authors also introduced an elevation correction into Equation 3.26. This adjustment is necessary for watershed studies since surface air temperature becomes a less reliable index of the available energy with increased elevation above the valley floor. However, because the model of this study was confined to the relatively flat valley floor areas, the effect of both slope and elevation on the evapotranspiration rate is neglected.

Deep Percolation

The final independent term, G_r , of Equation 3.16 represents the rate of deep percolation. Percolation is simply the movement of water through the soil. Deep percolation is defined as water movement through the soil from the plant root zone to the underlying groundwater basin. The dominant potential forces causing water to percolate downward from the plant root zone are gravity and capillary. Water is removed quickly by gravity from a saturated soil under normal drainage conditions. Thus, the rate of deep percolation, G_r , is most rapid immediately after irrigation when the gravity force dominates, and decreases constantly, continuing at slower rates through the unsaturated conditions. Because the capillary potential applies through all moisture regimes, deep percolation continues, though at low rates, even when the moisture content of the soil is less than field capacity (Willardson and Pope, 1963).

Because of a lack of data in the study area regarding deep percolation rates in the unsaturated state, and in order to simplify the model, the assumption was made that deep percolation occurs only when the available soil moisture is at its capacity level. In most cases, this assumption causes only slight deviation from prototype conditions. Thus, for this model, the deep percolation rate is expressed as:

$$G_r = F_r - ET_{cr}, [M_s(t) = M_{cs}] \quad (3.27)$$

$$G_r = 0, [M_s(t) < M_{cs}] \quad (3.28)$$

in which all terms are as previously defined.

River Outflow

Using the continuity of mass principle (Equation 2.1) the hydrologic balance is maintained by properly accounting for the quantities of flow

at various points within the system. The appropriate translation or routing of inflow water through the system in relationship to the chronological abstractions and additions occurring in space and time concentrates the water at the outlet point as both surface and subsurface outflow. As mentioned earlier, active network delays on the computer simulate the long transport time necessary for groundwater inflows and deep percolating waters to be routed to the outflow gaging station.

Thus, the total rate of water outflow from a subbasin is obtained through the summation of various quantities as follows:

$$Q_o = Q_{is} - W_{tr} + OF_r + Q_{ob} - Q_e \quad (3.29)$$

in which

- Q_o = total rate of outflow from the system
- Q_{is} = rate of total surface inflow to the subbasin including both measured and unmeasured flows
- W_{tr} = total rate at which water is diverted from the stream or reservoir
- OF_r = total of overland flow and interflow rates
- Q_{ob} = rate of outflow from the groundwater basin of routed deep percolating waters and subsurface inflows to the subbasin
- Q_e = rate of water diversions from surface sources for use outside the boundaries of the subbasin. Exports to other drainage basins fall within this category.

If subbasins are selected such that there exists no flow of subsurface water past the gaged outflow point, the hydrograph of surface outflow, Q_{so} , is given by Equation 3.29. This situation is assumed to exist at reservoir sites within the basin because of construction measures taken to eliminate subsurface flows under the dams which create the

reservoir. For this reason, whenever possible, subbasins were terminated at the outfall of a reservoir. These sites thus enabled a check to be made on groundwater inflow rates to the subbasin as predicted from verification studies involving models for one or more upstream subbasins.

For many subbasins the termination or outlet point was taken at a Geological Survey gaging station, and in several of these cases groundwater flow occurs in the streambed alluvium beneath the surface channel. For these basins, the total system outflow can be written as:

$$Q_{to} = Q_{so} + Q_{go} \dots \dots \dots (3.30)$$

in which

Q_{so} = rate of surface outflow from the subbasin

Q_{go} = rate of subsurface or groundwater outflow from the subbasin

Surface outflow rates, Q_{so} , can be compared to the recorded values, but subsurface outflow rates, Q_{go} , are unmeasured and must be predicted or estimated. In this study it was assumed that the subsurface outflow rates were directly proportional to the total outflow rates, and Q_{go} was therefore estimated by the following relationship:

$$Q_{go} = k_d Q_o \dots \dots \dots (3.31)$$

in which

k_d = a coefficient determined by model verification representing the percentage of total outflow which leaves the basin as subsurface flow.

Because of storage and permeability effects, fluctuations in groundwater flow rates tend to be much less extreme than in the case of surface flows. The value of k_d in Equation 3.31 was, therefore, not maintained as a constant, but was expressed as an inverse function of the surface flow rate, Q_{so} . During the spring runoff period, for example, the predicted increases in subsurface

outflow rate, Q_{go} , from Equation 3.31 were considerably less extreme than the increases in observed or computed surface flow rate, Q_{so} . Relationships expressing k_d as a function of Q_{so} were developed for each subbasin through the model verification process.

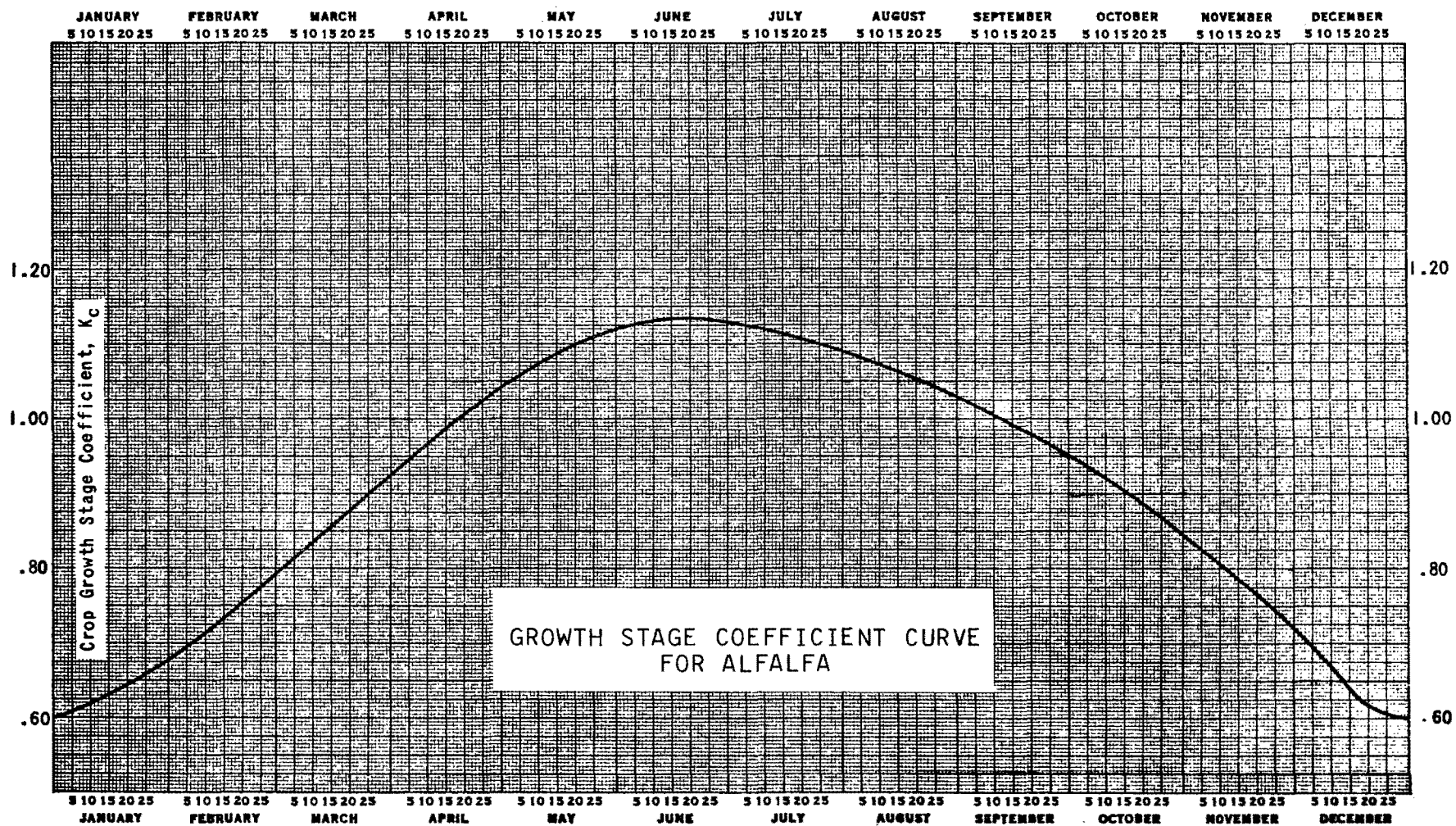


Figure 3.3. Crop growth stage coefficient curve for alfalfa. (Adapted from U. S. Soil Conservation Service Technical Release No. 21)

CHAPTER IV

THE COMPUTER MODEL

A computer model of a hydrologic system is produced by programming the mathematical relationships and logic functions of the hydrologic model as described in the previous chapter. The model does not directly simulate the real physical system, but is analogous to the prototype, because both systems are described by the same mathematical relationships. A mathematical function which describes a basic process, such as evapotranspiration, is applicable to many different hydrologic systems. The simulation program developed for the computer incorporates general equations of the various basic processes which occur within the system. The computer model, therefore, is free of the geometric restrictions which are encountered in simulation by means of network analyzers and physical models. The model is applied to a particular prototype system by establishing, through a verification procedure, appropriate constant values for the equations required by the system.

Electronic computers fall into one of three general classifications, namely analog, digital, and hybrid. The computing components of an analog computer execute the basic operations of addition, multiplication, function generation, and, most important in the study of dynamic or time variant systems, high-speed integration. By connecting computing components through a program "patch panel," it is possible to form an electronic model of a differential equation or a series of differential equations which describe the dynamic performance or operation of a physical system.

The general-purpose digital computer processes information which is reported by combinations of discrete or instructive data, as compared with the analog computer which operates on continuous data. While the analog computer is a "parallel" system

in which all problem variables are operated on simultaneously, the digital computer is basically a "sequential" system performing step by step operations at high speed.

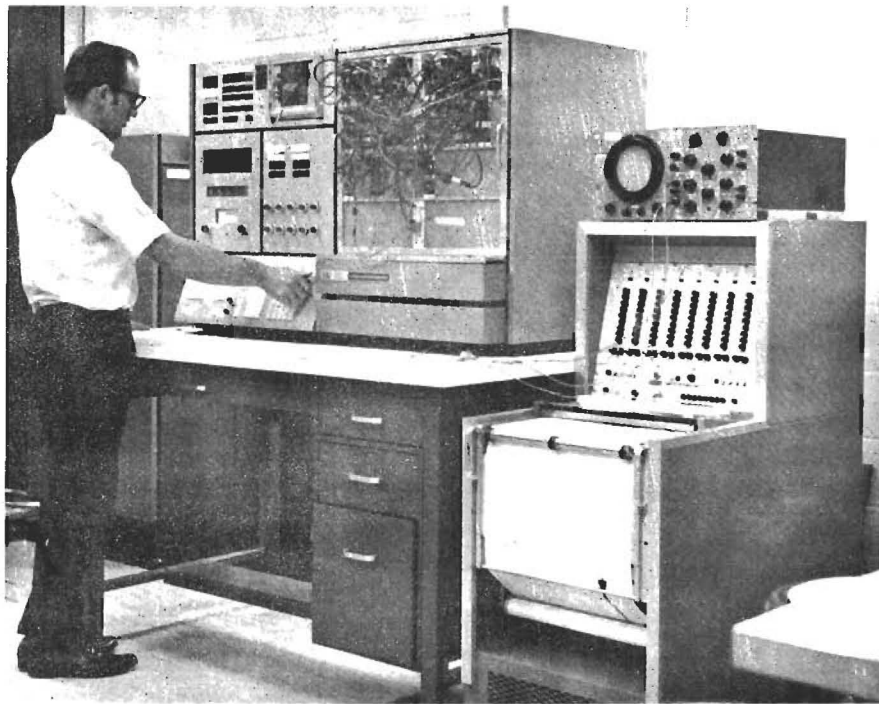
The digital computer is useful in processing large quantities of data or in solving complex mathematical problems which can be converted to a large number of simple arithmetic operations by the operator or by the computer. The digital computer can perform sequences of arithmetic and logical operations, not only on data, but also in its own program, and is, therefore, an immensely powerful device for processing or manipulating large amounts of discrete data and for performing precise arithmetic calculations at high speed.

In analog simulation, the operator communicates with, or controls, the simulation by means of hardware controls, while viewing the continuous problem solution. The digital computer programmer communicates with the computer primarily through "software" or programming languages. The design of software has become of equal or greater significance than hardware design. The development of "higher-order" or problem-oriented languages, in which one programming statement triggers a large number of sequential computer operations, has helped to simplify the interface problem between the user and the digital system.

The hybrid computer combines the memory and logic capabilities of the digital with the high speed and nonlinear solution capabilities of the analog. In addition, the high speed iterative solutions and graphic display which are characteristics of the hybrid computer provide close interaction between the hydrologist and the model. These features make the hybrid a very powerful computer in the development and verification of simulation



The console of the digital unit.



A view of the analog unit showing the servo-set pots, digital voltmeter, program board, and output devices.

Figure 4.1. Two views of the hybrid computer facility at the Utah Water Research Laboratory.

models. Two views of the Electronic Associates Incorporated (EAI) 590 hybrid computer available at the Utah Water Research Laboratory are shown by Figure 4.1.

The computer simulation model of the Bear River hydrologic system was programmed on the hybrid computer. The digital portion of the model was coded in FORTRAN IV (EAI subset), and the analog portion was programmed for the EAI 580 computer. Because an analog computer operates within specific voltage limits, in this case ± 10 volts, it was necessary to scale the analog component of the model such that these limits were not exceeded. The basic data were input to the digital computer, which processed and controlled the operation of the hydrologic mass balance model programmed on the analog component of the hybrid computer. Monthly values of input and output data were printed as stipulated in the program by the on-line printer as the simulation proceeded. Graphical output at various points within the model was obtained by connecting the x-y plotter to the appropriate terminals on the analog patch-board.

As mentioned earlier, the computer program is general in nature, and is applied to a particular prototype system by a verification procedure.

A general view of the program control structure is shown by Figure 4.2. As illustrated by this figure, the program contains several subroutines, each of which is controlled by the main program, labeled OPVER. Program OPVER performs the following two functions: (1) establishes the various options available for performing the hydrologic simulation, and (2) controls the operation of the modified pattern search for calibrating the model for a particular subbasin. The five options available through OPVER are as follows:

1. Simulation of an entire system of sub-basins without exiting from the simulation subroutine, HYDSM.

2. Input only basic data which are considered to be common for all subbasins that may be subsequently run.
3. Input and operate with data for a particular subbasin. Option 2 must have been previously selected.
4. Rerun the last simulation performed. Options 2 and 3 must have been previously selected.
5. Perform pattern search on subbasin data presently in memory. Options 2 and 3 must have been previously specified.

The subroutine interaction is illustrated by Figure 4.3. Program OPVER establishes the entry and exit conditions for HYDSM, which in turn calls the particular subroutines needed to perform the operations specified by OPVER. OPVER also calls the analog potentiometer subroutine POTST without going through HYDSM during the pattern search operation. A listing of the digital program, a flow chart of the analog program, flow charts for OPVER and the primary subroutines, program notations, and general instructions for use of the model are given in Appendix B.

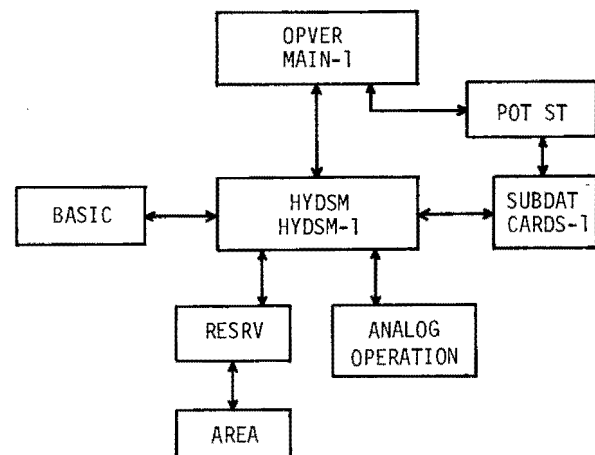


Figure 4.2. General view of the program control structure.

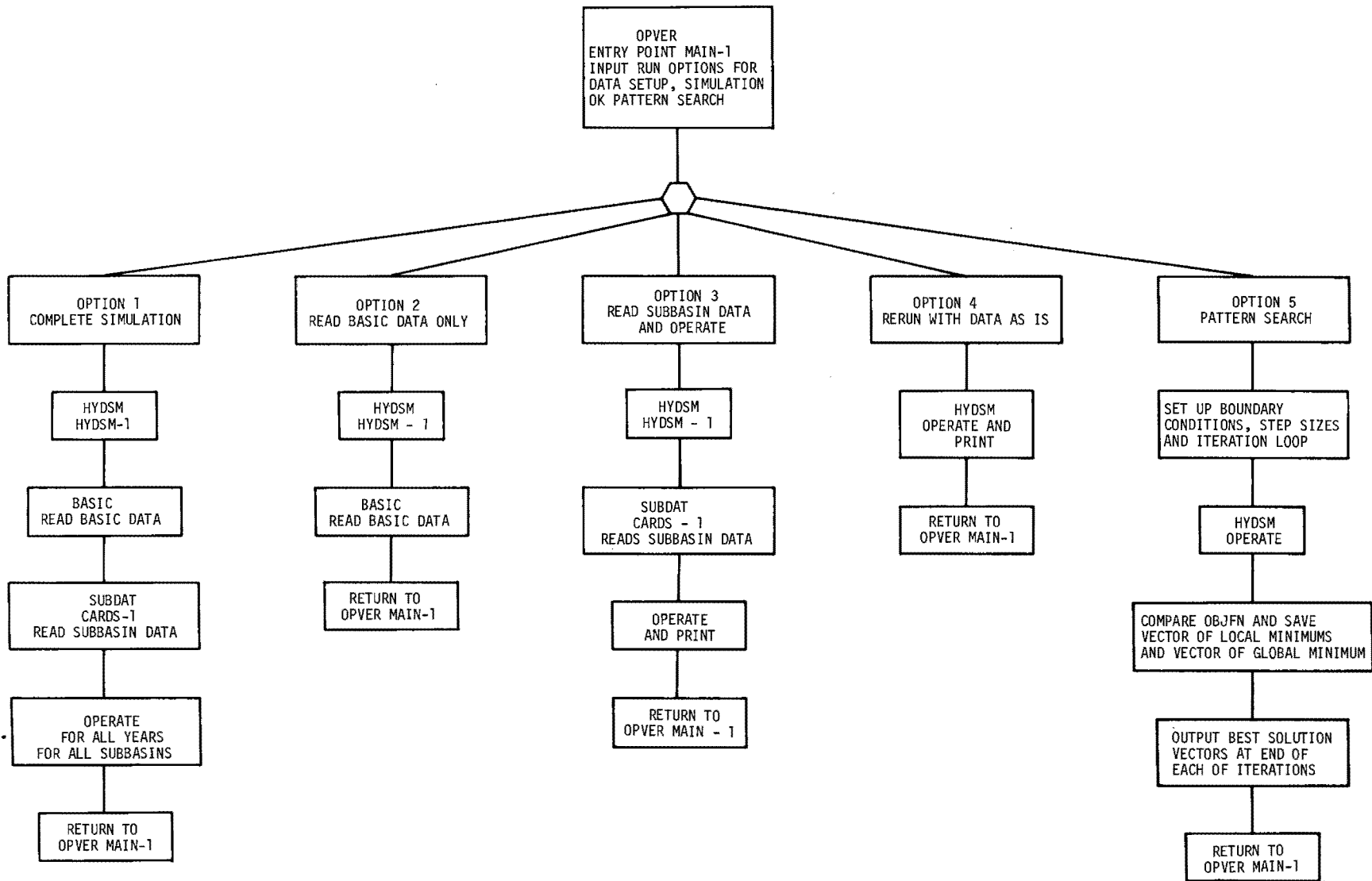


Figure 4.3. A flow diagram of the subroutine interaction for program OPVER.

CHAPTER V
APPLICATION OF THE HYDROLOGIC MODEL
TO THE BEAR RIVER BASIN

Verification

The general hydrologic model discussed in the previous chapter is applied to a particular basin through a verification procedure whereby the values of certain model parameters are established for a particular prototype system. Verification of a simulation model is performed in two steps, namely calibration, or system identification, and testing of the model. Data from the prototype system are required in both phases of the verification process. Model calibration involves adjustment of the model parameters until a close fit is achieved between observed and computed output functions. It therefore follows that the accuracy of the model cannot exceed that provided by the historical data from the prototype system.

Evaluation of the model parameters can follow any desired pattern, whether it be random or specified. In this study, each unknown system coefficient is assigned an initial value, an upper and lower bounds, and the number of increments to cover the range. The first selected variable is varied through the specified range while all other variables remain at their initial value. The values of the objective function (measure of error) for each value of the variable are printed, and the value which produced the minimum is stored. After completion of the runs for the first variable, the variable is reset to the initial value and the second variable is taken through the same procedure. After all coefficients have been varied, the set of values which produced each local minimum is run and the resultant objective function value is compared with the smallest attained in all previous runs. The vector which produced the minimum objective function value is selected as the initial

vector for the next phase and the process is repeated until a coefficient vector is found which produces a reasonable correspondence between computed and observed outflows. The algorithm used to implement the many trials required for model calibration is included in Appendix B as part of the digital computer source program for the model.

It should be noted that the choice of the variable vector for each phase is based on the judgment and experience of the programmer. However, selection of all variable vectors following the first choice is tempered by the experience gained during the first phase and subsequent phases of the procedure. Thus, model verification effectively uses all previous experience, including that gained during the verification procedure.

Calibration of the model of this study was based on three years of prototype data. Model output was compared to measured output by computing the sum of the squared deviations, which became the objective function for the pattern search procedure described previously. The final parameter vector that was selected to represent the system was that which minimized the objective function in the calibration procedure. The three years of data required 36 monthly solutions of the simultaneous system of equations in terms of water quantities as a function of time. Ideally, calibration data should cover a wide range of input values, such as those corresponding to a dry, a wet, and an average year.

Comparisons between the observed and computed output values from the calibrated model are shown by Figures 5.1 through 5.9. The verified model coefficients are shown in detail in Appendix C. When values of the model coefficients which produce acceptable reproductions of the output

function from a prototype system have been established, the model is said to be calibrated for that system. It is then assumed that the model is capable of predicting realistic system outputs corresponding to various input functions and system parameters.

Sensitivity Analysis

A sensitivity analysis is performed by changing one system variable while holding the remaining variables constant and noting the changes in the model output functions. If small changes in a particular system parameter induce large changes in the output or response function, the system is said to be sensitive to that parameter. Thus, through sensitivity analyses it is possible to establish the relative importance with respect to system response of various system processes and input functions. This kind of information is useful from the standpoint of system management, system modeling, and the assignment of priorities in the collection of field data.

The computer model that was developed under this study performs a sensitivity analysis during calibration. The final phase of the model calibration procedure sets out the most meaningful sensitivity analysis since at this stage all parameters are near their final values. Careful study of the outputs from the verification procedure in Table 5.1 reveals the results of the sensitivity analysis. For example, a seven-fold increase in variable 11 reduced the objective function by about 40 percent, while increasing variable two by something less than double produced a four-fold change in the objective function. On the other hand, a four-fold increase in parameter 13 caused very little change in the objective function. Therefore, variable 13 would be given a low priority for more thorough scrutinization. However, variable two would be given a high priority for additional study. Table

5.1 shows the sensitivity of the variables for the Evanston subbasin. Similar analyses were made for each subbasin of the Bear River basin. Table 5.1 also indicates the gradient of the objective function for each variable parameter, or the rate of change of the objective function per unit change in any variable. This information is useful for establishing parameter values which minimize the objective function, and for estimating the sensitivity of this function to changes in the variable parameters. For each phase of the calibration procedure, initial values of the gradient for each variable are set equal to zero.

Table 5.2 is a printout from the computer program and represents a phase of the calibration process. The table presents the variable parameter number, the terminal values at each end of the range, the increment by which each parameter is changed during the calibration procedure, and the number of runs needed to cover the range. In this case, the initial and final vectors are almost identical because they represent the last phase of the verification procedure. Previous phases in the calibration procedure would show more differences between corresponding parameter values in the initial and final vectors.

Management Opportunities

Opportunities for management of water in the Bear River basin are widely varied and range from a change in cropping patterns to water storage and export. Actual implementation of a management scheme will depend on benefits gained as compared to the costs of implementation. The simulation model developed under this study does not make comparisons of benefits and costs, but does predict changes in the system output associated with given management alternatives. The management schemes tested in this study do not begin to cover the possible combinations, but do demonstrate the capability of

Table 5.1. Sensitivity of Evanston subbasin variables.

	6.45	.75	.900	.380	1.000	.000	.700	.030	.000	32.000	24.000
	10.00	7.00	11.00	.20	.00	.00	.00	.00	.00	2.50	2.50
P	L	PAR		OBJ		OSA		GRAD			
1	1	.600		7.63027		.60905		.00000			
1	2	.700		7.01659		.50651		-6.13677			
1	3	.800		6.72995		.48210		-2.86648			
1	4	.900		6.54957		.57975		-1.80375			
2	1	.300		15.25176		7.05924		.00000			
2	2	.340		9.33559		2.53776		-147.90411			
2	3	.380		6.59475		.57975		-68.52113			
2	4	.420		8.31256		.30632		42.94525			
2	5	.460		14.22400		-1.53450		147.78604			
2	6	.500		24.27461		-2.69660		251.26504			
3	1	1.000		6.46163		.59928		.00000			
4	1	.000		6.43422		1.47819		.00000			
5	1	.200		11.90100		-3.66828		.00000			
5	2	.300		9.92734		-2.69660		-19.73664			
5	3	.400		8.45101		-1.55891		-14.76330			
5	4	.500		7.28981		-.72893		-11.61198			
5	5	.600		6.66571		.39421		-6.24101			
5	6	.700		6.47435		1.44889		-1.91360			
6	1	.020		6.24164		-1.55891		.00000			
6	2	.030		6.42178		1.47819		18.01357			
6	3	.040		7.97232		4.49089		155.05401			
6	4	.050		10.71584		7.38151		274.35217			
6	5	.060		15.00296		10.44792		428.71179			
6	6	.070		20.46119		13.54362		545.82373			
7	1	.000		6.47415		1.45866		.00000			
8	1	31.000		6.39105		1.42936		.00000			
8	2	31.500		6.39207		1.41950		.00204			
8	3	32.000		6.38694		1.43913		-.01025			
8	4	32.500		6.45121		1.37077		.12852			
8	5	33.000		6.34556		1.38053		-.21129			
9	1	23.000		8.45782		1.48307		.00000			
9	2	23.500		7.19685		1.42446		-2.52193			
9	3	24.000		6.44771		1.58073		-1.49828			
9	4	24.500		8.79396		1.55143		4.69251			
9	5	25.000		15.29298		1.75651		12.99803			
9	6	25.500		19.65886		1.70768		8.73176			
9	7	26.000		19.78175		.97526		.24578			
10	1	10.000		6.48482		.80436		.00000			
11	1	1.000		10.98001		-.11360		.00000			
11	2	2.000		9.36678		.18913		-1.61322			
11	3	3.000		9.94035		1.42448		.57357			
11	4	4.000		8.32566		1.47819		-1.61469			
11	5	5.000		6.94916		.46257		-1.37650			
11	6	6.000		6.54289		1.40983		-.40626			
11	7	7.000		6.52198		.71159		-.02090			
12	1	8.000		7.69265		4.59342		.00000			
12	2	9.000		7.16197		2.76725		-.53068			
12	3	10.000		6.59547		2.42057		-.46650			
12	4	11.000		6.42354		1.61003		-.27492			
12	5	12.000		6.95988		-.17219		.53933			
13	1	.000		6.55159		-.67024		.00000			
13	2	.100		6.37926		.74577		-2.72316			
13	3	.200		6.51555		.75066		1.36284			
13	4	.300		6.58709		1.49284		.71543			
13	5	.400		6.76384		2.20085		1.76745			
14	1	.000		6.60894		.91178		.00000			
15	1	.000		6.51977		.95085		.00000			
16	1	.000		6.37089		1.94206		.00000			
17	1	.000		6.50541		1.74674		.00000			
18	1	.000		6.39482		1.70260		.00000			
19	1	.000		6.37797		1.71745		.00000			
20	1	2.500		6.62894		.84831		.00000			
21	1	2.000		6.81623		.86784		.00000			
21	2	2.500		6.64224		1.28288		-.34798			
21	3	3.000		6.63550		1.46354		-.01349			
21	4	3.500		6.71831		2.23991		.16563			
21	5	4.000		7.09720		3.07487		.75776			

Table 5.2. Computer printout showing summary of calibration process.

PR	NP	PH	PL	XIN	DD
1	3	.900	.600	.900	.100
2	5	.500	.300	.380	.040
3	1	1.000	1.000	1.000	.000
4	1	.000	.000	.000	.000
5	5	.700	.200	.700	.100
6	5	.070	.020	.030	.010
7	1	.000	.000	.000	.000
8	4	33.000	31.000	32.000	.500
9	6	26.000	23.000	24.000	.500
10	1	10.000	10.000	10.000	.000
11	6	7.000	1.000	7.000	1.000
12	4	12.000	8.000	11.000	1.000
13	4	.400	.000	.200	.100
14	1	.000	.000	.000	.000
15	1	.000	.000	.000	.000
16	1	.000	.000	.000	.000
17	1	.000	.000	.000	.000
18	1	.000	.000	.000	.000
19	1	.000	.000	.000	.000
20	1	2.500	2.500	2.500	.000
21	4	4.000	2.000	2.500	.500

XIN

I		
1	.900	.900
2	.380	.380
3	1.000	1.000
4	.000	.000
5	.700	.700
6	.030	.030
7	.000	.000
8	32.000	33.000
9	24.000	24.000
10	10.000	10.000
11	7.000	7.000
12	11.000	11.000
13	.200	.200
14	.000	.000
15	.000	.000
16	.000	.000
17	.000	.000
18	.000	.000
19	.000	.000
20	2.500	2.500
21	2.500	2.500

the model to rapidly test many possible schemes. It is again emphasized that a simulation model does not of itself produce an optimum solution in terms of management objectives. The technique does, however, facilitate a rapid evaluation of many possible alternatives. An analytical optimizing procedure, used in conjunction with a simulation model, could produce system optimization in terms of a specific objective function.

The ability of the model to predict outflow characteristics under various management conditions is demonstrated for the Evanston subbasin. The predicted total annual outflows under actual conditions for 1954, 1955, and 1956 are given in Appendix C as being 72,183; 92,544; and 150,918 acre-feet, respectively. The computed outflow hydrograph on a mean monthly basis is shown by Figure 5.1. Studies were then conducted to investigate the changes induced in this hydrograph by three entirely different sets of assumed conditions within the subbasin.

Case 1

Conditions were changed in the model to represent the removal of all phreatophytes from the subbasin. In addition, it was assumed that sufficient irrigation water was applied to support potential evapotranspiration rates and to maintain available soil moisture levels at no less than 2.5 inches. Precipitation, temperature, and stream inflow data for the years 1954, 1955, and 1956 were input to the model. The computed outflow hydrograph under these conditions for this three-year period is shown by Figure 5.10. The corresponding predicted total annual outflows from the subbasin are 93,341; 113,227; and 163,983 acre-feet, respectively, as shown in Appendix D, Evanston 1-1. The negative surface outflow quantities in this case indicate diversions of more irrigation water than was available in the river, and are, therefore, an indication of the storage required to satisfy the water requirements during the irrigation season. In the restricted case where irrigation diversions are limited to the water available in the stream, the computed total annual outflows are 111,313; 125,508; and 181,826 acre-feet for 1954, 1955, and 1956, respectively (Appendix D, Evanston 1-2). Corresponding mean monthly discharge values during this three-year period are shown by Figure 5.10. It is interesting to note that total outflow quantities under the

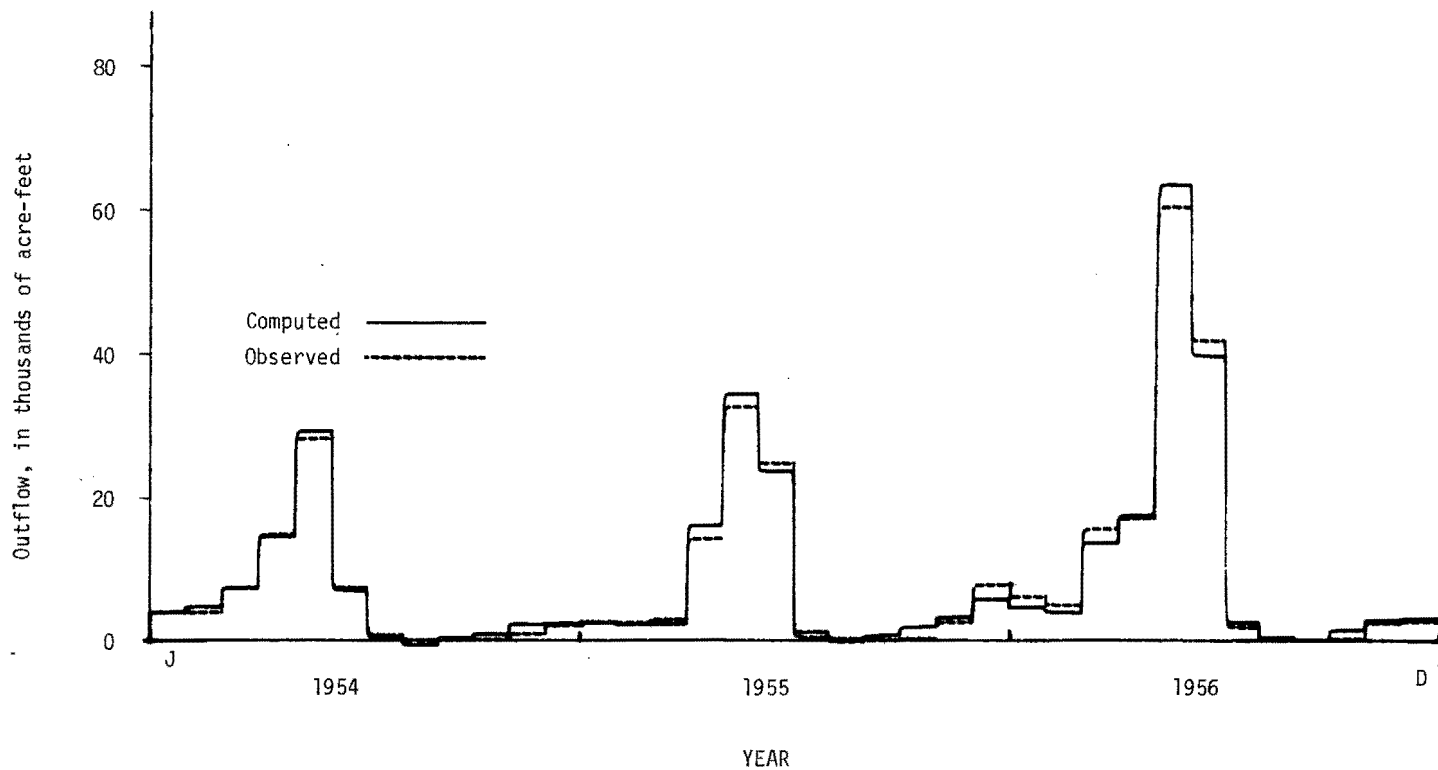


Figure 5.1. Computed and observed monthly outflow from Evanston subbasin 1954, 1955, and 1956.

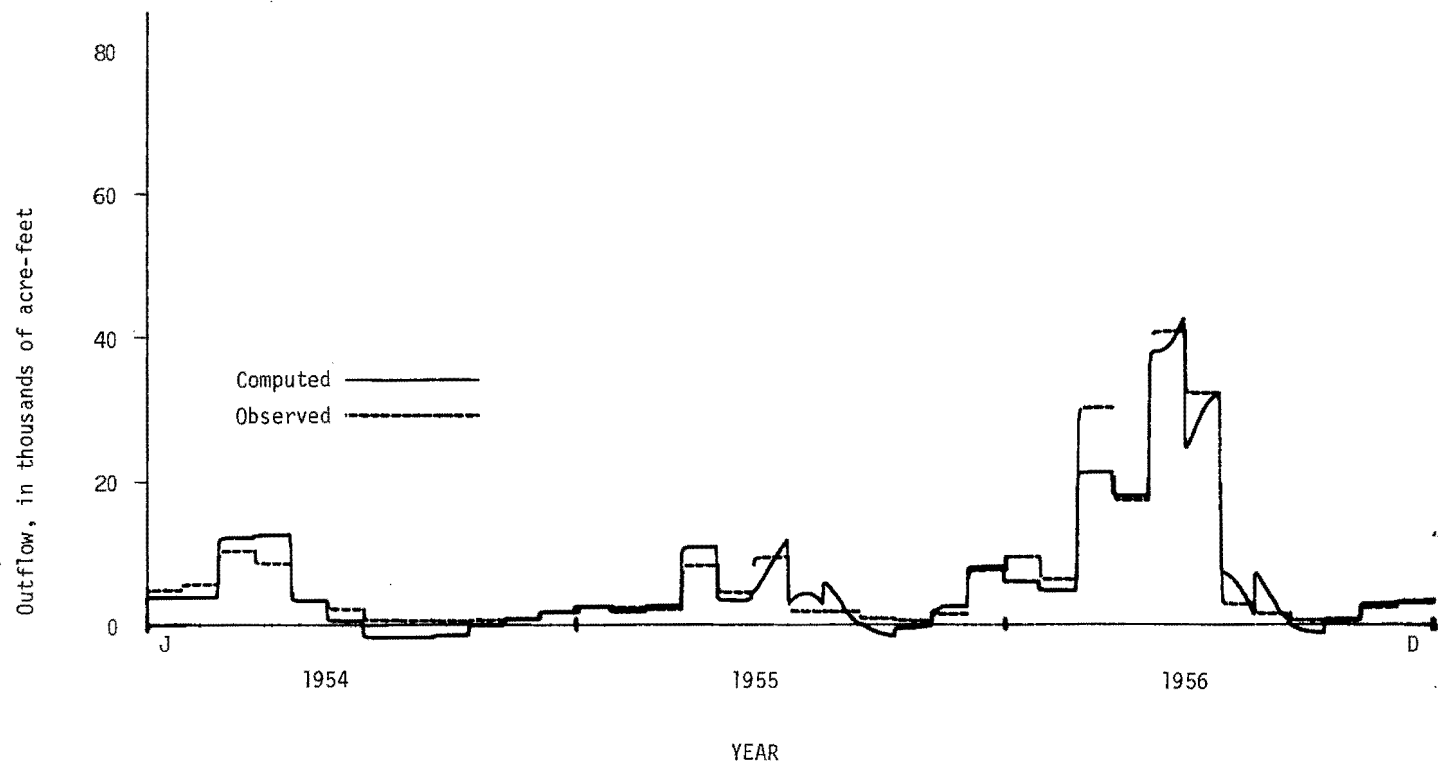


Figure 5.2. Computed and observed monthly outflow from Randolph subbasin 1954, 1955, and 1956.

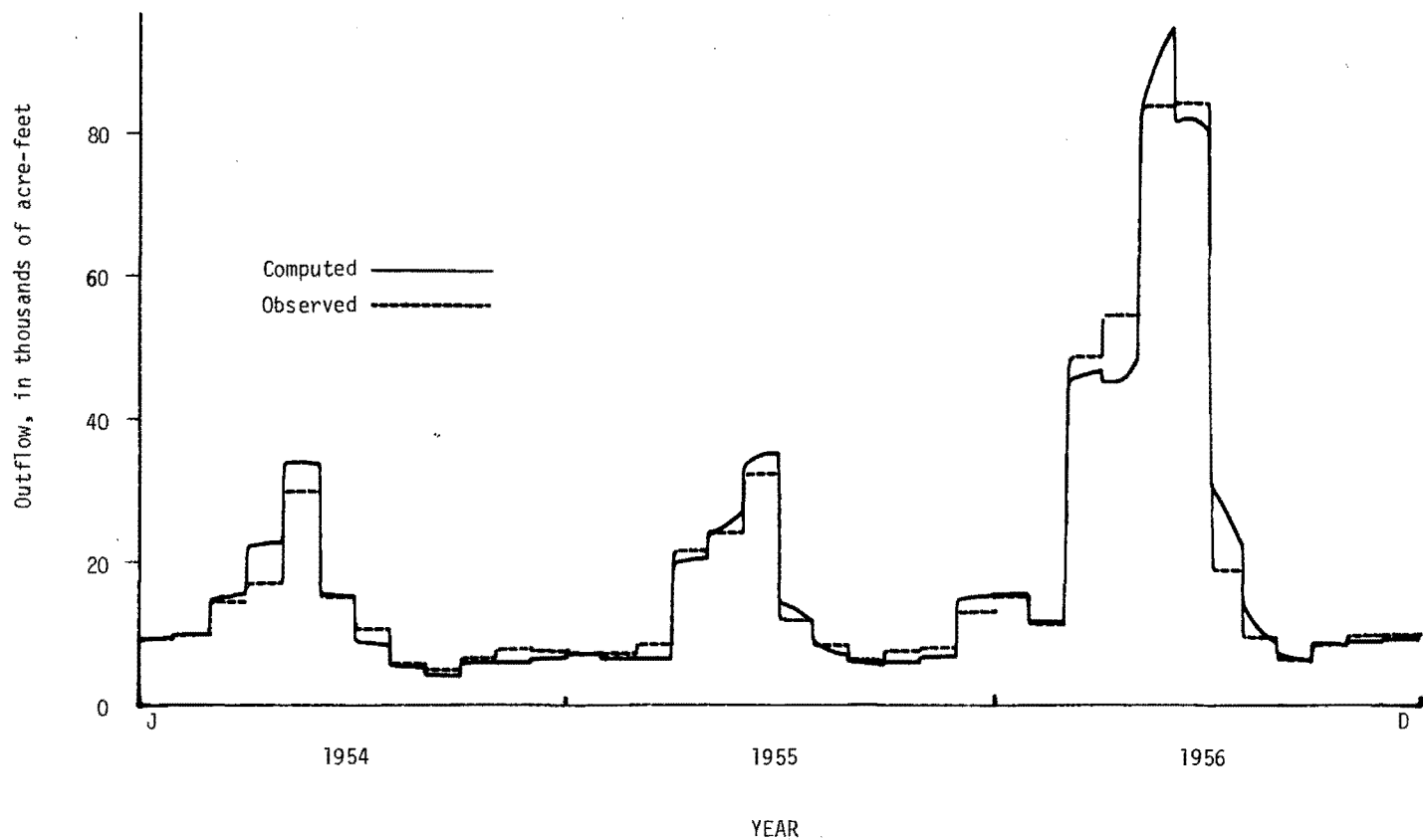


Figure 5.3. Computed and observed monthly outflow from Cokeville subbasin 1954, 1955, and 1956.

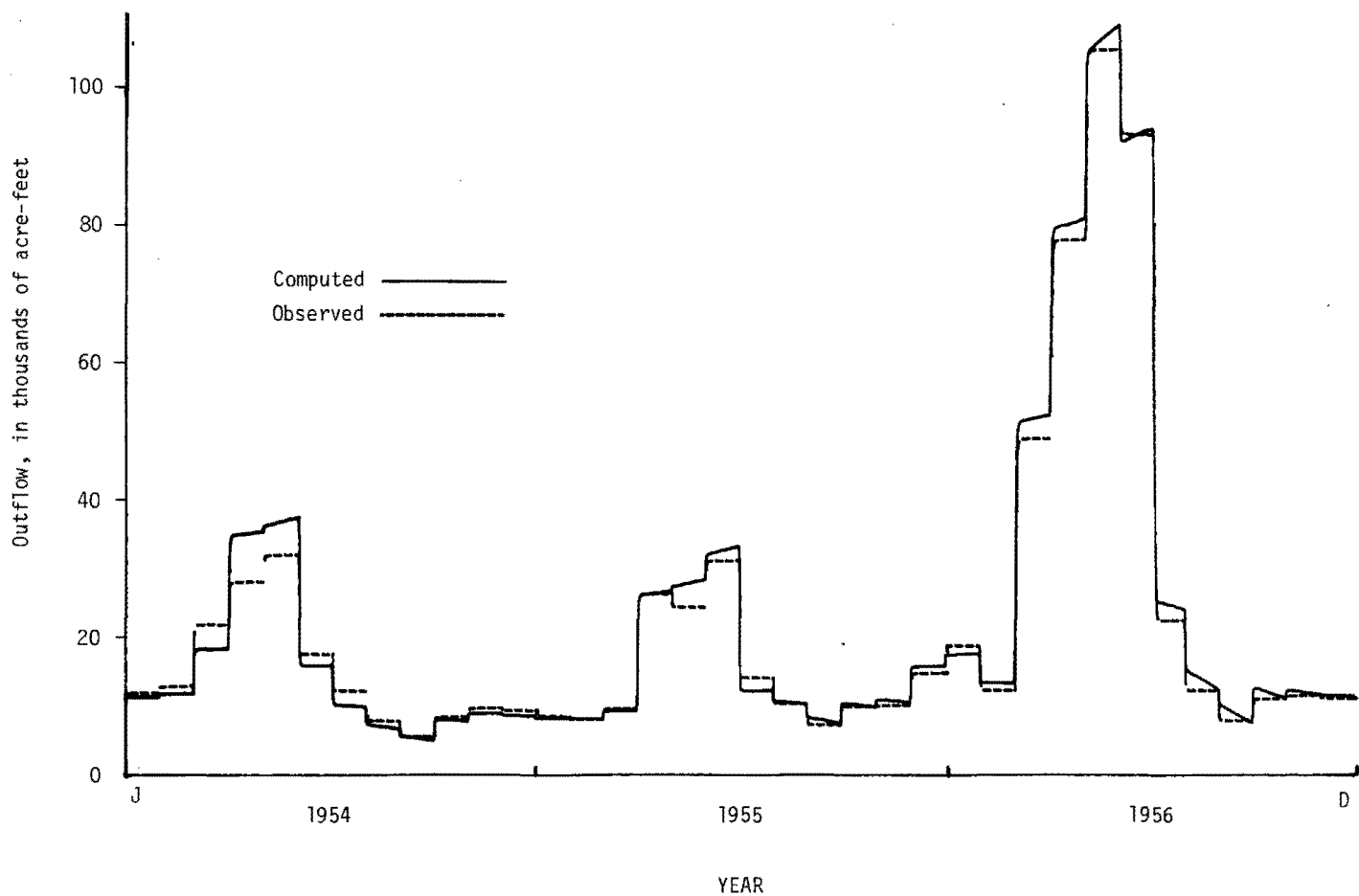


Figure 5.4. Computed and observed monthly outflow from Thomas Fork subbasin 1954, 1955, and 1956.

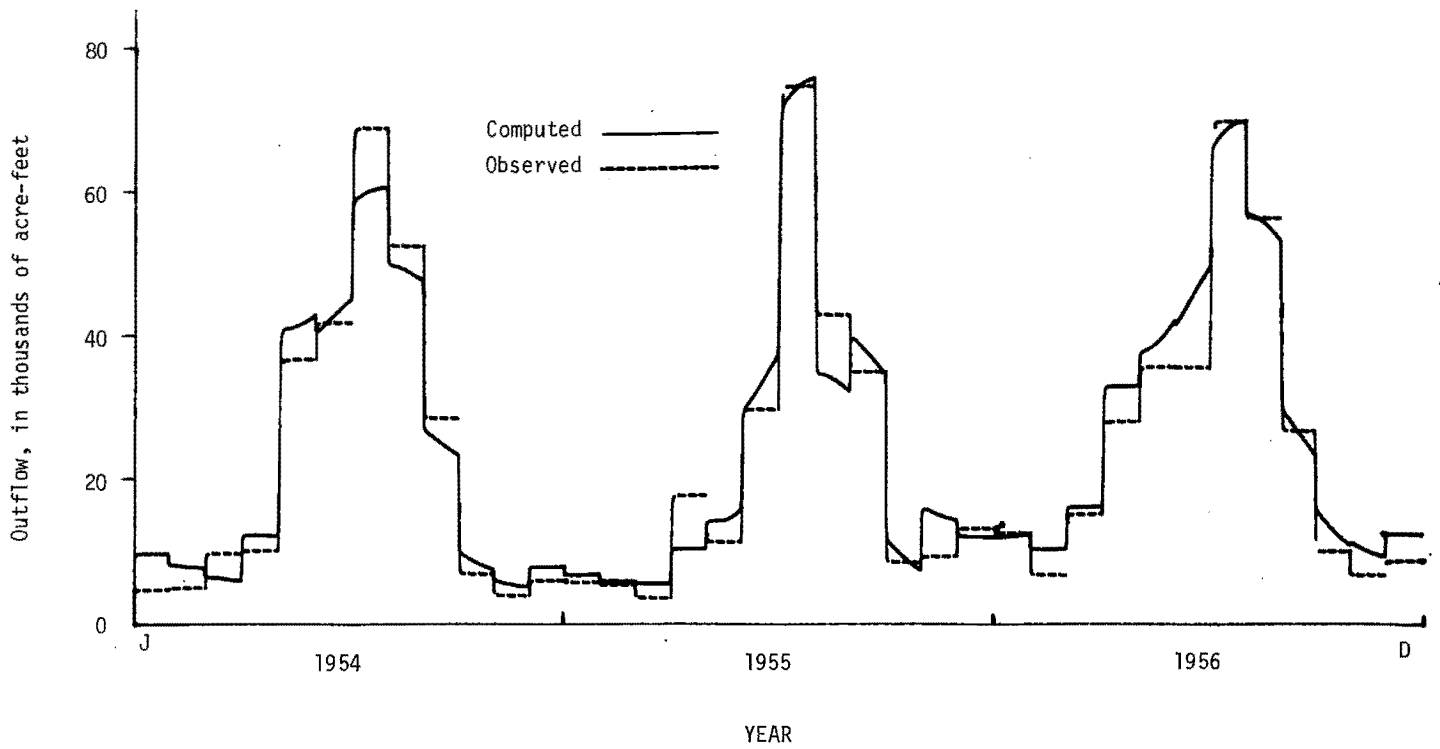


Figure 5.5. Computed and observed monthly outflow from Bear Lake subbasin 1954, 1955, and 1956.

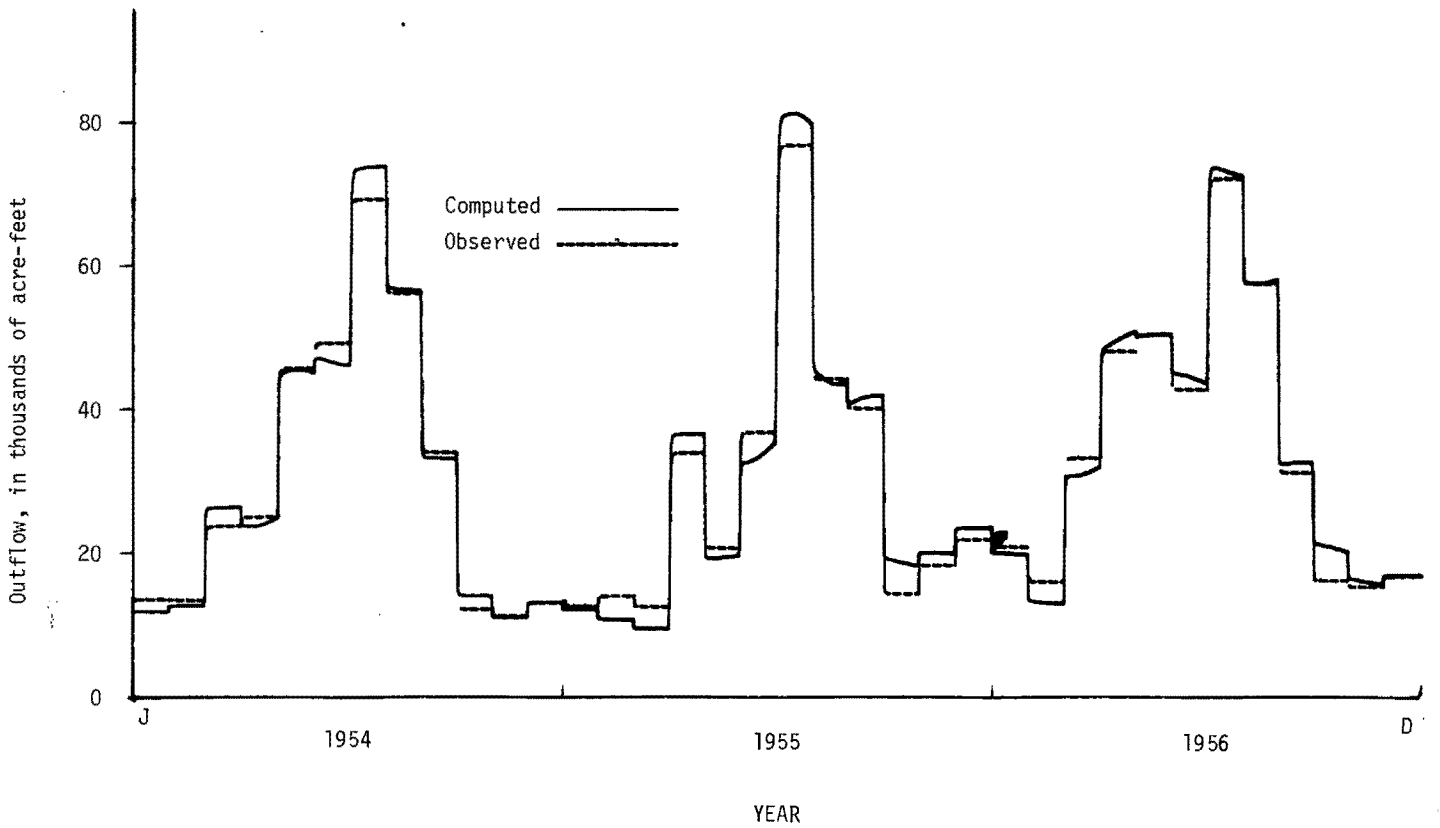


Figure 5.6. Computed and observed monthly outflow from Soda subbasin 1954, 1955, and 1956.

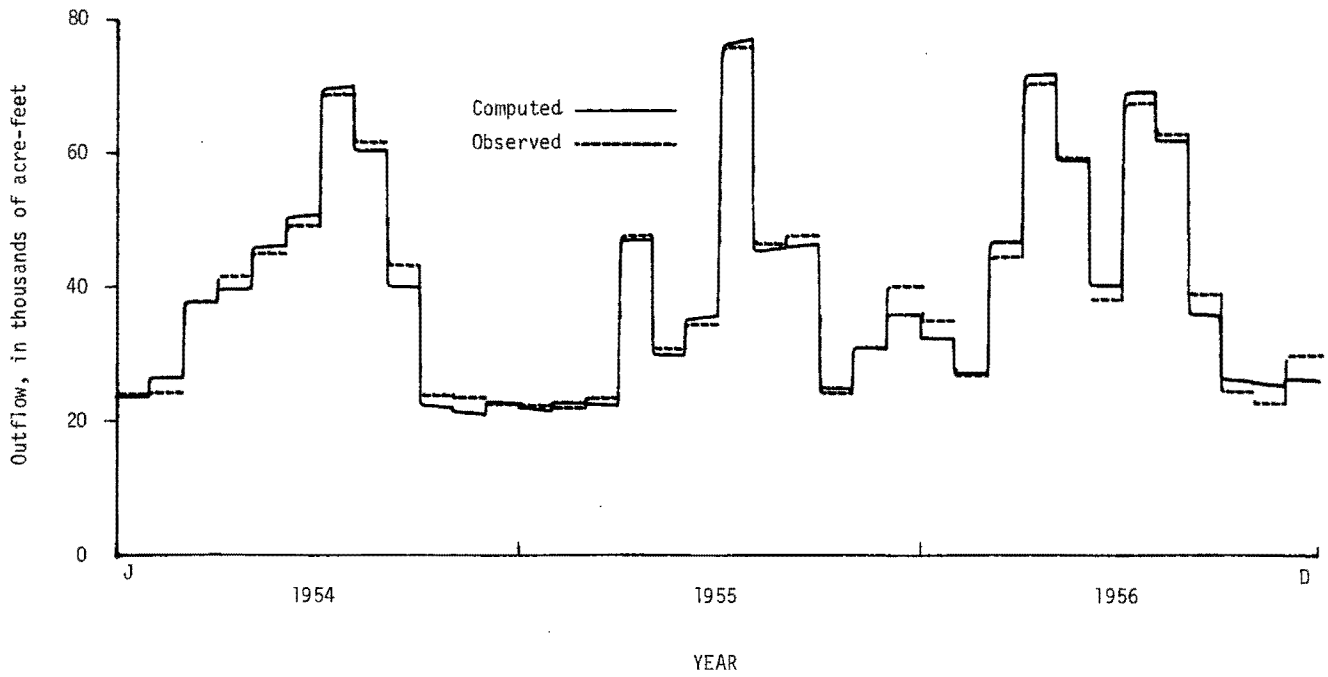


Figure 5.7. Computed and observed monthly outflow from Oneida subbasin 1954, 1955, and 1956.

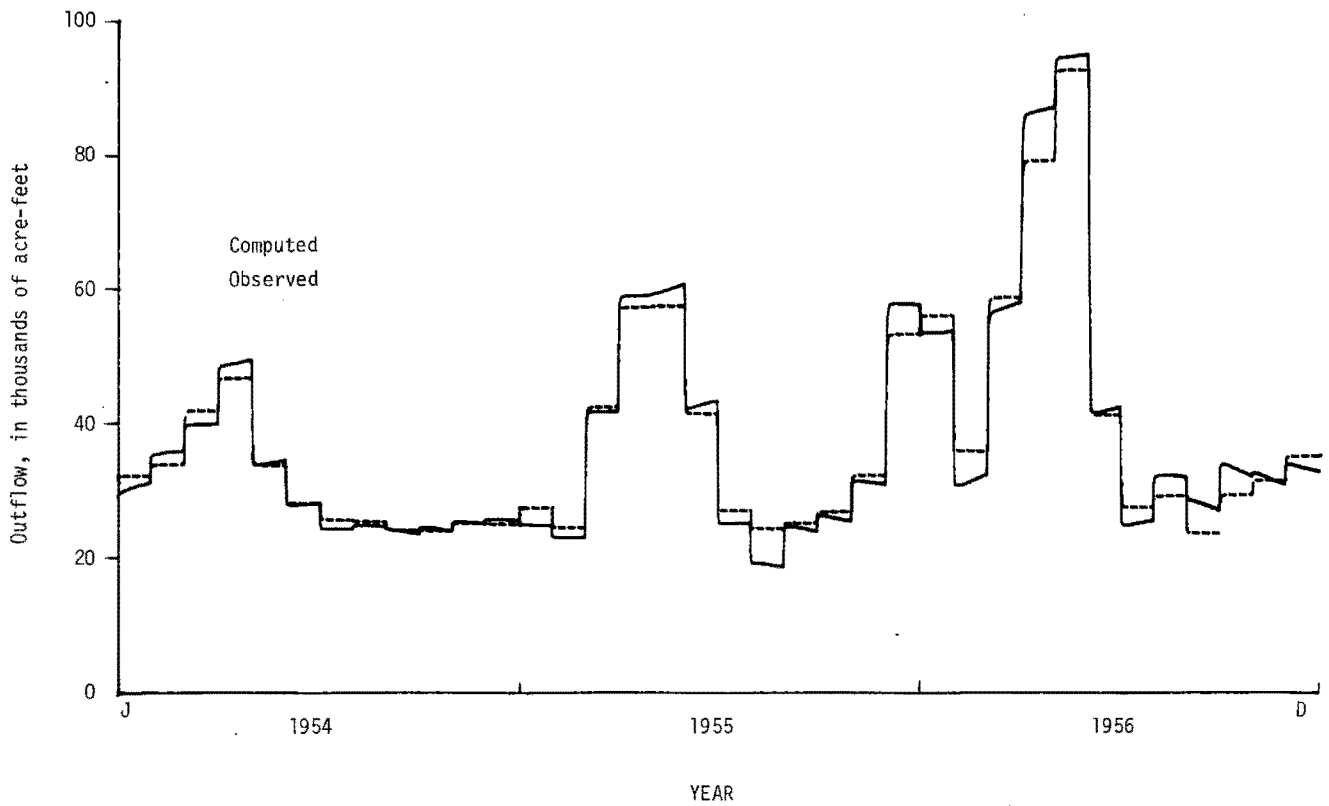


Figure 5.8. Computed and observed monthly outflow from Cache Valley subbasin 1954, 1955, and 1956.

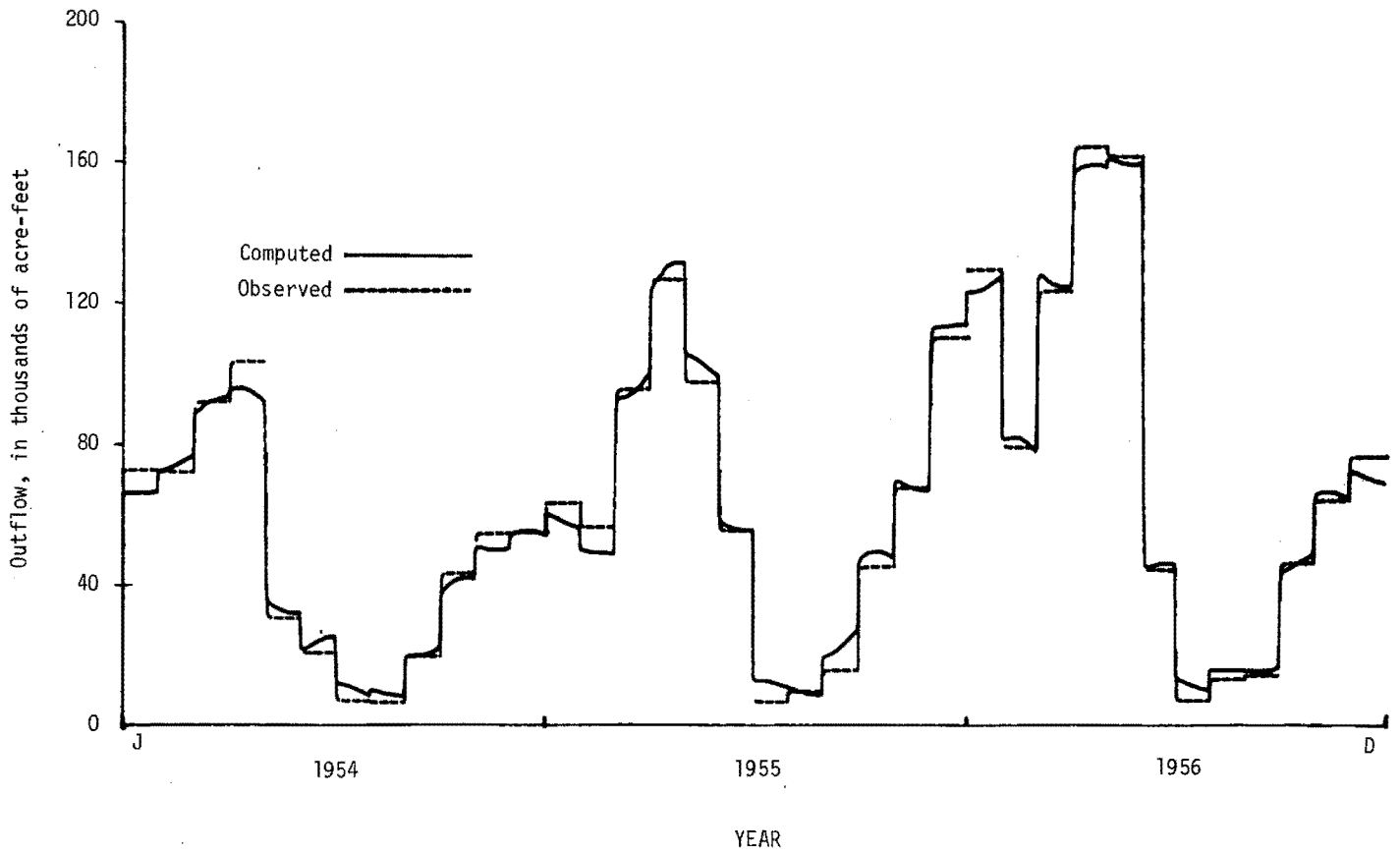


Figure 5.9. Computed and observed monthly outflow from Tremonton subbasin 1954, 1955, and 1956.

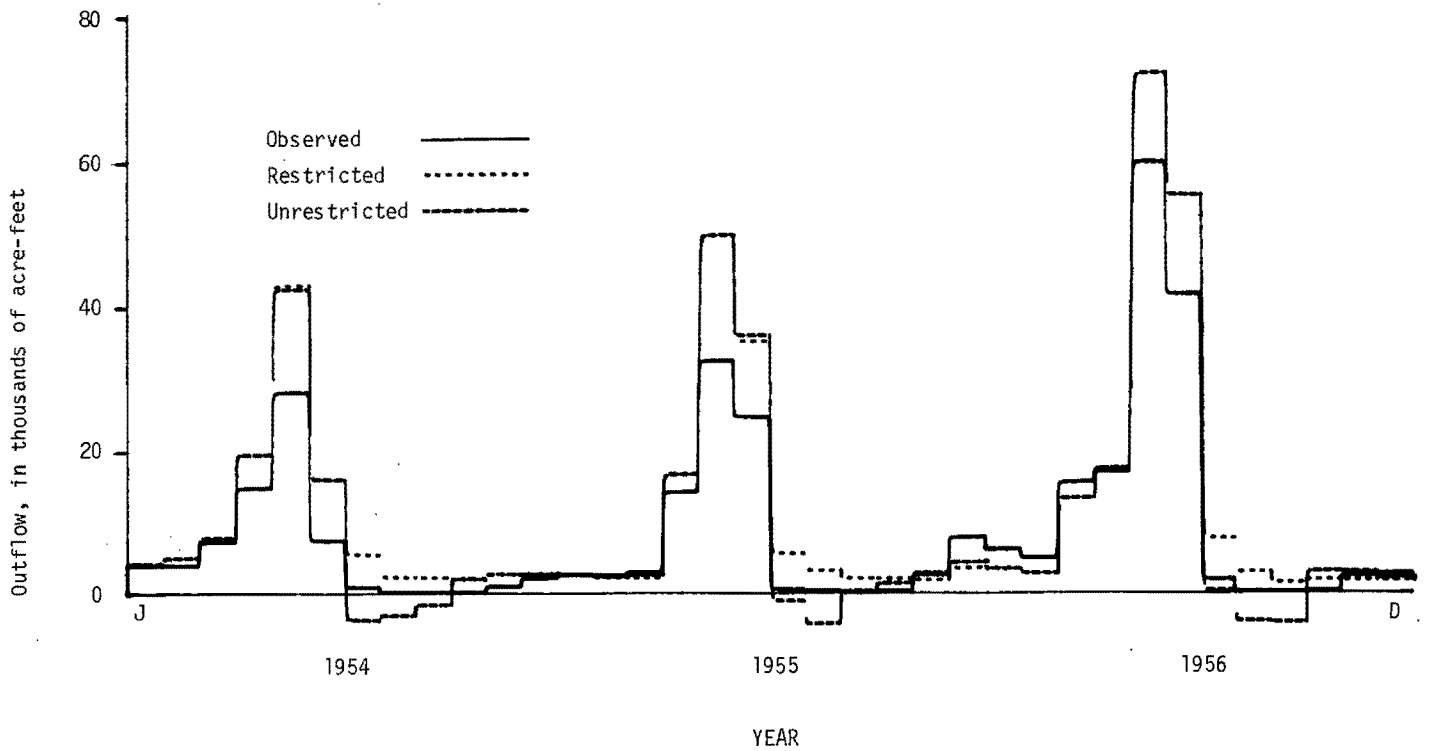


Figure 5.10. Management of Evanston subbasin, Case 1.

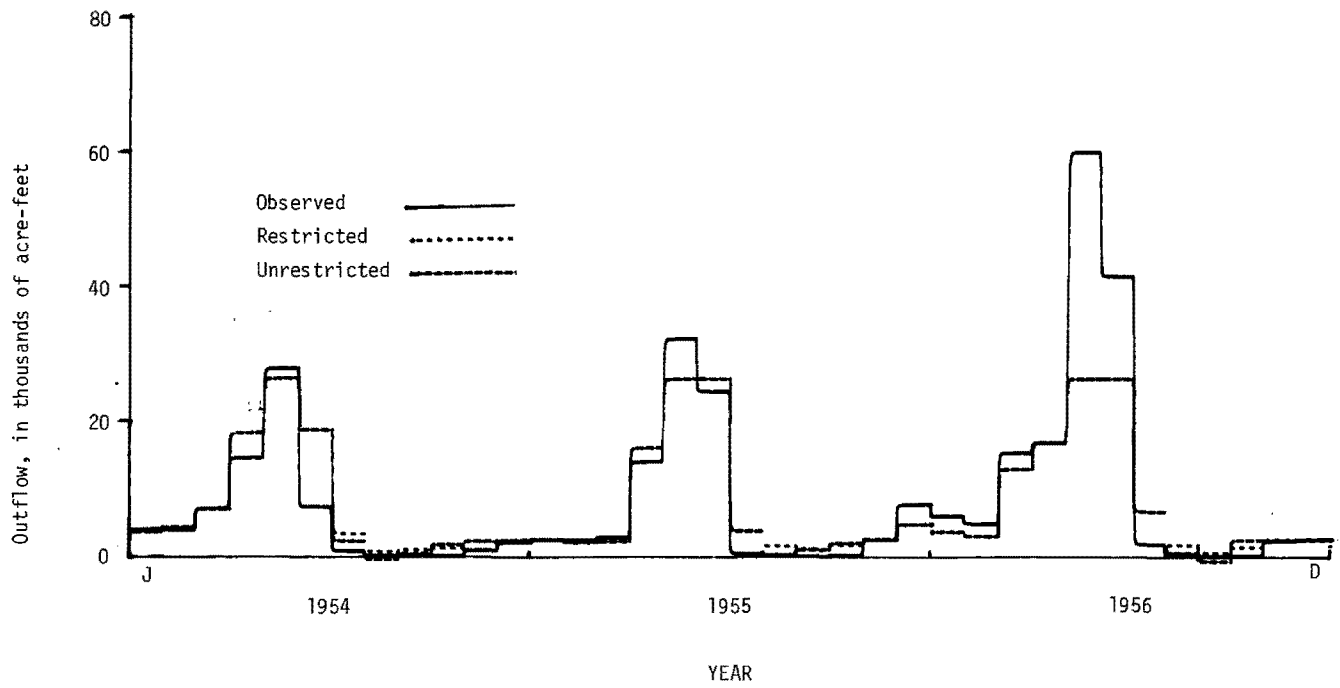


Figure 5.11. Management of Evanston subbasin, Case 2.

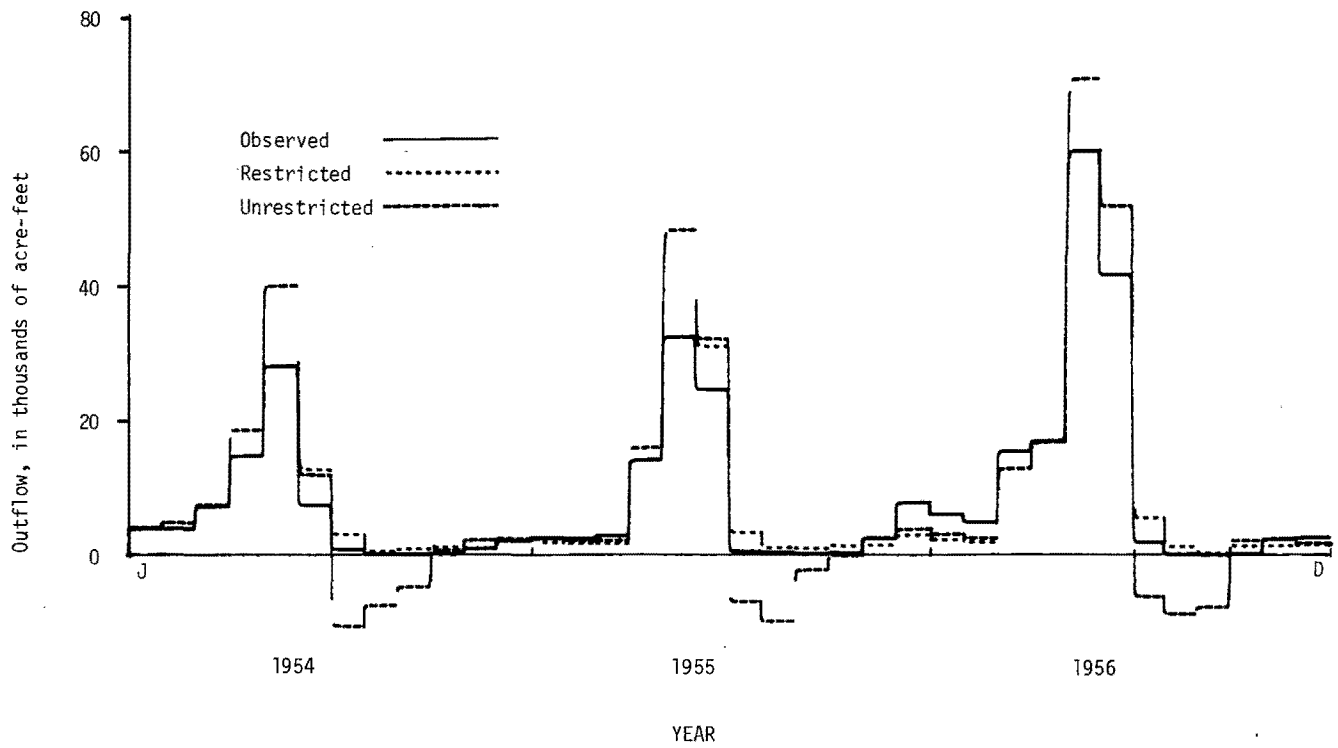


Figure 5.12. Management of Evanston subbasin, Case 3.

restricted water supply case appreciably exceed those of the unrestricted case. Under the conditions of restricted supply, water storage in the plant root zone was considerably reduced, and average evapotranspiration losses were approximately 20 percent below potential.

Cases 2 and 3

Under Case 2 crop acreages within the subbasin were reduced to 25 percent of the present area and phreatophytes were reduced to 75 percent. For Case 3 the cropland was increased to 125 percent of the present area while phreatophyte acreage was held at the present value. For both of these cases the model was operated under the two assumptions of first an unrestricted and then a restricted irrigation water supply. Model output functions for the four conditions described previously are given by Appendix D and Figures 5.11 and 5.12.

For the conditions of unrestricted irrigation water supply, the sum of the negative flows during

the irrigation period indicate storage requirements either by reservoir or in soil moisture. The operation of the model with 30 or more years of historical streamflow, precipitation, and temperature data would provide a realistic estimate of reservoir storage requirements to meet crop needs within the subbasin. A study of this nature would also facilitate the establishment and testing of suitable operating rules for any proposed reservoir or system of reservoirs within the subbasin. The effects of water export on reservoir operation could also be predicted.

The testing of various possible management alternatives for each subbasin within the Bear River model could be accomplished in the same manner as has been demonstrated for the Evanston subbasin. Using the model, management effects as reflected in the output functions of a particular subbasin may be traced throughout the entire Bear River basin.



CHAPTER VI

SUMMARY AND CONCLUSIONS

Increasing demands upon the available water resources of the nation have produced a need for the efficient utilization of these supplies. Related to good management practices is the evaluation of various alternatives in terms of their likely downstream effects on both water quantity and quality. Quantitative evaluation of these downstream consequences is difficult because of the complex and variable nature of the parameters which describe a hydrologic system. However, the advent of modern high-speed computers has made possible the application of simulation techniques to complex systems of this nature.

In this report, a general hydrologic model is proposed and is synthesized on a hybrid computer. The basis of the model is a fundamental and logical mathematical representation of the various hydrologic processes. Spatial definition is achieved by dividing the modeled area into specific space increments, or subbasins, for which average values of space variable model parameters are applied. Temporal resolution is obtained by selecting a specific time increment over which average values of time varying parameters are used. The ultimate in modeling would utilize continuous time and space definition. However, the practical limitations of this approach are obvious. The complexity of a model designed to represent a hydrologic system largely depends upon the magnitude of the time and spatial increments used in the model. In model development it is, therefore, necessary to select increments which are consistent with time, budget, and computer capability constraints, and at the same time provide sufficient resolution to consider the kinds of questions which might be asked of the model.

Computer simulation of hydrologic systems has many practical applications in the areas of both research and project planning and management. As a research tool the computer is valuable in the process of investigating and improving mathematical relationships. In this respect, the computer is applied not only for its calculating potential, but also for its ability to yield optimum solutions. Simulation is also ideal for investigations of hydrologic sensitivity. Problems range from the influence of a single factor upon a particular process to the effects of an entire process, such as evapotranspiration, upon the system as a whole.

In many ways computer simulation can assist in planning and development work. Models can provide the designer with runoff estimates from the input of recorded precipitation data. In addition, simulated streamflow records from statistically generated input information enable the establishment of synthetic flow frequency distribution patterns.

In the area of water resource management, computer simulation permits the rapid evaluation of the effects of various management alternatives upon the entire system. These alternatives might involve such variables as watershed treatment, including urbanization, the construction of storage reservoirs, and changes in irrigation practices within a basin.

In this study the computer model was applied to the hydrologic system of the Bear River basin of western Wyoming, southern Idaho, and northern Utah. To provide spatial resolution the basin was divided into 10 subareas or subbasins, and each was modeled separately. The submodels then were linked into a single model of the entire basin. The time increment selected for the model was one month,

and time varying quantities, therefore, were expressed in terms of mean monthly values. The model was calibrated for the Bear River hydrologic system by adjusting model parameters until close agreement was achieved between simulated and corresponding gaged outflow hydrographs for each subbasin. Data for one subbasin was inadequate for satisfactory model calibration. The calibration procedure was incorporated into the hybrid computer program of the model so that this process was implemented largely by the computer itself. Differences between observed and computed hydrographs were evaluated on the basis of the sums-of-squares. This technique of model verification is accomplished more quickly and is more objective than was the case with the manual procedure used for previous studies of this nature. The agreement achieved between observed and computed outflow hydrographs from each subbasin in the model is illustrated by Figures 5.1 to 5.9, inclusive.

The utility of the model for predicting the effects of various possible water resource management alternatives within the Bear River basin was demonstrated for the number 1 or Evanston subbasin. For example, on the assumption that all phreatophytes were eliminated from this subbasin the model predicted that the average annual discharge would be approximately 139,500 acre-feet. This figure may then be compared with the average annual discharge of 107,500 acre-feet under present conditions. Similarly, to meet the annual consumptive use demands of the existing crops within the subbasin during the dry year of 1954 would require an estimated 8,660 acre-feet of reservoir storage. These and other management studies are illustrated by Figures 5.10, 5.11, and 5.12.

Because of its fast turn-around and graphical display capabilities and its ability to solve differential equations, the hybrid computer is very efficient for model development and verification. However, for operational studies many models,

once verified, can be readily programmed for solution on the more common all-digital computer. The analog component of the Bear River model developed under this study, for example, now could be reprogrammed for general application of the entire model on a digital computer.

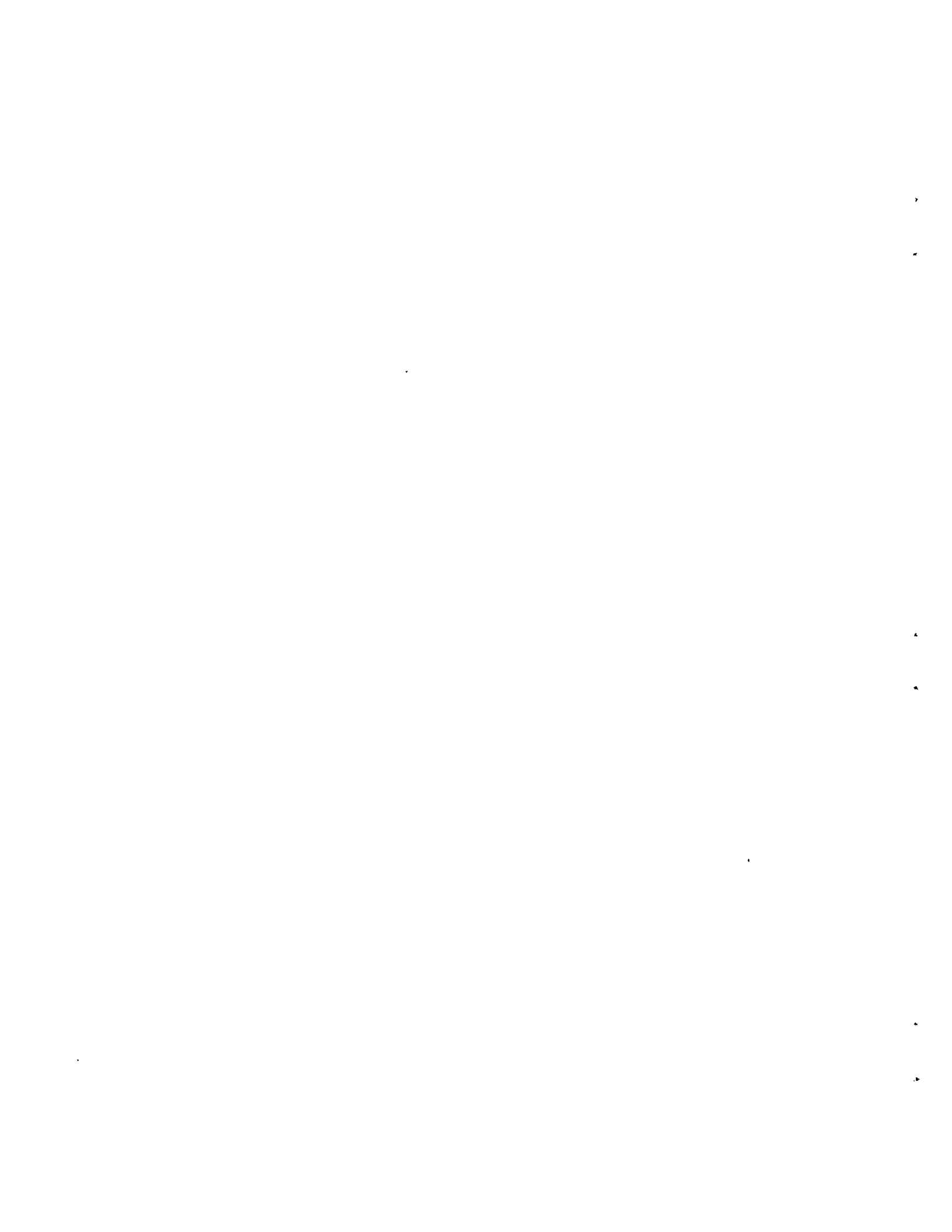
In conclusion, it is again emphasized that a model is limited by the availability of the field data used in the verification process. As further data become available, the model can be improved in terms of both the accuracy with which it defines individual processes and its time and spatial resolution. Modeling is, therefore, a continuous process, with each phase providing further insight and understanding of the system, and thus leading towards additional refinement and improvement of the model.

For each simulation study certain constraints or boundary conditions limit the degree of achievement during any particular phase of the overall program. The most important of these limiting features are the extent to which research information and basic input data are available, the degree of accuracy established by the time and spatial increments adopted for the model, equipment limitations, and the necessary time limit imposed upon the investigation period.

The model presented by this report represents a particular phase in the development of a simulation model of the hydrologic system of the Bear River basin. Further development of the model will continue and other related dimensions, such as water quality and economics, will be added. However, the model is now capable of answering many questions pertaining to the management of the water resources of the basin. The study has demonstrated the soundness and validity of the computer simulation approach to hydrologic problems within the Bear River basin, and has provided a firm basis for extending the model to include additional dimensions encountered in the comprehensive planning and management of water resource systems.

BIBLIOGRAPHY

- Blaney, Harry F., and Wayne D. Criddle. 1950. Determining water requirements in irrigated areas from climatological and irrigation data. Technical Paper 96, Soil Conservation Service. U.S. Department of Agriculture. February. 48 p.
- Chow, Ven Te. 1964. Handbook of applied hydrology. McGraw-Hill Book Company, Inc., New York. 1453 p.
- Gardner, W. R., and C. F. Ehlig. 1963. The influence of soil water on transpiration by plants. Journal of Geophysical Research 68(20):5719-5724.
- Linsley, Ray K., Jr., Max A. Kohler, and Joseph L. H. Paulhus. 1958. Hydrology for engineers. McGraw-Hill Book Company, Inc., New York. 340 p.
- McCulloch, Allan W., Jack Keller, Roger M. Sherman, and Robert C. Mueller. 1967. Ames Irrigation Handbook, W. R. Ames Company, Milipitas, California.
- Phelan, John T. 1962. Estimating monthly "k" values for the Blaney-Criddle formula. Presented at the Agriculture Research Service-Soil Conservation Service Workshop on Consumptive Use, Phoenix, Arizona. March 6-8. 11 p.
- Riley, J. Paul, D. G. Chadwick, and J. M. Bagley. 1966. Application of electronic analog computer to solution of hydrologic and river-basin-planning problems: Utah Simulation Model II, Utah Water Research Laboratory, Utah State University, Logan, Utah.
- Riley, J. Paul, J. M. Bagley, D. G. Chadwick, and E. K. Israelsen. 1967. The development of an electronic analog device for hydrologic investigations and conservation planning in the Sevier River Basin: Utah Simulation Model I. Utah Water Research Laboratory, Utah State University, Logan, Utah.
- Riley, J. Paul, and D. G. Chadwick. 1967. Application of an electronic analog computer to the problems of river basin hydrology. Utah Water Research Laboratory, Utah State University, Logan, Utah. December.
- Soil Conservation Service. Department of Agriculture. 1964. Irrigation water requirements, Technical Release No. 21, Washington, D. C. April. 61 p.
- Thorne, D. W., and H. W. Peterson. 1954. Irrigated soils. McGraw-Hill Book Company, Inc. New York. 392 p.
- U.S. Army, Corps of Engineers. 1956. Snow hydrology; summary report of snow investigations, North Pacific Division, Portland, Oregon. 437 p.
- U.S. Bureau of Reclamation, Department of Interior. 1970. Bear River Investigations. Status Report, Salt Lake City, Utah. June.
- West, A. J. 1959. Snow evaporation and condensation. Proceedings of the Western Snow Conference, Cheyenne, Wyoming. pp. 66-74.
- Willardson, Lyman S., and Wendall L. Pope. 1963. Separation of evapotranspiration and deep percolation. Journal of the Irrigation and Drainage Division, Proceedings of the American Society of Civil Engineers 89(IR3):77-88.



APPENDIX A
SUBBASIN INPUT DATA

EVANSTON												
1	EVANS	7	1	2599	2	8623	3	19835	4	314		
1	EVANS	7										
1	EVANS	8	1	832	2	809	3	3523	4	261	5	2434
			00	36	100	00	70	00	00	3200	2400	159
			1000	700	1100	00	20	00	00	00	00	250
			1	1	2	2	5					
(10X12F4,1)												
1TR			4	221	242	247	406	497	548	652	593	537
1TR			5	122	147	203	342	473	549	621	630	521
1TR			6	282	107	252	355	483	589	626	569	531
(10X12F4,2)												
1A			4	69	34	75	14	76	143	111	160	70
1A			5	67	81	49	19	129	115	137	115	128
1A			6	121	35	7	39	232	67	71	36	2
(10X12F5,0)												
1	1954	5	492	555	881	2978	1438	2840	202	77	53	70
1	1955	5	165	147	194	3878	2879	1860	183	103	52	75
1	1956	5	645	486	2560	2170	3728	652	266	216	43	68
(10X12F6,0)												
1-4	54	0	0	0	10524	36633	34202	11129	3394	2500	2631	0
1-4	55	0	0	0	0	38964	41595	11268	5551	2789	2631	0
1-4	56	0	0	0	0	21047	44726	17154	5157	2157	3167	0
1-4	54	0	0	0	0	0	0	0	0	0	0	0
1-4	55	0	0	0	0	0	0	0	0	0	0	0
1-4	56	0	0	0	0	0	0	0	0	0	0	0
(10X12F6,0)												
020554	4000	3670	4960	12520	24520	5380	654	38	0	63	423	1800
020555	2640	2400	1560	9510	28740	20530	424	136	0	214	2010	7600
020556	5980	4830	14500	14880	57090	37330	1310	57	0	9	1300	2750
019554	0	20	2350	2200	3450	1670	112	0	0	19	603	392
019555	0	0	1380	4660	3670	3640	23	80	2	192	599	8
019556	0	0	984	2050	3040	4050	531	0	0	242	1120	0
(10X12F6,0)												
018554	0	0	0	54	1800	1818	1268	562	545	427	98	0
018555	0	0	0	0	333	1350	1210	494	778	718	0	0
018556	0	0	0	0	0	1520	1650	1060	535	530	0	0
011554	2340	2220	2500	7660	34160	15670	6120	2300	2200	1970	1930	2030
011555	1950	1720	1900	3360	37470	33100	6740	3870	2210	2010	2050	2430
011556	2150	1830	2370	6920	52640	50910	9460	2750	1420	2080	2220	2190
012054	492	500	536	2250	6110	1540	431	238	293	354	386	341
012055	328	365	367	802	6900	3490	557	460	314	484	458	641
012056	580	430	652	2650	10780	4960	627	410	272	487	449	446
016054	492	555	881	2978	1438	2840	202	77	53	70	173	158
016055	165	147	194	3878	2879	1860	183	103	52	75	222	1080
016056	645	486	2560	2170	3728	652	266	216	43	68	101	145
017054	0	26	181	758	533	88	0	0	0	0	0	0
017055	0	0	0	743	1480	233	5	6	0	0	0	231
017056	123	86	548	1320	2420	270	0	0	0	0	0	0

COKEVILLE												
3	COKEV	7	1	877	2	9076	3	16982	4	510		
3	COKEV	7										
3	COKEV	8	2	88	3	1344	4	15	5	803		
			40	35	100	00	25	05	00	3380	2580	156
			2000	100	1100	00	20	00	2200	600	86	87
			2	1	2	2	1	3	1			
(10X12F4,1)												
3WTR			4	218	199	276	418	580	547	646	590	528
3WTR			5	78	115	197	350	476	544	621	628	522
3WTR			6	193	106	275	396	505	562	640	571	525
3BRTR			4	171	170	226	394	486	532	643	564	520
3BRTR			5	61	87	168	321	407	533	618	610	588
3BRTR			6	174	162	213	373	502	578	637	593	541
(10X12F4,2)												
3A			4	225	28	108	28	48	135	45	133	34
3A			5	97	157	31	79	181	169	61	218	142
3A			6	144	91	33	79	247	115	97	42	10
(10X12F5,2)												
3			4	329	384	589	1270	491	411	250	168	167
3			5	267	253	335	2350	1370	1290	420	276	192
3			6	746	469	6190	2480	2140	780	396	295	197
(10X12F5,2)												
3												
3												
3												
(10X12F5,2)												
3												
3												
3												
(10X12F6,0)												
032054	3700	3400	3620	8360	34930	24500	16073	10489	8936	5990	4250	3970
032055	3730	3050	3250	5000	24247	29141	15665	9970	7345	4810	4280	4630
032056	4330	3670	4100	10440	52471	51579	28652	11818	6605	5760	4800	4410
027054	329	384	589	1270	491	411	250	168	167	241	386	254
027055	267	253	335	2350	1370	1290	420	276	192	273	396	1320
027056	746	469	6190	2480	2140	780	396	295	197	403	374	371
026554	4890	5870	10300	8430	3290	2100	810	480	396	628	889	1620
026555	2480	2280	2000	6300	4430	9310	1790	1850	784	447	1540	7600
026556	9400	6170	38010	17070	40530	31890	2760	1440	531	849	2480	3420
(10X12F6,0)												
3GI	54	1228	1140	3287	3367	1069	854					
3GI	58	891	1208	911	2931	1059	2179	1869	1129			
3GI	56	1683	1486	5505	463410081	7327	1624	1387				

RANDOLPH												
2	RANDH	7	1	1916	2	5518	3	40025	4	1213		
2	RANDH	7										
2	RANDH	8	1	844	2	2145	3	785	4	608	5	2073
			130	45	100	00	50	02	00	3200	2650	168
			1000	140	1400	00	00	4000	100	00	20	30
			1	1	1	2	1	6				
(10X12F4,1)												
2WTR			4	218	199	276	418	580	547	646	590	528
2WTR			5	78	115	197	350	476	544	621	628	522
2WTR			6	193	106	275	396	505	562	640	571	525
(10X12F4,2)												
2A			4	93	47	102	19	105	194	150	217	95
2A			5	78	110	67	26	175	157	186	157	174
2A			6	164	40	9	53	314	92	96	51	3
(10X12F5,2)												
2	1954	5	565	571	782	843	1250	976	742	559	489	464
2	1955	5	390	338	395	446	1410	960	857	542	447	443
2	1956	5	567	467	843	2810	2920	1980	1550	1220	1810	966
(10X12F5,2)												
2												
2												
2												
2												
2												
2												
2												
(10X12F6,0)												
028554	4890	5670	19300	8430	3290	2100	810	480	396	626	889	1620
028555	2480	2280	2000	6300	4430	9310	1790	1850	784	447	1540	7600
026556	9400	6170	38010	17070	40530	31890	2760	1440	531	849	2480	3420
(10X12F6,0)												
024054	299	265	340	151	394	216	179	241	214	154	220	308
024055	290	253	280	258	257	284	234	192	173	114	284	318
024056	287	258	474	217	289	245	249	198	184	128	220	300
023054	585	571	782	843	1250	976	742	559	489	464	429	411
023055	390	338	395	446	1410	960	857	542	447	443	436	636
023056	567	467	843	2810	2920	1980	1550	1220	1810	966	737	660
021054	26	19	38	182	231	394	1170	389	0	0	22	12
021055	12	17	25	126	557	248	1430	884	32	32	23	57
021056	70	58	146	542	2220	868	1588	824	6	6	24	15
021054	552	585	937	2567	4490	1220	697	515	474	780	684	534
021055	457	443	531	1630	7520	2840	914	638	571	622	622	1680
021056	988	764	1550	4860	11460	2790	1049	688	638	698	621	573
019554	0	28	2350	2200	3450	1670	112	0	0	110	603	392
019555	0	0	1380	4660	3670	3640	23	80	2	192	599	8
019556	0	0	984	2050	3040	4050	531	0	0	242	1120	0
020554	4000	3670	4960	12520	24520	5380	654	38	0	63	423	1800
020555	2640	2400	1560	9510	28740	20530</						

BEAR LAKE
 5 BRLKE 7 1 8959 2 12347 3 20121 4 18098 5 42 11 46
 5 BRLKE 7
 5 BRLKE 6 1 21283 2 7307 3 3100 4 2636 5 8038
 20 40 100 00 00 24 03 3500 3100 155 2800 100
 1000 250 600 40 00 00 00 00 00 00 00 250 350
 3 1 1 2 1 4 1
 .33333333 100 100 100,000232496,000232498 100 100
 (10X12F4,1)
 MONTTR54 235 235 277 426 516 548 676 626 551 438 360 174 422
 MONTTR55 138 124 192 331 495 555 639 661 552 442 264 241
 MONTTR56 230 115 257 406 516 590 661 621 587 439 263 193
 LIFTR54 139 250 270 431 520 568 696 624 568 437 365 194
 LIFTR55 136 125 199 333 495 576 653 661 543 442 232 253
 LIFTR56 229 120 267 409 529 604 661 622 550 435 270 203
 LAKETR54 277 276 310 452 520 548 670 624 559 445 370 216
 LAKETR55 178 147 210 349 494 552 632 640 543 444 301 303
 LAKETR56 261 167 293 428 513 561 647 607 561 447 288 239
 (10X12F4,2)
 5 PR54 223 52 170 36 148 190 47 55 116 164 137 181
 5 PR55 184 185 99 149 154 94 208 241 75 175 397
 5 PR56 200 92 23 69 311 82 58 52 22 115 16 180
 (8X12F6,3)
 LOGR54 6830 5760 6800 12530 28260 17430 12140 8900 7090 6640 6000 5460
 LOGR55 5320 4610 5890 8640 29680 28500 15090 10220 7780 7370 6490 6660
 LOGR56 8010 6300 8200 22630 40230 41860 18920 12560 9620 8870 7640 7130
 (10X12F5,2)
 5 4 361 401 261 100 135
 5 295 374 291 122 136
 5 498 818 402 190 295
 5 1200 400
 BRLKCN54 1480 700 150 100
 BRLKCN55 1192 1080 300 200 100 100
 (8X12F6,0)
 PESC54 4640 5160 9950 10370 36940 41940 69190 52610 26620 7009 3989 6191
 PESC55 5823 5430 3600 18040 11429 30818 75045 42977 35804 8643 9554 13363
 PESC56 12652 6856 15459 28261 35872 35643 70171 56506 26899 10121 6893 8897
 (8X12F6,0)
 HARE54 12130 13120 22110 26290 32260 17610 12260 7950 5730 8690 9990 9440
 HARE55 8820 6180 9930 26590 24500 31420 14160 10450 7350 10290 10370 15000
 HARE56 19000 12420 4230 7831100800 93550 22610 12450 8000 11390 11910 11210
 MONT54 443 308 513 1380 1800 1250 752 492 460 471 429 358
 MONT55 350 305 332 825 1450 2010 956 573 425 461 456 594
 MONT56 582 391 559 3820 5030 2710 1260 745 580 598 584 529
 046054- 9550-10450-20520-26010-11510- 780- 2160- 2190- 732- 4710- 7930- 5370
 046055- 6020- 6130- 7540-22980-11770- 7390- 2680- 5570- 1650- 7630- 6630-10480
 046056-13620- 8320-39340-74140-85450-67020-10650- 7130- 935- 5180- 8380- 7330
 059554 71 96 81 60 32540 35940 65770 53380 26120 3730 714 155
 059555 123 111 123 119 9990 14780 78520 34440 34070 3340 6590 841
 059556 762 805 881 3190 4570 18740 82860 51790 20800 3230 825 3420
 (10X12F5,2)
 SODA
 6 SODA 7 1 2677 2 3703 3 6098 4 3022
 6 SODA 7
 6 SODA 8 1 848 3 2886 5 1890
 20 35 100 00 230 31 00 3600 2400 92 2500 240
 1000 100 600 00 00 00 00 00 00 00 250 300
 2 1 1 1 1 1
 .50 100 100 100,8899 8899 100
 (10X12F4,1)
 MONTTR54 235 235 277 426 516 548 676 626 551 438 360 174 422
 MONTTR55 138 124 192 331 495 555 639 661 552 442 264 241
 MONTTR56 230 115 257 406 516 590 661 621 587 439 263 193
 GRACR54 151 261 288 444 521 543 672 627 566 447 388 213
 GRACR55 138 154 234 364 491 553 645 655 552 460 286 255
 GRACR56 148 146 279 417 520 590 659 615 566 441 273 201
 (10X12F4,2)
 6 PR54 172 184 263 132 164 294 73 165 181 60 176 34
 6 PR55 87 93 95 191 281 425 59 256 184 195 158 380
 6 PR56 210 84 23 93 298 73 55 16 38 147 32 133
 (10X12F5,2)
 GEOR 54 1530 1330 1490 1478 1880 1910 1910 1830 1680 1640 1550 1510
 GEOR 55 1358 1168 1300 1280 1540 2040 2000 1890 1720 1720 1490 1620
 GEOR 56 1450 1320 1420 1680 3290 2970 2390 2130 2020 1900 1703 1650
 (10X12F5,2)
 6 1954 4 0 0 0 0 200 700 300 500 400 0 0 0
 6 1955 4 0 0 0 0 0 1300 1100 1400 400 0 0 0
 6 1956 4 0 0 0 0 0 1000 1600 1600 1700 1000 0 0 0
 (10X12F5,2)
 6 1954 6 1217 1200 2107 2216 4023 4325 6985 4930 2988 1989 1005 1181
 6 1955 6 1128 1259 1117 2999 1830 3245 6754 3888 3531 1276 1632 1943
 6 1956 6 1840 1424 2933 4230 4434 3749 6337 5048 2748 1437 1362 1493
 (10X12F5,2)
 6 1954 3 554 584 994 1630 3376 3813 6183 4734 2535 752 482 670
 6 1955 3 624 574 426 1681 1128 2788 6705 3901 3199 991 996 1303
 6 1956 3 1228 711 1468 2604 3405 3358 6310 5999 2515 1094 765 939
 (10X12F5,2)

ONEIOA
 7 ONEIO 7 1 11873 2 5381 3 2367 4 7927 5 36 6 1471 7 1363
 7 ONEIO 7 11 466
 7 ONEIO 8 1 597 3 1233 5 1005
 40 60 100 00 50 00 00 00 00 2200 78 2000 200
 1000 450 700 50 300 00 00 00 00 00 250 350
 1 1 1 1 1 1 1 1 1
 1 1 100 1 1 1 1 1,38713 .38713 1
 (10X12F4,1)
 GRACR54 151 261 288 444 521 543 672 627 566 447 388 213
 GRACR55 138 154 234 364 491 553 645 655 552 460 286 255
 GRACR56 148 146 279 417 520 590 659 615 566 441 273 201
 (10X12F4,2)
 7 PR54 146 89 223 112 139 250 62 140 154 51 149 29
 7 PR55 73 79 88 162 234 360 50 217 158 160 134 322
 7 PR56 170 71 23 79 240 62 47 14 33 125 27 113
 (10X12F5,2)
 COTTON54 612 376 1160 3930 1160 469 171 148 150 260 371 332
 COTTON55 376 353 473 2360 4210 2020 326 314 182 185 363 1090
 COTTON56 1070 817 2840 9100 4270 637 297 295 127 387 451 507
 (10X12F5,2)
 7 1954 4 0 0 0 0 640 510 530 330 240 0 0 0
 7 1955 4 0 0 0 0 250 750 550 490 260 0 0 0
 7 1956 4 0 0 0 0 470 800 880 480 310 0 0 0
 (10X12F5,2)
 7 1954 6 2420 2440 3804 4180 4520 4940 6910 6190 4340 2390 2360 2260
 7 1955 6 2240 2210 2370 4800 3090 3470 7630 4650 4800 2430 3130 4030
 7 1956 6 3510 2700 4400 7090 5950 3820 6790 6310 3910 2450 2270 3000
 (10X12F5,2)
 7 1954 3 1467 1443 2547 2952 4761 5840 7040 5710 3470 1200 1200 1400
 7 1955 3 1340 1490 1340 3700 2540 3950 7830 4510 4100 1490 1920 2250
 7 1956 3 2230 1730 3210 5800 5550 4390 7340 6860 3100 1700 1620 1770
 (10X12F4,2)
 GRWATR54 300 300 300 300 300 300 300 300 300 300 300 300
 GRWATR55 300 300 300 300 300 300 300 300 300 300 300 300
 GRWATR56 300 300 300 300 300 300 300 300 300 300 300 300
 CACHE VALLEY
 8 CACHE 7 1 52420 2 27363 3 6050 4 50020 5 9469 6 4827 7 289
 8 CACHE 7 8 392 10 3 11 883 13 275
 8 CACHE 8 1 7915 2 15863 3 19771 4 5776 5 7775
 20 50 100 00 00 17 00 3100 2500 116 1080 200
 1000 350 700 00 00 00 43 00 00 00 00 250 300
 5 1 1 1 3 4 1 1
 20 1 100 1 1 1 1,000078943,000078943 1
 (10X12F4,1)
 PRESTR54 176 297 351 491 587 610 230 600 603 484 405 268
 PRESTR55 159 192 287 240 544 613 695 710 601 408 318 299
 PRESTR56 300 204 368 467 371 643 706 662 612 486 313 237
 LEWITR54 272 300 350 486 564 602 715 682 587 475 400 250
 LEWITR55 144 169 272 413 542 601 681 701 585 474 295 284
 LEWITR56 200 194 307 470 370 630 698 655 596 470 308 215
 RICHTR54 226 315 363 496 567 697 732 687 625 494 427 251
 RICHTR55 167 215 308 419 542 613 697 726 611 508 334 312
 RICHTR56 318 213 360 460 569 632 704 679 627 494 324 244
 LOUSTR54 207 308 366 522 592 611 741 696 625 493 416 267
 LOUSTR55 175 208 384 422 565 621 716 735 620 512 316 316
 LOUSTR56 309 208 374 487 582 660 730 694 645 503 308 257
 LOGATR54 279 308 382 498 566 603 725 685 612 493 415 255
 LOGATR55 135 197 292 420 547 615 696 707 598 508 330 314
 LOGATR56 309 295 365 476 577 651 721 680 623 409 321 249
 (10X12F4,2)
 8 PR54 170 82 295 92 96 197 31 22 142 68 199 125
 8 PR55 205 184 100 211 168 227 24 168 225 100 215 411
 8 PR56 303 66 9 86 303 89 47 69 23 21 148 71 174
 (8X12F6,3)
 LOGR54 6830 5760 6800 12530 28260 17430 12140 8900 7090 6640 6000 5460
 LOGR55 5320 4610 5890 8640 29680 28500 15090 10220 7780 7370 6490 6660
 LOGR56 8010 6300 8200 22630 40230 41860 18920 12560 9620 8870 7640 7130
 (10X12F5,2)
 CANALS54 980 550 640 340 150
 CANALS55 400 450 800 300 250
 CANALS56 200 800 1300 1000 500 250
 (8X12F6,0)
 8EAR54 63030 66650 84070 91320 20330 12890 2800 2130 15800 35020 45200 46950
 8EAR55 53740 46300 6481015000 80340 46200 2020 4842 13300 38060 59630105400
 8EAR56 111400 70920117300158200152000 32390 4690 8630 9200 39030 58810 67510
 ECNL54 0 3 0 642 9050 8810 9880 9560 6700 2170 333 2
 ECNL55 0 0 0 0 5900 7210 10830 8640 6460 2720 35 0
 ECNL56 0 0 0 831 8650 9210 9980 9580 8590 2980 424 0
 WCNL54 1720 1480 26 1782 38270 34550 39030 30240 25910 11030 5560 3180
 WCNL55 1590 924 452 0 21100 29710 42140 35340 30910 13300 5260 1530
 WCNL56 1180 978 728 0 27398 46890 40600 31790 16400 4540 3340
 (8X12F6,0)
 ONID04 24140 24280 37850 41650 39350 41860 60190 56920 40080 23750 23450 22470
 ONID05 22370 22050 23570 47840 26890 26190 67710 39620 42970 24190 31160 40120
 ONID06 34880 26900 44600 70650 54810 20360 58530 35150 24410 22620 29850
 LOGN54 6830 5760 6800 12530 28260 17430 12140 8900 7090 6640 6000 5460
 LOGN55 5320 4610 5890 8640 29680 28500 15090 10220 7780 7370 6490 6660
 LOGN56 8010 6300 8200 22630 40230 41860 18920 12560 9620 8870 7640 7130
 BLFK54 5950 4480 5630 10200 8560 5870 5160 4720 4290 4240 4910 3910
 BLFK55 4070 3610 4030 7720 15140 7443 5710 5160 4590 4660 4330 6830
 BLFK56 7000 5300 7600 20360 19290 10770 8580 7340 6300 6100 5650 5460
 LBPN54 3390 3360 5100 11400 1840 1610 1000 829 809 1920 2620 2340
 LBPN55 2560 2450 3660 13900 18540 3860 1180 964 1080 1930 2850 9840
 LBPN56 7300 4500 9590 17140 14170 3320 1400 1060 956 1840 3100 3340
 (10X12F3,2)
 GWATER54 43 43 43 43 43 43 43 43 43 43 43
 GWATER55 43 43 43 43 43 43 43 43 43 43 43
 GWATER56 43 43 43 43 43 43 43 43 43 43 43

* See Appendix B for an explanation of the variables.

TREMONTON

10 BRTRE 7	1	17803	2	13750	3	1158	4	16645	5	6513	6	8812	7	72
10 BRTRE 7	8	2893	10	507	11	217	13	217						
10 BRTRE 8	1	934	2	3092	3	4525	4	2698	5	9506				
30	55	100	00	40	11	80	3600	2600	111	2800	200			
1000	100	600	00	00	2400	1700	83	84	85	250	550			
2	5	1	1	4	1	1								

(10X12F4.1)

CORITR54	307	335	308	525	592	624	747	705	623	512	433	291		
CORITR55	165	222	322	458	589	640	718	735	615	584	311	317		
CORITR50	310	224	393	508	610	667	740	685	630	510	327	276		
GARLTR54	285	324	360	490	599	623	756	700	620	486	431	291		
GARLTR55	140	205	305	422	559	624	723	731	611	499	301	279		
GARLTR50	312	197	374	481	585	603	743	698	630	586	322	281		

(14X12F4.2)

421731	1954	162	70	281	34	110	78	16	10	225	29	102	113	1253
421731	1955	310	144	83	189	145	215	10	126	183	43	194	204	1818
421731	1956	330	30	15	150	223	70	57	00	00	127	11	153	1172
423122	1954	105	47	173	56	53	129	52	16	172	70	139	106	1120
423122	1955	141	185	90	84	126	222	09	229	120	38	77	120	1444
423122	1956	241	46	08	82	190	48	13	01	09	69	54	113	673

(8X12F5.0)

10109054	6830	5700	8800	12530	28260	17430	12140	8800	7090	6640	8000	5460		
10109055	5320	4810	5890	6040	29660	26500	15800	10220	7700	7370	6490	6660		
10109056	8010	6300	8200	22030	49230	41860	18920	12500	9020	8870	7640	7130		

(10X12F5.2)

10 1954	4	0	0	0	50	900	900	1010	1010	660	270	120	60	
10 1955	4	0	0	0	0	560	760	1000	910	770	330	110		
10 1956	4	0	0	0	0	680	1040	1030	1040	790	400	100	60	

(8X12F6.0)

BRC054	73220	72490	92750	104200	31840	21140	7540	6970	20510	44010	55270	55520		
BRC055	63970	58910	96400	127700	87970	55870	7280	10380	18490	45820	68370	111100		
BRC058	130500	79540	124500	165000	102500	44720	7690	14000	15150	46920	64750	76990		

(8X12F8.0)

BEAR54	63030	66550	64070	91320	20330	12890	2000	2130	15890	35020	45200	46950		
BEAR55	53740	48300	64810	115000	88340	46200	2020	4840	13380	38060	59830	105400		
BEAR56	11400	70920	17300	150200	152800	32390	4600	6630	9290	39830	58610	67510		
MLA054	3670	5350	5840	3250	1990	1480	1420	1200	1260	1690	2510	3270		
MLA055	2990	2950	5700	5900	3690	2480	1230	1420	1320	1670	3410	4720		
MLA056	4910	3460	7520	3990	2510	1350	1120	1140	1050	1350	2160	3020		
ECNL54	0	0	0	662	9050	8810	9680	9560	0700	2170	533	2		
ECNL55	0	0	0	0	5900	7010	10030	8640	6480	2720	35	0		
ECNL56	0	0	0	631	5650	9210	5900	9500	6590	2090	424	0		
WCNL54	1720	1460	28	1700	38270	34550	39030	39240	25910	11030	5060	3180		
WCNL55	1550	924	452	0	21100	29710	42140	35340	30610	13380	5260	1530		
WCNL56	1160	978	728	0	27390	40890	40640	40680	31790	16480	4340	3190		

(10X12F3.2)

* See Appendix B for an explanation of the variables.

APPENDIX B
COMPUTER PROGRAM

APPENDIX B

USER INSTRUCTIONS FOR THE HYDROLOGIC SIMULATION PROGRAM, OPVER

The computer program titled OPVER is a main driving program for linking the various subroutines required for simulating the hydrology of a river basin. In addition, a pattern search algorithm is incorporated within it. A flow chart of OPVER is shown in Figure B.1.

The operating instructions for OPVER are summarized as follows:

1. Load OPVER with the core image loader. Upon loading, the teletype should type MAIN 1 and the computer should be in PAUSE mode.
2. Ready the card reader, line printer, and analog computer. Insure that the proper patch panels are in place on the analog computer, and that a properly set-up card deck is in the read hopper.
3. Place the analog computer in SP and DIG MODE and set logic mode to R and time selector to 10^1 . Insure that counter 0 is set to 1 for FAST operation (line printer output only) or 10 for SLOW operation (x-y plotter output).
4. Push RUN-SINGLE-RUN (RSR) buttons whereupon card reader should start and option selected will be performed. For options 1 and 2, go to step 5. For option 3, go to step 7. For option 4 go to step 9, and for option 5 go to step 11.
5. Teletype will type HYDSM 1 and computer PAUSES.
6. Insure proper data for option specified is in card reader and RSR. For option 1 and 2, BASIC data (Group 2 cards) should be read by the card reader.
7. Teletype will type CARDS (I) for options 1 and 3 and MAIN 1 for option 2, and then PAUSE. Insure that data for subbasin I (Group 3 cards) are in hopper and RSR to continue for option 1 and 3. For option 2, return to step 2.
8. Teletype will type RESET DB. Set SSW D if desire reruns each year, SSW B if desire reruns each subbasin, and SSW C if desire acre-feet table.
9. Push RSR and analog computer will operate for specified time after which teletype will print MAIN 1, CARDS (I+1), or RESET DB and computer will PAUSE. For MAIN 1, CARDS (I+1), and RESET DB return to steps 2, 7, and 8, respectively. Set or reset SSW D, B, and C as specified in step 8 and set SSW E if desire to use recorded inflow for QRIV and QGLI rather than upstream subbasin simulated outflow for these inflow values. (When using SSW E option, all inflow data must be acre-feet.)
10. Analog computer will operate for specified time and teletype will respond as in step 8. Follow appropriate option outlined in step 8 to continue.
11. Card reader should have input the information necessary for the pattern search operation of the program (Group 4 cards) and upon completing all phases specified teletype will print MAIN 1. Return to step 2 to continue further operation.

The operating procedure is shown schematically in Figure B.2. The input data necessary for a run may be classified as:

1. Control cards for OPVER specifying the desired option.
2. Basic data consisting of labels for row and column headings for printed output and other data that is common to all subbasins that may subsequently be run.
3. Subbasin data needed to define the specific simulation desired.
4. Boundary conditions and options necessary to control the pattern search.

The deck set up for a typical pattern search run is shown in Figure B.3. Detailed instructions for preparing the cards for each of the four groups of data are given in Tables B.1, B.2, B.3, and B.4 respectively. Notation used in the program is given in Table B.5. A list of input data for a sample problem is shown in Figure B.4. Input data for each subbasin is listed in Appendix A. Representative output may be observed in Appendix C. The program for the analog portion of the model is shown as Figure B.5 and a listing of OPVER and all of its subroutines is given in Figure B.6. Flow charts for the major subroutines HYDSM, BASIC, SUBDAT and RESRV are also included in Figures B.7, B.8, B.9, and B.10 respectively.

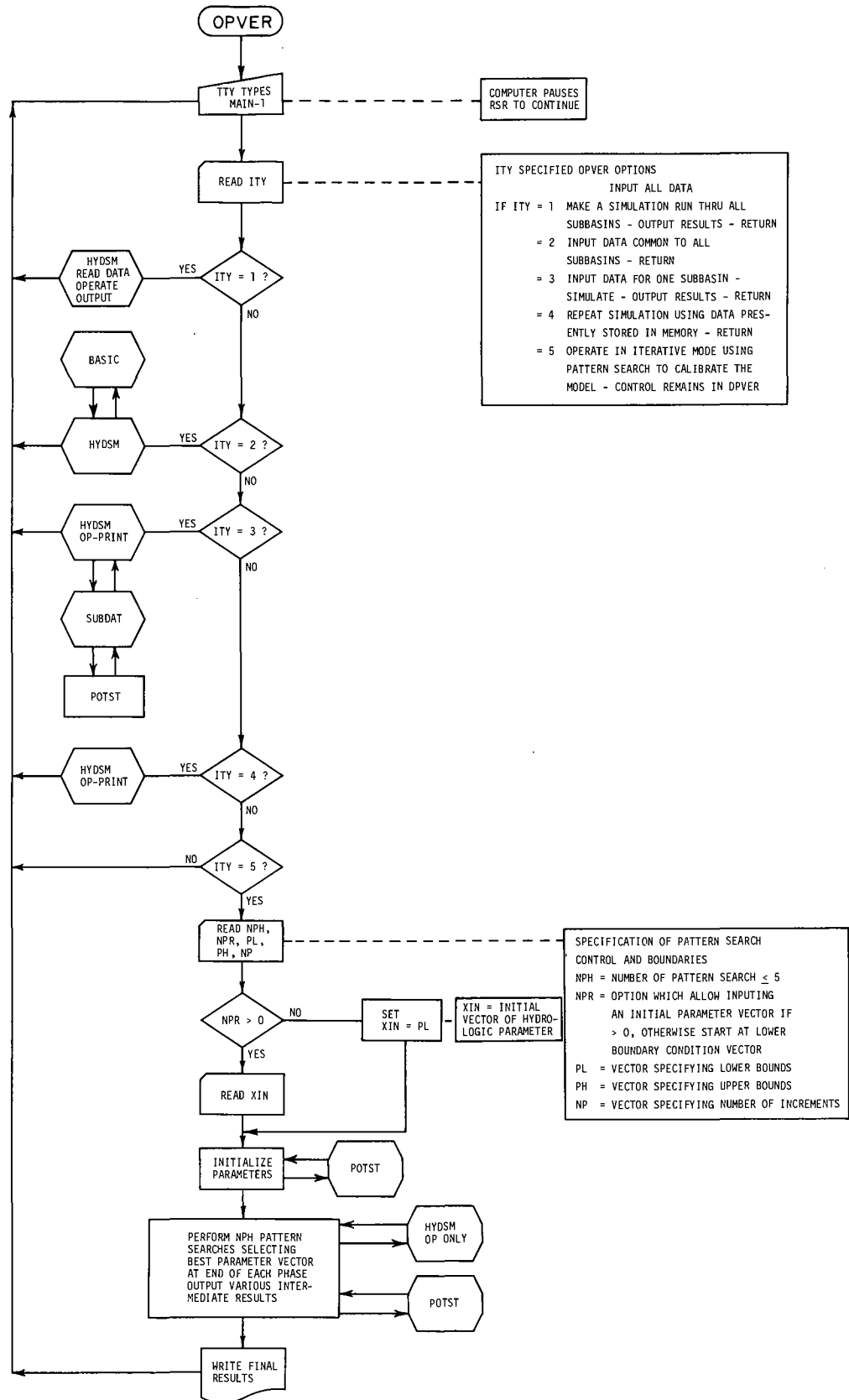


Figure B.1. Flow chart of hydrologic simulation program OPVER.

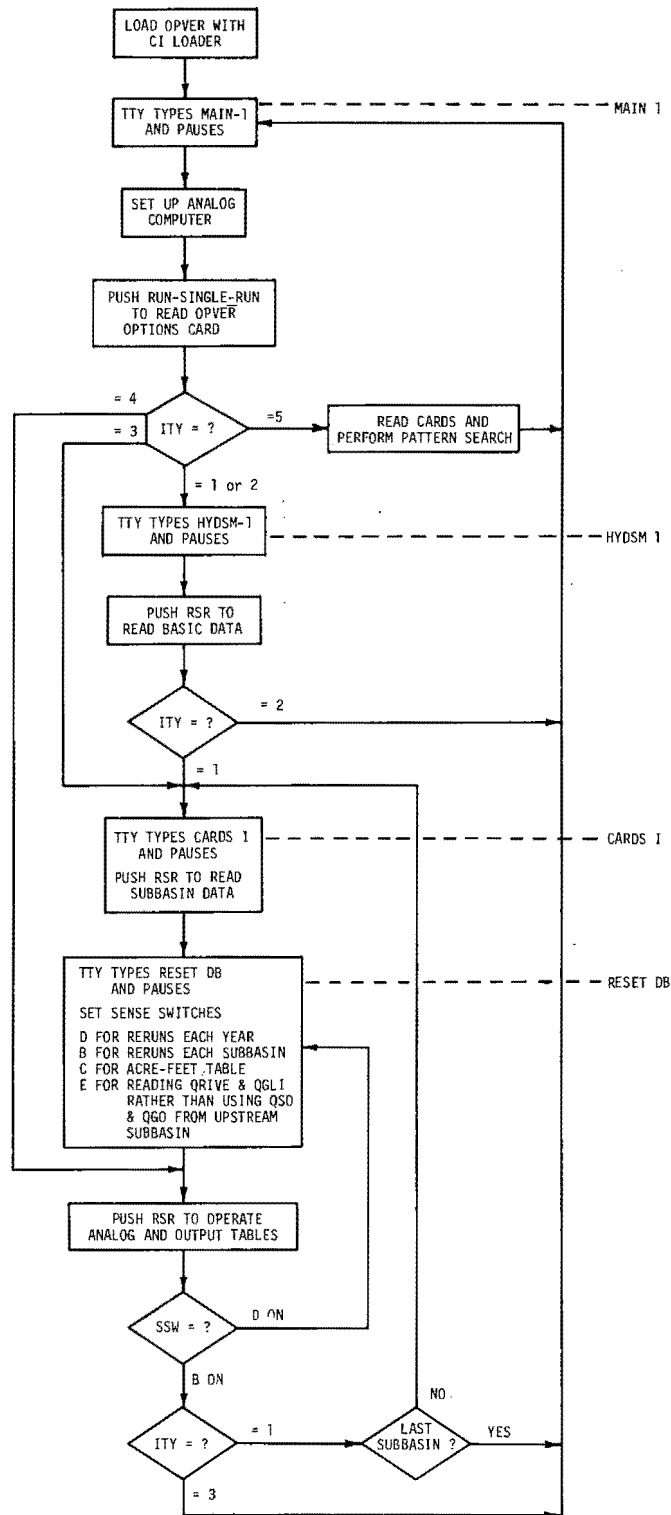


Figure B.2. Schematic diagram of operating procedures for OPVER.

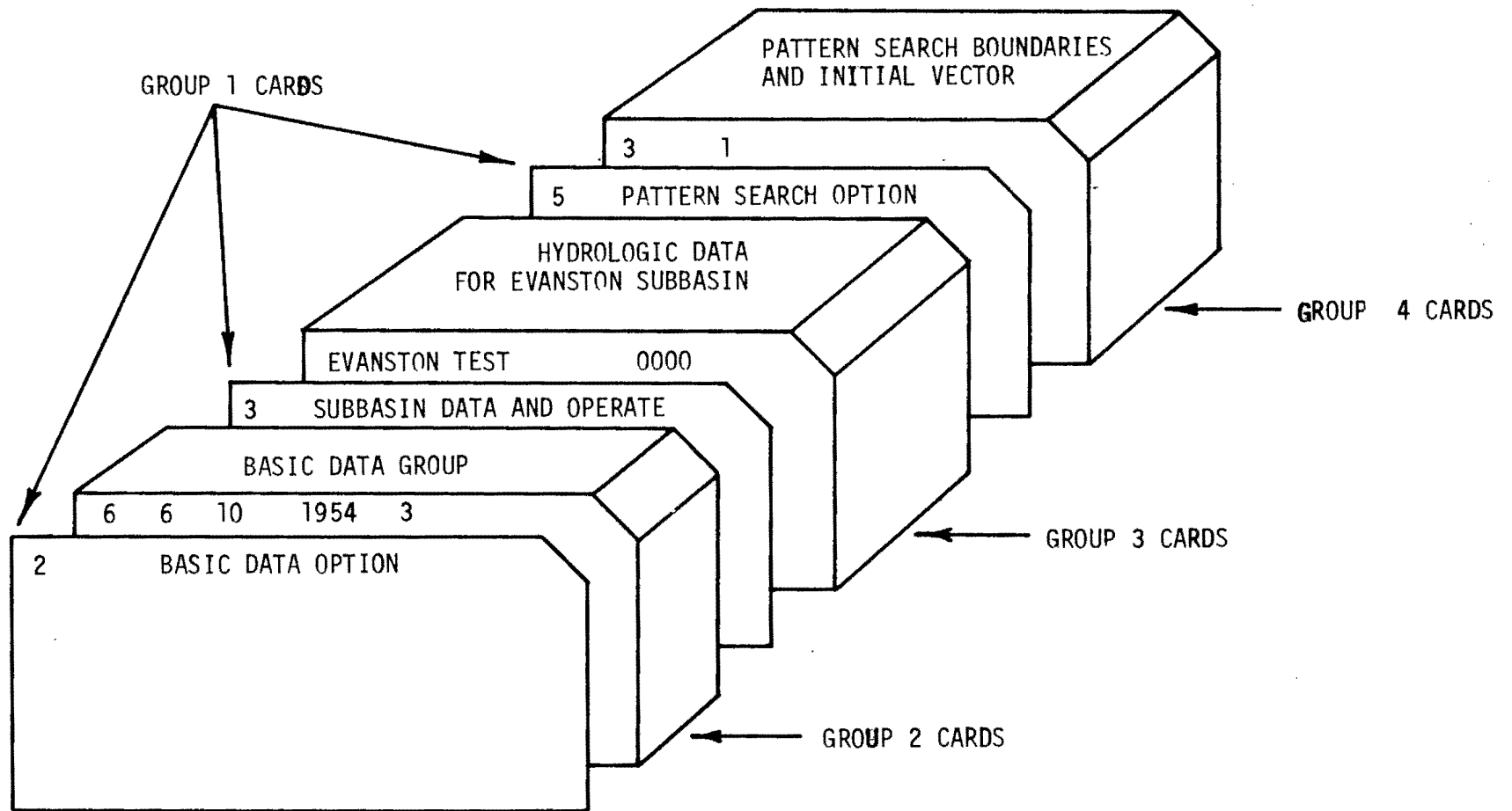


Figure B.3. Deck setup for typical OPVER run.

Table B.1. Preparation instructions for OPVER option control cards - group 1 cards.

<u>Column</u>	<u>Format</u>	<u>Mnemonic</u>	<u>Description</u>
1-5	I5	ITY	OPVER option specification: if ITY = 1 simulation = 2 read basic data only = 3 read subbasin data and operate for specified period = 4 rerun last subbasin = 5 perform pattern search

Table B.2. Preparation instructions for BASIC data - group 2 cards.

<u>Card</u>	<u>Format</u>	<u>Mnemonic</u>	<u>Description</u>
1	(5I5)	INP IOUT	Input device number for subbasin data Output device number for simulation output
		NSB LYRO NYR	Number of subbasins First year of simulation Number of years of simulation
2	(13(1XA3))	V_k	13 element vector of column headings for output tables; i. e. JAN., FEB., ANN
3	(20A4)	$VARLB_i$	20 element vector of row titles for output tables. Must correspond to elements as shown in sample output shown in Figure
4	(12F5.3)	PDL_k	Vector of proportion of daylight hours for months in the same order as vector V
5_1-5_{14}	(10X12F5.2)	WKC_{jk}	Array of consumptive use coefficient for crops for modified Blaney- Criddle equation. Fourteen cards required, one for each crop. j is crop, k is month
6_1-6_7	(10X12F5.2)	PKC_{jk}	Array of consumptive use coefficient for phreatophytes. Seven cards required, one for each phreatophyte. j is phreatophyte, k is month

Table B.3. Preparation of subbasin data cards - group 3 cards.

Card	Format	Mnemonic	Description
1	(10A4, 4I5)	BASID IRES MANG JRES JCONV	40 column page heading >0 specifies reservoir operation option of HYDSM >0 specifies management option of HYDSM >0 specifies reservoir operation on canal diversions - not presently implemented >0 specifies conversion factors to be read from card for converting input data to inches
2*	(10X10F7.0)	RES ₁	10 element vector of reservoir operating parameters. Needed only if IRES > 0. See Table B. 5-C for detailed element breakdown.
3*	(10X3F7.0)	CTM CMS BAREA	Temperature for management of canal diversions Management parameter for soil moisture storage Base area for which the model parameters were developed. Needed only if MANG > 0
4*	(10X10F7.0)	RESC ₁	10 element vector of canal reservoir parameters. Needed only if JRES > 0. Not implement at present
5	(10X7(I3, F10.0))I _{1j} , DCA _j		Vectors of crop number and area in acres for j th crop corresponding to WKC _{jk} . Exactly 2 cards are required. If DCA _j = 0, neither I _{1j} nor DCA _j need be punched
6	(10X7(I3, F10.0))I _{1j} , DCA _j		Vector of phreatophyte no and area in acres for phreatophyte j corresponding to j th phreatophyte in PKC _{jk} . One card required

* These cards are required only if an option parameter for them is greater than zero.

Table B.3. Continued.

Card	Format	Mnemonic	Description
7	(12F6.2)	DIG ₁ SKAL SKF	10 element vector of digital model parameters. See Table B. 5-A for detailed element breakdown. Scale factor for soil moisture phase of analog simulation Scale factor for channel phase of analog simulation. If SKF is read as 0, it is set to 2.0 by the program
8	(12F6.2)	PH ₁	12 element vector of analog model parameters. See Table B. 4-B for detailed breakdown
9	(8I5)	N ₁	Vector of the number of stations with NYR years of data of type 1 which are to be read in and used by the program. Data types correspondence is as follows: 1 = 1 temperature stations = 2 precipitation stations = 3 stream correlation station = 4 canal diversion stations = 5 gage outflow stations = 6 gage river inflow stations = 7 subsurface inflow stations = 8 minimum monthly outflow stations (used only if IRES > 0)
10*	(8F10.2)	CVR _j	Vector of conversion factors to convert input data to inches. Needed only if JCON > 0. If JCONV = 0, program assumes that all input flow data is in acre-feet
11 ₁ *-11 ₈ *	(10A4)	FMT ₁	40 character format specification card followed by (NYR* N ₁) cards of input data for type 1 above. A set of these cards for a particular type data are included only if N ₁ 0

Table B.4. Preparation instructions for pattern search specification cards - group 4 cards.

Card	Format	Mnemonic	Description
1	(3I5)	NPH	Number of phases to be run during pattern search. $1 \leq NPH \leq 5$
		NPR	Option specifying initial search vector If NPR = 0 start at lower boundary > 0 Input initial vector from cards
		NWC	Option specifying monthly weighting coefficients for calculating $OBJ = \sum W_R (DIFF_R)^2$ If NWC = 0 use $W_R = 1.0$ > 0 Input W_R from cards
2	(12F6.2)	W_R	Vector of monthly weighting coefficients for calculating OBJ Needed only if NWC > 0
3	(9F6.2)	PL_1	Vector of lower bounds for the digital parameters. See Table B.5-A for a detailed description $l = 1$ to 9
4	(9F6.2)	PH_1	Vector of upper bounds for the digital parameters. $l = 1$ to 9
5	(9I5)	NP_1	Number of steps for each digital parameter. $l = 1$ to 9
6	(12F6.2)	PH_1	Vector of lower bounds for the analog parameters. See Table B.5-B for a detailed description. $l = 10$ to 21
7	(12F6.2)	P PH_1	Vector of upper bounds for the analog parameters $l = 10$ to 21
8	(12I5)	NP_1	Number of steps for each of the analog parameters $l = 10$ to 21
9*	(9F6.2)	XIN_1	Vector of initial digital parameter $l = 1$ to 9 needed only if NPR > 0
10*	(12F6.2)	XIN_1	Vector of initial analog parameters $l = 10$ to 21 Needed only if NPR > 0

* These cards are required only if an option parameter is greater than zero

Table B.5. Notation for OPVER and its subroutines.

A. Digital parameters, DIG(I). Input by SUBDAT.

I	Mnemonic	Description
1	KS	Snowmelt rate exponent
2	CIR	Irrigation efficiency (decimal)
3	CKC	Consumptive use coefficient (=1.00)
4	C1	Precipitation ungaged inflow coefficient
5	C2	Snowmelt ungaged inflow coefficient
6	COR	Surface stream ungaged inflow coefficient
7	PTH	Precipitation threshold for runoff (inches)
8	TS	Snowfall temperature (°F)
9	TSM	Snowmelt temperature (°F)
10	SNW	Initial snow water content (inches)

B. Analog parameters, PH(I). Input by SUBDAT.

I	Mnemonic	Description
10	KG	Smoothing coefficient for groundwater inflow (≤ 1.0)
11	DTA	Cropland groundwater return flow delay time (months)
12	MCS	Soil moisture capacity (inches)
13	QGTIC	Initial cropland groundwater return flow (inches)
14	QGZIC	Initial groundwater inflow (inches)
15	QH	Threshold separating high and medium groundwater outflow ranges
16	QM	Threshold separating medium and low groundwater outflow ranges
17	CGH	Fraction groundwater outflow, high range
18	CGM	Fraction groundwater outflow, medium range
19	CGS	Fraction groundwater outflow, low range
20	MES	Critical soil moisture level (inches)
21	MIC	Initial soil moisture storage (inches)

Table B.5. Continued.

C. Reservoir operation parameters, RES(I). Input by SUBDAT when IRES > 0.

<u>I</u>	<u>Mnemonic</u>	<u>RES(I) Description</u>
1	STI	Initial storage volume in reservoir (acre-feet) at time 0
2	STMN	Minimum usable storage (acre-feet)
3	STMX	Maximum storage (acre-feet)
4	ER	Desired accuracy level for successive area computation
5	CA	Reservoir area at STMN = 0, (acres)
6	C1	Constant in area equation one
7	C2	Exponent in area equation one
8	STB	Break point storage between area equation one and two (acre-feet)
9	C3	Constant in area equation two
10	C4	Exponent in area equation two

D. Subbasin hydrologic input data, DUM(J,K,L). Input by SUBDAT. J is the year, K is the month, and L is the data type.

<u>L</u>	<u>Mnemonic</u>	<u>Description</u>
1	TEMP	Subbasin monthly temperature data ($^{\circ}$ F)
2	PPT	Subbasin monthly precipitation data (inches)
3	QCOR	Surface streamflow data for correlating to obtain monthly ungaged surface inflow (acre-feet)
4	QCNL	Subbasin monthly canal diversions (acre-feet)
5	QGAG	Subbasin monthly gaged surface outflow to be used for verification with OPVER (acre-feet)
6	QRIV	Subbasin measured monthly surface inflows (acre-feet)
7	QGLI	Subbasin measured or estimated monthly groundwater inflows (acre-feet)
8	QR	Minimum monthly outflow values for the reservoir when IRES > 0 (acre-feet)

Table B.5. Continued.

E. Labels on tables of printed output, OUT(K,L). K is the month and L is the data type.

<u>L</u>	<u>Mnemonic</u>	<u>Description</u>
1	TEMP	Monthly temperatures ($^{\circ}$ F)
2	F	Blaney-Criddle F
3	PPT	Monthly precipitation (inches)
4	QRIV	Measured monthly surface inflow
5	QUNG	Monthly unmeasured surface inflow
6	QCNL	Monthly canal diversions
7	QSIT	Surface water available for transfer through the basin
8	QIGS	Surface water applied to soil moisture storage of the agricultural area
9	QGLI	Monthly measured or estimated groundwater inflow
10	SNW	Snow storage at end of month
11	SNMT	Monthly snowmelt
12	ETPH	Evapotranspiration from the phreato-phyte area
13	ETP	Potential evapotranspiration from the crop area
14	ET	Actual evapotranspiration from the crop area
15	MS	Soil moisture storage at end of month
16	DP	Monthly deep percolation after delay
17	QTO	Total monthly outflow from basin
18	QGO	Groundwater outflow from basin
19	QSO	Surface outflow from basin
20	QGAG	Gaged surface outflow from basin
21	DIFF	Difference between QSO and QGAG
	OBJ	Sum of squared differences (DIFF) ²
	OBA	Algebraic sum of annual differences

```

2          INITIAL DATA IN
6 6 10 1954 3
JAN FEB MAR APR MAY JUN JULY AUG SEP OCT NOV DEC ANN
TEMP P PRTQRIVQUNGQCNLQISITQIGSSGLI SNWSNMTETPH ETP ET MS DP QTO QGG QSOQGAG
06 67 83 90 101 102 104 98 84 78 66 63
A1 ALFA 1 63 74 86 99 112 119 110 105 99 90 79 65
A2 PAST 2 55 66 81 86 102 99 93 91 87 80 74 58
A3 ACHA 3 55 66 81 94 109 115 110 105 95 84 77 62
A4 SNGR 4 29 29 28 74 118 127 73 40 19 22 29 29
A5 CORN 5 29 29 28 22 60 73 93 106 109 99 29 29
A6 SUBT 6 29 29 28 22 58 95 106 120 111 102 29 29
A7 POTA 7 29 29 28 22 30 42 88 131 134 22 29 29
A8 ORCH 8 64 74 86 98 108 113 111 106 99 90 78 65
A9 PEAS 9
A10 TOMA10 29 29 28 45 50 75 101 97 83 40 29 29
A11 SMTR11 29 29 28 37 62 77 82 78 81 40 29 29
A12 IDLE12
A13 BEAN13 29 29 28 22 67 111 89 75 20 25 29 29
A14 BLAN14
C1 HWHC 1 185 185 185 185 185 185 185 185 185 185 185
C2 HWHG 2 65 80 113 136 141 142 141 136 125 102 75
C3 MWGT 3 58 53 53 55 61 68 77 82 83 81 76 69
C4 LWGT 4 35 33 33 34 38 42 48 51 51 50 47 42
B1 OPWT 5 101 130 149 156 155 151 144 141 138 137 128 112
UR URBN 6
B1 OPWT 5 100 100 100 100 100 100 100 100 100 100 100
3          SUBBASIN DATA IN OP AND PRINT
EVANSTON
1 EVANS 7 1 2599 2 8823 3 19835 4 314
1 EVANS 7
1 EVANS 8 1 632 2 609 3 3523 4 261 5 2434
90 38 100 00 70 79 00 3200 2400 159 2000 200
1000 700 1100 20 00 00 00 00 00 00 250 250
1 1 1 2 2 5
(10X12F4.1)
1TR 4 221 242 247 406 497 548 652 593 537 438 344 174
1TR 5 122 147 203 342 473 549 621 630 521 420 229 204
1TR 6 202 107 252 355 483 589 626 569 531 397 223 166
(10X12F4.2)
1A 4 69 34 75 14 78 143 111 160 70 89 142 73
1A 5 57 81 49 19 129 115 137 115 128 40 82 180
1A 6 121 35 7 39 232 67 71 38 2 94 14 83
(10X12F5.0)
1 1954 5 492 555 881 2970 1430 2040 202 77 53 70 170 160
1 1955 5 165 147 194 3870 2070 1880 163 103 52 75 222 1080
1 1956 5 645 488 2560 2170 3720 652 266 216 43 68 181 145
(8X12F6.0)
1-4 54 0 0 0 10524 36833 34202 11129 3394 2500 2631 0 0
1-4 55 0 0 0 0 36964 41595 11260 5551 2789 2631 0 0
1-4 56 0 0 0 0 21047 44726 17154 5157 2157 3157 0 0
1-4 54
1-4 55
1-4 56
(8X12F6.0)
020554 4000 3870 4960 12520 24520 5380 654 38 0 63 423 1800
020555 2640 2400 1580 9510 28740 20530 424 136 0 214 2010 7800
020556 5980 4830 14500 14880 57090 37330 1310 57 0 9 1360 2750
019554 0 20 2350 2200 3450 1870 112 0 0 110 603 392
019555 0 0 1380 4660 3670 3840 23 80 2 102 599 8
019556 0 0 984 2050 3040 4050 531 0 0 242 1120 0
(8X12F6.0)
010554 0 0 0 54 1090 1010 1260 562 545 427 90 0
010555 0 0 0 0 333 1360 1210 494 778 718 0 0
010556 0 0 0 0 0 1520 1650 1060 535 530 0 0
011554 2340 2220 2500 7660 34180 15670 6120 2300 2200 1970 1930 2030
011555 1950 1720 1900 3360 37470 33100 6740 3870 2010 2010 2050 2430
011556 2150 1830 2370 6900 52640 50910 9460 2750 1420 2080 2200 2190
012054 492 500 536 2250 6110 1540 431 238 293 354 386 341
012055 328 305 367 802 6960 3490 557 460 314 404 458 641
012056 500 430 652 2650 10780 4960 627 410 272 407 449 440
016054 492 555 881 2970 1430 2040 202 77 53 70 173 158
016055 165 147 194 3870 2070 1880 163 103 52 75 222 1080
016056 645 488 2560 2170 3720 652 266 216 43 68 181 145
017054 0 26 181 758 533 80 0 0 0 0 0 0
017055 0 0 0 743 1400 233 5 6 0 0 0 0 231
017056 123 86 548 1320 2420 270 0 0 0 0 0 0
5          OPTIMAL VERIFICATION OP ONLY
1 1
80 30 100 00 20 02 00 3100 2300
90 50 100 00 70 07 00 3300 2600
3 5 1 1 5 5 1 4 6
1000 100 800 00 00 00 00 00 00 00 250 200
1000 700 1200 40 00 00 00 00 00 00 250 400
1 6 4 4 1 1 1 1 1 4
90 38 100 00 70 03 00 3200 2400
1000 700 1100 20 00 00 00 00 00 00 250 250

```

GROUP 1 CONTROL CARD

GROUP 2 CARDS-BASIC DATA
READ BY SUBROUTINE BASIC

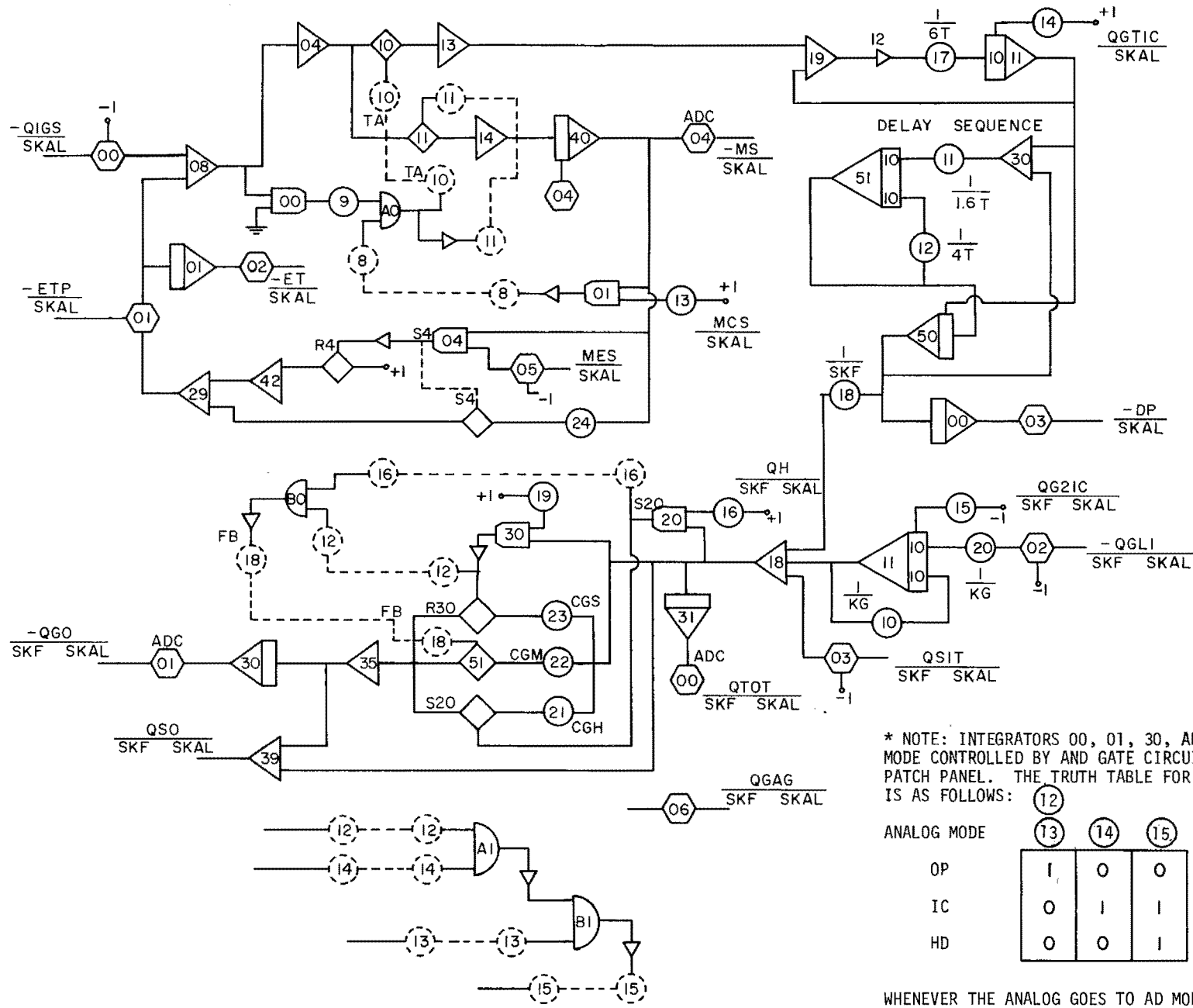
GROUP 1 CONTROL CARD

GROUP 3 CARDS
SUBBASIN HYDROLOGIC DATA,
READ BY SUBROUTINE SUBDAT

GROUP 1 CONTROL CARD

GROUP 4 CARDS-PATTERN
SEARCH SPECIFICATIONS
READ BY OPVER

Figure B.4. List of typical input data for OPVER.



* NOTE: INTEGRATORS 00, 01, 30, AND 31 HAVE IC MODE CONTROLLED BY AND GATE CIRCUIT ON THE LOGIC PATCH PANEL. THE TRUTH TABLE FOR THIS CIRCUIT IS AS FOLLOWS:

	12	13	14	15
ANALOG MODE				
OP	1	0	0	
IC	0	1	1	
HD	0	0	1	

WHENEVER THE ANALOG GOES TO AD MODE, INTEGRATORS 00, 01, 30, AND 31 GO TO IC MODE.

Figure B.5. Analog computer program for use with OPVER.

```

C OPTIMAL VERIFICATION BY MODIFIED PATTERN SEARCH = OPVER
REAL MTC,MS,MES
COMMON WKC(14,12),WK(12),POL(12),N(8),OO(12),FMT(10),CVR(8),
IV(13),A(10),BASIO(10),PV(15),DUM( 3,12,8),PKC(7,12),SHKC(12),
2SPKC(12),I1(14),OCA(14),CAC(14),PCA(14),PAC(7),PPA(7),OUT(13,21)
3,DIG(10),RES(10),RESC(10),ROUT(4,10,2),XIM(21)
4,MTC,MS,EHS2,SKAL,SKF,XIN(8,21),PH(21),PL(21),DR(21),NP(21)
COMMON INP,TDUT,MSB,LYRD,NYR,IRES,WANG,IRES,CTM,CONV1,CONPV
1,MES,SKAL1,SKAL2,SKAL3,SPAC,SCAC,NYB,K(12),CHS,BAREA
CALL QSHYIN(ITER,580)
CALL QSC(1,ITER)
OO 65 L=1,12
65 W(L)=1.0
1 TYPE 200
200 FORMAT(5HMAIN 1/)
OCT 25000
100 FORMAT(10I5)
READ(6,100)ITY
IF(ITY)99,99,2
2 GOTO(5,6,7,8,9),ITY
C ITY=1 OPERATE AS ORIGINAL PROGRAM RETURN AFTER 30
C 2 INITIAL DATA ONLY
C 3 SUBBASIN DATA IN OP AND PRINT
C 4 OPERATE AND PRINT
C 5 OPTIMAL VERIFICATION OPERATE ONLY
5 IENT=1
IRET=0
J .88
6 IENT=1
IRET=1
J .80
7 IENT=2
IRET=2
J .88
8 IENT=3
IRET=2
J .88
C READ NO OF PHASES (NPH) AND OPTIONS FOR READING XIN (NPR)
C AND WEIGHTING COEFFICIENTS (NWC)
9 READ(6,100)NPH,NPR,NWC
IF NWC > 0 READ MONTHLY WEIGHTING COEFFICIENTS FOR OBJ
IF(NWC .GT. 0) READ(6,101)W(L),L=1,12)
C INPUT DIG BOUNDS AND LEVELS
READ(6,101)PL(L),L=1,9)
READ(6,101)PH(L),L=1,9)
READ(6,101)NP(L),L=1,9)
101 FORMAT(12F6,2)
C INPUT BOUNDS FOR ANALOG
11 READ(6,101)PL(L),L=10,21)
READ(6,101)PH(L),L=10,21)
READ(6,100)NP(L),L=10,21)
C COMPUTE INCREMENTS
DO20L=1,21
XL=NP(L)
XIM(L)=PL(L)
XIN(L)=PH(L)
20 OR(L)=[PH(L)-PL(L)]/XL
IF NPR GT 0 INPUT XIN(1,L)
LA NPR
A /0
OCT 027407
J .13
READ(6,101)(XIN(1,L),L=1,9)
READ(6,101)(XIN(1,L),L=10,21)
C SET XIM AT INITIAL VECTOR
DO 14 L=1,21
14 XIM(L)=XIN(1,L)
13 WRITE(6,102)
102 FORMAT(1M1,9X,36HPR NP PH PL XIN DO///)
OO21L=1,21
21 WRITE(6,103)L,NP(L),PH(L),PL(L),XIN(1,L),DR(L)
103 FORMAT(7X,214,4F8.3)
WRITE(6,100)
108 FDRMAT(1M1)
ROBJ=50000.0
ROBA=0.0
DO FOR EACH PHASE
25 DO70K=1,NPH
C SET ALL PARAMETERS TO INITIAL LEVEL AND OPERATE
C DIGITAL
OO 27 L=1,9
27 DIG(L)=XIN(K,L)
C ANALOG
DO 28L=10,21
VAL=XIN(K,L)
CALL POTST(L,VAL)
28 CONTINUE
C OPERATE WITH PHASE INITIAL DATA
CALL HYDSM(3,3,OBJ,DBA)
104 FORMAT(1M0,F10.2,F6.2,9F7.3)
WRITE(6,104)OBJ,DBA,(XIN(K,L),L=1,9)
WRITE(6,101)(XIN(K,L),L=10,21)
WRITE(6,104)ROBJ,ROBA,(XIM(L),L=1,9)
WRITE(6,101)(XIM(L),L=10,21)
C CHECK ROBJ AGAINST OBJ OF XIN(K,L)
IF(OBJ-ROBJ)160,170,170
160 ROBJ=OBJ
ROBA=ROBA
J .100
170 IF(K=1)171,171,175
171 ROBJ=OBJ
ROBA=ROBA
J .180
175 DO 176 L=1,21
176 XIN(K,L)=XIN(L)
C RESET PARAMETERS TO XIM
DIGITAL
OO 177 L=1,9
DIG(L)=XIN(K,L)
ANALOG
DO 178 L=10,21
VAL=XIN(K,L)
CALL POTST(L,VAL)
178 CONTINUE
C OPERATE WITH BEST VECTOR
100 WRITE(6,100)
CALL HYDSM(3,2,ROBJ,ROBA)
WRITE(6,104)ROBJ,ROBA,(XIN(K,L),L=1,9)
WRITE(6,101)(XIN(K,L),L=10,21)
106 FORMAT(1M04X1M4X1M5X3HPR13X3HOB15X3HDBA15X4HGRAD/)
WRITE(6,106)
C DO FOR EACH PARAMETER
35 DO00I=1,21
XIN(K+1,I)=XIN(K,I)
PAR=PL(I)
NT=NP(I)+1
IF(NP(I).LE.1)NT=1
C DO FOR EACH LEVEL
38 DO 50 J=1,NT
IF(I=9)40,40,41
40 DIG(I)=PAR
J .45
41 CALL POTST(I,PAR)
45 CALL HYDSM(3,3,OBJ,DBA)
IF(J=1)55,55,56
55 GRAD=0.
POBJ=OBJ
OBJ1=OBJ
GO TO 57
56 GRAD=(OBJ-OBJ1)/DR(I)
OBJ1=OBJ
57 WRITE(6,107)I,J,PAR,OBJ,OBJ,GRAD
107 FORMAT(1X215,F10.3,3F18.5)
C CHECK OBJECTIVE FUNCTION IMPROVEMENT
IF(OBJ-POBJ)46,46,48
46 POBJ=OBJ
POBA=POBA
XIN(K+1,I)=PAR
C CHECK OBJ AGAINST MINIMUM ROBJ
IF(OBJ-ROBJ)140,48,48
140 ROBJ=OBJ
ROBA=ROBA
OO 150 L=1,21
150 XIM(L)=XIN(K,L)
XIM(I)=PAR
48 PAR=PAR+DR(I)
50 CONTINUE
C RESET PARAMETERS
IF(I=9)52,52,53
52 DIG(I)=XIN(K,I)
J .80
53 VAL=XIN(K,I)
CALL POTST(I,VAL)
50 CONTINUE
WRITE(6,100)
70 CONTINUE
C END OF ALL PHASES OPERATE AND PRINT LAST TIME
K=NPH+1
C SET ALL PARAMETERS TO INITIAL LEVEL AND OPERATE
DIGITAL
DO 127 L=1,9
127 DIG(L)=XIN(K,L)
ANALOG
DO128L=10,21
VAL=XIN(K,L)
CALL POTST(L,VAL)
128 CONTINUE
C OPERATE AND RETURN OBJ
CALL HYDSM(3,2,OBJ,DBA)
WRITE(6,104)OBJ,ROBA,(XIN(K,L),L=1,9)
WRITE(6,101)(XIN(K,L),L=10,21)
WRITE(6,104)ROBJ,ROBA,(XIM(L),L=1,9)
WRITE(6,101)(XIM(L),L=10,21)
IF(OBJ-ROBJ)240,240,200
200 DO 200 L=1,21
200 XIN(K,L)=XIM(L)
C RESET PARAMETERS TO XIM
DIGITAL
DO 227 L=1,9
227 DIG(L)=XIN(K,L)
ANALOG
DO228L=10,21
VAL=XIN(K,L)
CALL POTST(L,VAL)
228 CONTINUE
240 WRITE(6,100)
C OPERATE AND PRINT WITH FINAL DATA
CALL HYDSM(3,2,OBJ,DBA)
WRITE(6,104)OBJ,ROBA,(XIN(K,L),L=1,9)
WRITE(6,101)(XIN(K,L),L=10,21)
WRITE OUT XIN TABLE
WRITE(6,201)
201 FORMAT(1M1,32X,3HXIN/10X,3H I/)
NPP=NPH+1
OO 78 I=1,21
78 WRITE(6,202)I,(XIN(I),L=1,NPP)
202 FDRMAT(10X,13,6F7.3)
J .1
80 CALL HYDSM(IENT,IRET,OBJ,DBA)
J .1
99 STOP
END

```

Figure B. 6. List of digital computer program OPVER with all subroutines.

```

C HYDROLOGIC SIMULATION MODEL = SUBROUTINE HYOSH
SUBROUTINE HYOSH(IENT,IRET,OBJ,OBJA)
REAL MIC,MS,K5,K6,MS,MCS,NETPH
COMMON MKC(14,12),WK(12),POL(12),N(8),OD(12),PMT(10),CVR(8),
1V(13),A(10),BASID(10),PV(13),DUM( 3,12,8),PKC(7,12),SKKC(12),
2SPKC(12),I(14),DCA(14),CAC(14),PCA(14),PAC(7),PPA(7),OUT(13,21)
3DIG(10),RES(10),RESC(10),ROUT(4,13,2),XIM(21)
4MIC,MS,EMS2,SKAL,SKF,AIN(8,21),PH(21),PL(21),DR(21),NP(21)
COMMON INP,IOUT,N8B,LYRO,NYR,IRES,HANG,JRES,CTM,CONV,CONV1,CONPV
1,MS,SKAL1,SKAL2,SKAL3,SPAC,SCAC,NY8,N(12),CNS,BAREA
DIMENSION P(15),VARLB(21)
DATA P(1),P(2),P(3),P(4),P(5),P(6),P(7),P(8),P(9),P(10),P(11),
1P(12),P(13),P(14),P(15),VARLB(21)/4HP010,4HP011,4HP012,4HP013,
24HP014,4HP015,4HP016,4HP017,4HP018,4HP019,4HP020,4HP021,4HP022,
34HP023,4HP024,4HOIFF/
C OPT VER EXTRACT
  NLL=21
  GOTO(7,8,15),IENT
7 TYPE 210
510 FORMAT(7HMYDSM=1/)
  OCT 25000
  DD 2 I=1,10
2 A(I)=0.
  CALL QWBDAR(A,0,0,IERR)
  CALL QSTDA
  CALL QRBADR(A,0,10,IERR)
C INP IS INPUT DEVICE, IOUT IS OUTPUT DEVICE, N8B IS NO OF SUB-
C BASINS LYRO IS THE BEGINNING YEAR OF SIMULATION AND NYR IS THE NO
C OF YEARS
CSR CALL BASIC(VARLB)
CSR WRITE(6,207)
  IF(IRET.EQ.1)RETURN
  INITIALIZE ORIV AND OGDI
C OPT VER EXTRACT
  DD 3 J=1,NYR
  DD 1 K=1,12
  DUM(J,K,6)=0.
  1 DUM(J,K,7)=0.
  3 CONTINUE
C REPEAT PROCEDURES FOR EACH SUB-BASIN
  DD 30 I=1,N8B
CSR 24 CALL SUBOAT(P,VARLB,I)
CSR WRITE(IOUT,207)
207 FORMAT(1M1)
C IF SSW B ON DO ALL NYR YEARS BEFORE PARAMETER CHANGES
C BYPASS SSW A,D AND G
C IF SSW D ON PAUSE EVERY YEAR TO ALLOW SETTING SSW A FOR RERUNS
  SNM2=DIG(10)
  EMS2=MS
14 TYPE 245
245 FORMAT(6HRESET 08)
  OCT 25000
C ENTRY POINT FOR OPT VER
15 PHIC=MIC*SKAL1
  PHES=MS*SKAL1
  CALL QWJDAR(PHIC,04,IERR)
  CALL QWJDAR(PHES,05,IERR)
C INITIALIZE OBJECTIVE FUNCTION
  OBJ=0.0
  OBA=0.0
C SET ANALOG TO INITIAL MDOE
  CALL OSIC(IERR)
C REPEAT PROCEDURES FOR EACH YEAR
  DD 125 J=NYB,NYR
  IFF=1
  SNM1=DIG(10)
  EMS1=MS
C IF SSW D ON PAUSE EVERY YEAR TO ALLOW SETTING SSW A, C, AND E
C IF SSW B ON IGNORE SSW D
  OCT 023500
  OCT 023400
  J .160
106 FORMAT(5HSET A)
  TYPE 106
  OCT 025000
166 JJ=LYRO+J-1
  INITIALIZE ANNUAL VALUES
  DD 23 L=1,21
23 OUT(13,L)=0.
  STORMM=0.0
C REPEAT CALCULATIONS FOR EACH MONTH
  DD 28 K=1,12
  TEMP=DUM(J,K,1)
  PPT=DUM(J,K,2)
  QCOR=DUM(J,K,3)
  QGAG=DUM(J,K,8)
  QRIV=DUM(J,K,8)
  OGDI=DUM(J,K,7)
  DUT(K,2)=TEMP*PUL(K)
  EKT=.0173*TEMP+.314
  IF(EKT.LT.3) EKT=.3
  ETF=EKT*OUT(K,2)*DIG(3)
  ETP=SKKC(K)*ETF
  ETPH=SPKC(K)*ETF
  NETPH=NETPH+(SPAC/SCAC)
  RPMT=0.
  RPSM=PPT
  SNMT=0.
  IF(TEMP.GT.DIG(8))GOTO9
  OIG(10)=OIG(10)+PPT
  RPSM=0.
9 IF(TEMP.LT.DIG(9))GOTO10
  SNMT=DIG(10)*(1+EXP(-DIG(1)*(TEMP-OIG(9))))
  IF(OIG(10).LT.SNMT)SNMT=OIG(10)
  DIG(10)=DIG(10)-SNMT
10 RPMT=RPSM+SNMT
C MANAGEMENT STUDY CANAL DIVERSIONS
C PUT LEACHING WATER REED IN DUM(J,K,4)
  LA HANG
  A /0
  OCT 027410
  J .4
  QCNL=DUM(J,K,4)
  J .6
4 ETP1=ETP
  NLL=19
  DTM=TEMP-CTM
  LA DTM
  SKP
  J .35
  J .30
35 ETP1=0.0
36 ETN=ETP1-RPMT*(MS-CMS)
  IF(ETN.LT.0)ETN=0.
  QCNL=DUM(J,K,4)+ETN/DIG(2)
6 PC=(RPSM-DIG(7))*DIG(4)
  IF(PC.LT.0) PC=0
  SC=DIG(5)+SNMT
  QUNG=SC+PC*DIG(6)+QCOR
  QIN=QRIV+QUNG
  WAD=QIN-NETPH
  IF(HANG.LT.2) GO TO 87
  IF(WAD.LT.0)WAD=0.
  IF(QCNL.GT.WAD) QCNL=WAD
87 QDIV=DIG(2)+QCNL
  DIGS=RPMT+QDIV
  QSIT=WAD-QDIV
  A(1)=DIGS*SKAL1
  A(2)=ETP*SKAL1
  A(3)=OGDI*SKAL3
  A(4)=QSIT*SKAL3
  PGAG=OGAG*SKAL3
  CALL QWJOAR(PGAG,00,IERR)
C TRANSFER DATA FROM DIGITAL TO ANALOG
  CALL QWBDAR(A,00,4,IERR)
  CALL QSTDA
11 TEST SENSE LINE TO PROCEED COMPUTATIONS
  CALL QRLBB(ITEST,IERR)
  IF(ITEST.EQ.200) GO TO 11
12 CALL QRLRB(ITEST,IERR)
  IF(ITEST.NE.200) GO TO 12
  CALL QSOP(IERR)
13 CALL QRLBB(ITEST,IERR)
  IF(ITEST.EQ.200) GO TO 13
  CALL QRBADR(A,0,5,IERR)
  CALL QSM (IERR)
C TRANSFER RESULTS BACK TO DIGITAL
  QTO=A(1)*SKAL2
  QGO=A(2)*SKAL2
  ET=A(3)*SKAL
  DP=A(4)*SKAL
  MS=A(5)*SKAL
  QSO=QTO-QGO
C IF IRES GT 0 OPERATE RESERVOIR
  LA IRES
  A /0
  OCT 027410
  J .33
  J .34
33 CALL RESRV(J,K,QSO,ETF,IFF)
C OUTPUT THE RESULTS OF SIMULATION
C CALCULATE OUTPUT ARRAY IN INCHES
C ACCUMULATE SUMS FOR ANNUAL VALUES
34 CALL DOUT(OUT,K,1,TEMP)
  CALL DOUT(OUT,K,3,PPT)
  CALL DOUT(OUT,K,4,ORIV)
  CALL DOUT(OUT,K,5,QUNG)
  CALL DOUT(OUT,K,6,QCNL)
  CALL DOUT(OUT,K,7,QSIT)
  CALL DOUT(OUT,K,8,QIGS)
  CALL DOUT(OUT,K,9,OGDI)
  CALL DOUT(OUT,K,10,DIG(10))
  CALL DOUT(OUT,K,11,SNMT)
  CALL DOUT(OUT,K,12,ETPH)
  CALL DOUT(OUT,K,13,ETP)
  CALL DOUT(OUT,K,14,ET)
  CALL DOUT(OUT,K,15,MS)
  CALL DOUT(OUT,K,16,DP)
  CALL DOUT(OUT,K,17,QTO)
  CALL DOUT(OUT,K,18,QGO)
  CALL DOUT(OUT,K,19,QSO)
  CALL DOUT(OUT,K,20,OGAG)
  OXX=QSO-OGAG
  CALL DOUT(OUT,K,21,OXX)
  OUT(13,2)=OUT(13,2)+OUT(K,2)
C CALCULATE OBJ
  OBJ=OBJ+DUT(K,21)*OUT(K,21)*W(K)
C IF SSW D ON KEEP ORIV AND OGDI UNCHANGED
C IF SSW B ON DO SAME
  OCT 023500
  J .26
  J .20
26 OCT 023420
  J .21
  J .20
C IF SSW E ON USE RECORDED INFLOW FOR ORIV AND OGDI
21 OCT 023410
  J .22
  OUM(J,K,6)=0.0
  OUM(J,K,7)=0.0
  J .20
22 OUM(J,K,6)=QSO*CONV
  OUM(J,K,7)=QGO*CONV
29 CONTINUE
  OUT(13,1)=OUT(13,1)/12.
  OUT(13,10)=OUT(12,10)

```

Figure B. 6. (cont'd)

```

OUT(13,15)=OUT(12,15)
OUT(13,21)=OUT(13,19)+OUT(13,20)
OBA=OBA+OUT(13,21)
C   SKIP PRINTING IF DPT VER
   IF (IRET.EQ.3)GOTO75
   LL=1
76 WRITE(6,200) (BASIO(L),L=1,10),JJ
200 FORMAT(1X10A4,8I5)
225 FORMAT(1HG,7X3HVAR,7(7XA3))
WRITE(IOU,225) (V(K),K=1,6)
166 DO 88 L=1,NLL
226 FORMAT(7XA4,7F10.2)
88 WRITE(IOU,226)VARLB(L), (OUT(K,L),K=1,6)
WRITE(IOU,225) (V(K),K=7,13)
DO 85 L=1,NLL
85 WRITE(IOU,226)VARLB(L), (OUT(K,L),K=7,13)
IF (HANG.GT.0) GO TO 86
WRITE(6,209)O8, O8A
209 FORMAT(///1HG,10X,4HOBJ=F20.3/1H ,10X,4HOBAN=F20.3)
86 WRITE(IOU,207)
   IFF=2
   CALL RESRV(J,K,O8O,ETF,IFF)
   IFF=1
   IF (LL.75,75,77)
C   IF 88W C ON OUTPUT ACRE=FT TABLE
77 OCT 023440
   J .75
   LL=8
   DO 78 L=3,NLL
   DO 78 K=1,13
   IF (L=12)82,81,82
81 OUT(K,L)=CONPV+OUT(K,L)
   J .78
82 OUT(K,L)=CONV+OUT(K,L)
78 CONTINUE
   J .76
C   IF 88W A DN ENTER PARAMETER VALUE CHANGES ON TTY
C   IF 88W B DN AND J LT NYR SKIP CHANGES
75 CONTINUE
   IF (J.EQ.NYR)GOTO79
   J .125
79 NYB=1
   HIC=EMS2
   MS=EMS2
   DIG(10)=3NW2
C   RETURN POINT FOR OPT VER
206 IF (IRET.GT.1)RETURN
125 CONTINUE
30 RETURN
END

C   HYDROLOGIC SIMULATION OUTPUT ARRAY ALLOCATOR
SUBROUTINE OOUT(OUT,K,L,DX)
DIMENSION OUT(13,21)
OUT(K,L)=OXX
OUT(13,L)=OUT(13,L)+OXX
RETURN
END

C   BASIC DATA FOR B-C EVAPOTRANSPIRATION - SUBROUTINE BASIC
SUBROUTINE BASIC(VARLB)
REAL MIC,MS,MES
COMMON WK(14,12),WK(12),POL(12),N(8),DD(12),FMT(10),CVR(8),
1V(13),A(10),BASIO(10),PV(15),DUM( 3,12,8),PKC(7,12),SNKC(12),
2SPKC(12),I(14),OCA(14),CAC(14),PCA(14),PAC(7),PPA(7),DUT(13,21)
3,OIG(10),RES(10),RESC(10),ROUT(4,13,2),XIM(21)
4,MIC,MS,EMS2,SKAL,SKF,XIN(8,21),PH(21),PL(21),DR(21),NP(21)
COMMON INP,IOU,NSB,LYRO,NYR,RES,HANG,JRES,CTH,CONV,CONV1,CONPV
1,MES,SKAL1,SKAL2,SKAL3,SPAC,SCAC,NYB,4(12),CMS,BAREA
DIMENSION VARLB(21)

CSR
1 READ(6,100)INP,IOU,NSB,LYRO,NYR
100 FORMAT(16I5)
110 FORMAT(13(1XA3))
READ(6,110) (V(I),I=1,13)
111 FORMAT(20A4)
READ(6,111) (VARLB(I),I=1,20)
102 FORMAT(12F5.3)
READ(6,102) (POL(K),K=1,12)
C   READ USE COEFFICANTS
DO 52 I=1,14
52 READ(6,220) (WK(I,J),J=1,12)
220 FORMAT(10X12F5.2)
DO 53 I=1,7
53 READ(6,220) (PKC(I,J),J=1,12)
C   WRITE INITIAL DATA
WRITE(6,200)
WRITE(6,110) (V(I),I=1,13)
WRITE(6,111) (VARLB(I),I=1,20)
WRITE(6,102) (POL(K),K=1,12)
DO 500 I=1,14
500 WRITE(6,220) (WK(I,J),J=1,12)
DO 501 I=1,7
501 WRITE(6,220) (PKC(I,J),J=1,12)
CSR
206 FORMAT(1X10A4,8I5)
RETURN
END

C   SUBBASTN DATA INPUT - SUBROUTINE SUBDAT
SUBROUTINE SUBDAT(P,VARLB,I)
REAL MIC,MS,MES
COMMON WK(14,12),WK(12),POL(12),N(8),DD(12),FMT(10),CVR(8),
1V(13),A(10),BASIO(10),PV(15),DUM( 3,12,8),PKC(7,12),SNKC(12),
2SPKC(12),I(14),OCA(14),CAC(14),PCA(14),PAC(7),PPA(7),DUT(13,21)
3,OIG(10),RES(10),RESC(10),ROUT(4,13,2),XIM(21)
4,MIC,MS,EMS2,SKAL,SKF,XIN(8,21),PH(21),PL(21),DR(21),NP(21)
COMMON INP,IOU,NSB,LYRO,NYR,RES,HANG,JRES,CTH,CONV,CONV1,CONPV
1,MES,SKAL1,SKAL2,SKAL3,SPAC,SCAC,NYB,4(12),CMS,BAREA
DIMENSION P(15),VARLB(21)

CSR
24 TYPE 202,I
202 FORMAT(6HCAROS=,I3/)
C   OPT VER EXTRACT
OCT 25000
NYB=1
201 FORMAT(10A4,8I5)
C   OPT VER EXTRACT
READ(6,201) (BASIO(L),L=1,10),IRES,HANG,JRES,JCONV
C   IF IRES GT 0 INPUT RES PARAMETERS
IF (IRES.GT.0)READ(6,350) (RES(L),L=1,10)
C   IF HANG GT 0 READ MANAGEMENT PARAMETERS
IF (HANG.GT.0)READ(6,350) CTH,CMS,BAREA
C   IF JRES GT 0 READ CANAL RESERVOIR PARAMETERS
IF (JRES.GT.0)READ(6,350) (RESC(L),L=1,10)
350 FORMAT(10X10F7.0)
215 FORMAT(8F10.2)
C   INPUT CROP ACREAGES FOR BASIN
O8A=1,14
54 CAC(J)=O.0
221 FORMAT(10X,I3,F7.0,I3,F7.0,I3,F7.0,I3,F7.0,I3,F7.0,I3,F7.0,
I3,F7.0)
READ(6,221) (I(J),OCA(J),J=1,14)
SCAC=O.0
DO 55 J=1,14
L=I(J)
IF (L.LE.0)GOTO55
CAC(L)=OCA(J)
SCAC=SCAC+CAC(L)
55 CONTINUE
C   COMPUTE CROP PROPORTIONS
57 DO 50J=1,14
60 PCA(J)=CAC(J)/SCAC
C   INPUT PHREATOPHYTE ACREAGES
DO 61 J=1,7
61 PAC(J)=O.0
READ(6,221) (I(J),OCA(J),J=1,7)
SPAC=O.0
DO 62 J=1,7
L=I(J)
IF (L.LE.0)GOTO62
PAC(L)=OCA(J)
SPAC=SPAC+PAC(L)
62 CONTINUE
CONV=SCAC/12.
CONV1=12./SCAC
CONPV=SPAC/12.
C   COMPUTE PHREATOPHYTE PROPORTIONS
DO 66 J=1,7
66 PPA(J)=PAC(J)/SPAC
C   COMPUTE WEIGHTED USE CDEF.
CROPS
DO 70 J=1,12
SCKC=O.0
DO 89 L=1,14
89 SCKC=SCKC+WK(L,J)+PCA(L)
70 SNKC(J)=SCKC
PHREATOPHYTES
DO 72 J=1,12
SCKC=O.0
DO 71 L=1,7
71 SCKC=SCKC+PKC(L,J)+PPA(L)
72 SPKC(J)=SCKC
73 READ(6,104) (OIG(L),L=1,10),SKAL,SKF
IF (SKF.LE.0.)SKF=2.0
104 FORMAT(12F6.2)
READ(6,104) (PH(L),L=10,21)
HIC=PH(21)
MES=PH(20)
RMES=10.*MES-SKAL
LA RMES
SKP
J .30
RMES=SKAL-PH(12)
LA RMES
SKP
J .30
J .31
30 RMES=10.*MES
TYPE 105,PH(12),SKAL,RMES
105 FORMAT(11H SKAL ERROR,3F10.5/)
OCT 325000
J .73
31 MS=MIC
READ(6,100) (N(L),L=1,8)
C   OPT VER EXTRACT
WRITE(6,206) (BASIO(L),L=1,10)
C   OPT VER EXTRACT
WRITE(6,100) IRES,HANG,JRES,JCONV
100 FORMAT(13I5)
IF (IRES.GT.0)WRITE(6,224) (RES(L),L=1,10)
IF (HANG.EQ.0) GO TO 32
BCONV=BAREA/SCAC
OIG(4)=OIG(4)+BCONV

```

Figure B. 6. (cont'd)

```

DIS(5)=DIG(5)*BCONV
PH(15)=PH(15)*BCONV
PH(16)=PH(16)*BCONV
PH(17)=PH(17)*BCONV
PH(18)=PH(18)*BCONV
PH(19)=PH(19)*BCONV
WRITE(6,215) CTH,CH8,BAREA,BCONV
OPT VER EXTRACT
C
32 IF (JRES,GT,8) WRITE(6,224) (RE8C(L),L=1,10)
206 FORMAT(1X10A4,8I5)
WRITE(IOUT,222) (CAC(J),J=1,14),SCAC
222 FORMAT(1X7F9,0/1X8F9,0)
WRITE(IOUT,223) (PCA(J),J=1,14),CONV
223 FORMAT(1X,7F9,5/1X7F9,5)
WRITE(IOUT,222) (PAC(J),J=1,7),SPAC
WRITE(IOUT,223) (PPA(J),J=1,7),CONPV
WRITE(IOUT,224) (SWKC(J),J=1,12)
224 FORMAT(1X13F8,2)
WRITE(IOUT,224) (SPKC(J),J=1,12)
WRITE(IOUT,224) (DIG(L),L=1,10),SKAL,SKF
WRITE(6,224) (PH(L),L=10,21)
C
INITIALIZE DUM EXCEPT FOR DRIV AND OGLI
DO 88 II=1,NYR
DO 88 JJ=1,12
DUM(II,JJ,8)=0.
DO 88 J=1,5
88 DUM(II,JJ,J)=0.
C
READ DATA FOR BASIN I
IF (JCONV,GT,8) READ CONVERSION FACTORS FOR INPUT DATA
IF (JCONV,GT,8) READ(6,215) (CVR(J),J=1,8)
165 DO 97 J=1,8
NN=N(J)
IF (J=5) 232,232,235
232 IF (NN) 97,97,92
235 CVRS=CONV1
IF (J,EQ,8) CVRS=1.0
IF (NN) 91,91,92
92 READ(6,201) (FMT(L),L=1,10)
DO 94 L=1,NN
DO93II=1,NYR
READ(INP,FMT) (DD(JJ),JJ=1,12)
DO95JJ=1,12
95 DUM(II,JJ,J)=DUM(II,JJ,J)+DD(JJ)
93 CONTINUE
94 CONTINUE
IF (J=3) 16,17,17
C
OPT VER EXTRACT
16 NC=FLOAT(NN)
CVRS=1./NC
GOTO400
17 CVRS=CONV1
IF (J,EQ,8) CVRS=1.0
C
OPT VER EXTRACT
IF (JCONV,GT,8) USE CONVERSION FACTORS READ ON INPUT
400 IF (JCONV,GT,8) CVRS=CVR(J)
C
SCALE INPUT DATA TO INCHES
91 DO96II=1,NYR
DO98JJ=1,12
300 DUM(II,JJ,J)=DUM(II,JJ,J)+CVRS
C
OPT VER EXTRACT
C
IFSSW 8 ON PRINT INPUT DATA
L=LYRD+II=1
230 FORMAT(1X12,I3,12F6,2)
WRITE(IOUT,230) J,L,(DUM(II,JJ,J),JJ=1,12)
96 CONTINUE
97 CONTINUE
162 SKAL1=1./SKAL
SKAL2=SKF*SKAL
SKAL3=1./SKAL2
C
DETERMINE POT VALUES
CALL POT3T(22,SKF)
DO 19 L=10,21
VAL=PH(L)
CALL POT3T(L,VAL)
19 CONTINUE
WRITE(6,303)
303 FORMAT(41HPOTS 10 THRU 24 SHOULD BE SET AS FOLLOWS)
WRITE(6,302) (PV(L),L=1,15)
WRITE(6,301)
CALL QSPS(IERR)
DO 5 L=1,15
PADR=P(L)
CALL QPAR(PADR,PVAL,IERR)
5 PV(L)=PVAL
WRITE(6,302) (PV(L),L=1,15)
301 FORMAT(35HPOTS 10 THRU 24 ARE SET AS FOLLOWS )
302 FORMAT(1X5F8,5)
CSR
RETURN
END
C
POTENTIOMETER SETTING ALGORITHM - SUBROUTINE POTST
SUBROUTINE POTST(XP,XV)
REAL MIC,MS,MES
COMMON WKC(14,12),WK(12),POL(12),N(8),DD(12),FMT(10),CVR(8),
1V(13),A(10),BASID(10),PV(15),DUM( 3,12,8),PKC(7,12),SWKC(12),
2SPKC(12),II(14),OCA(14),CAC(14),PCA(14),PAC(7),PPA(7),OUT(13,21)
3,DIG(10),RES(10),RESC(10),ROUT(4,13,2),XIM(21)
4,MIC,MS,EMS2,SKAL,SKF,XIN(8,21),PH(21),PL(21),DR(21),NP(21)
COMMON INP,IOUT,NSB,LYRD,NYR,IRES,HANG,JRES,CTH,CONV,CONV1,CONPV
1,MES,SKAL1,SKAL2,SKAL3,SPAC,SCAC,NY8
DIMENSION PT(15)
DATA PT(1),PT(2),PT(3),PT(4),PT(5),PT(6),PT(7),PT(8),PT(9),PT(10),
1PT(11),PT(12),PT(13),PT(14),PT(15)
2 /4HP010,4HP011,4HP012,4HP013,4HP014,4HP015,4HP016,4HP017,
34HP018,4HP019,4HP020,4HP021,4HP022,4HP023,4HP024/
ITS=XP-9
GOTO(5,10,15,20,25,30,35,40,45,50,55,60,70),ITS
5 PVAL=1./XV
PV(1)=PVAL
PADR=PT(1)
CALL QMPR(PADR,PVAL,IERR)
PV(11)=PVAL
PADR=PT(11)
J .100
10 PVAL=1./((1.5*XV*XV)
PV(21)=PVAL
PADR=PT(2)
CALL QMPR(PADR,PVAL,IERR)
PVAL=1./((4.0*XV)
PV(3)=PVAL
PADR=PT(3)
CALL QMPR(PADR,PVAL,IERR)
PVAL=1./((6.0*XV)
PV(8)=PVAL
PADR=PT(8)
J .100
15 PVAL=XV/SKAL
PV(4)=PVAL
PADR=PT(4)
J .100
20 PVAL=XV/SKAL
PV(5)=PVAL
PADR=PT(5)
J .100
25 PVAL=XV/(SKAL*SKF)
PV(6)=PVAL
PADR=PT(6)
J .100
30 PVAL=XV/(SKF*SKAL)
PV(7)=PVAL
PADR=PT(7)
J .100
35 PVAL=XV/(SKF*SKAL)
PV(10)=PVAL
PADR=PT(10)
J .100
40 PVAL=XV
PV(12)=PVAL
PADR=PT(12)
J .100
45 PVAL=XV
PV(13)=PVAL
PADR=PT(13)
J .100
50 PVAL=XV
PV(14)=PVAL
PADR=PT(14)
J .100
55 PVAL=0.1*SKAL/XV
PV(15)=PVAL
PADR=PT(15)
J .100
60 EMS2=XV
MS=XV
MIC=XV
J .101
C
OPTION FOR SETING POT 10
70 PVAL=1./XV
PV(9)=PVAL
PADR=PT(9)
100 CALL QMPR(PADR,PVAL,IERR)
101 RETURN
END
C
RESERVOIR OPERATION ALGORITHM - SUBROUTINE RESRV
SUBROUTINE RESRV(J,K,QSD,ETF,IFF)
REAL MIC,MES,K9,KG,MS,MCS
COMMON WKC(14,12),WK(12),POL(12),N(8),DD(12),FMT(10),CVR(8),
1V(13),A(10),BASID(10),PV(15),DUM( 3,12,8),PKC(7,12),SWKC(12),
2SPKC(12),II(14),OCA(14),CAC(14),PCA(14),PAC(7),PPA(7),OUT(13,21)
3,DIG(10),RES(10),RESC(10),ROUT(4,13,2),XIM(21)
4,MIC,MS,EMS2,SKAL,SKF,XIN(8,21),PH(21),PL(21),DR(21),NP(21)
COMMON INP,IOUT,NSB,LYRD,NYR,IRES,HANG,JRES,CTH,CONV,CONV1,CONPV
1,MES,SKAL1,SKAL2,SKAL3,SPAC,SCAC,NY8
J IS YEAR,K IS MONTH,QSD IS SUBBASIN SURFACE OUTFLOW,
C
ETF IS MOD. B=C EVAP TEMP. FACTOR
C
IFF=1 OPERATE RESERVOIR RULES
C
IFF=2 PRINT JTH YEAR DATA
C
RETURN IF IRES =0
LA IRES
4 /8
OCT 027410
J .5
J .99
C
IFF=1 OPERATE
5 LA IFF
S /2
OCT 027402
J .70
C
IF 1ST MONTH OF 1ST YR INITIALIZE RESV AND EXTREMES
JJ=K+J
LA JJ
S /2
OCT 027410
J .7
STI=RES(1)
SMAX=STI
SMIN=STI
JNN=LYRD-1
JHX=JNN
KNN=12
MNX=12
IF 1ST 73
C
IF 1ST MONTH OF ANY YR INIT ANNUAL TOTALS
7 LA K
S /1

```

Figure B.6. (cont'd)

```

OCT 027410
J .9
DO B L=1,4
ROUT(L,13,2)=0.0
B ROUT(L,13,1)=0.0
C SET UP INITIAL MONTHLY VALUES
9 QIN=QSO*CONV
QR=DUM(J,K,8)
SI=STI
IC=0
EVAP=ETP*PKC(7,K)
DCS=DUM(J,K,2)=EVAP
C OPERATE RESERVOIR ITERATION
10 IC=IC+1
CALL AREA(SI,AR,RES)
11 OTS=QIN-QR+DCS*AR/12.0
ST=SI+OTS
C CHECK EDM ST AGAINST STMAX AND STMH
IF(ST.GT.RES(3))GOTO13
IF(ST.LT.RES(2))GOTO14
QR=QR
J .20
13 QRR=QR+ST-RES(3)
ST=RES(3)
J .20
14 QDM=RES(2)-ST
QDD=QR-QDM
IF(QDD.LT.0.0)GOTO15
QRR=QDD
ST=RES(2)
J .20
15 QRR=0
ST=RES(2)+QDD
IF(RES(3).LE.0.0)ST=0.0
C COMPUTE AVERAGE STORAGE FOR MONTH
20 SA=(ST+ST)/2.0
C COMPUTE AVE AREA FOR MONTH
CALL AREA(SA,AT,RES)
C CHECK AGAINST GUESSED AVERAGE
ER=RES(4)
AC=(AT-AR)/AR
AK=ABS(AC)
AC=ER-AK
LA AC
SKP
J .21
J .25
C CHECK ITERATIONS
21 ICC=IC-30
LA ICC
SKN
J .23
SI=SA
J .10
23 WRITE(6,100)SI,SA,ST
IC EXCEEDS 30
C 100 FORMAT(12H EXCESS ITER,3F20.3)
C SET UP FOR NEXT MONTH
25 QR=QRR
QSD=QR/CONV
C COMPUTE OUTPUT ARRAY
DA=ST/12.0
CALL RSDUT(1,K,1,ST,DA,ROUT)
DH=ST-STI
CALL RSDUT(2,K,1,DH,DH,ROUT)
DH=EVAP*AR/12.0
CALL RSDUT(3,K,1,DH,DH,ROUT)
DH=DUM(J,K,2)*AR/12.0
CALL RSDUT(4,K,1,DH,DH,ROUT)
CALL RSDUT(1,K,2,QIN,QIN,ROUT)
CALL RSDUT(2,K,2,QR,QR,ROUT)
CALL RSDUT(3,K,2,EVAP,EVAP,ROUT)
C INITIALIZE NEXT MONTHS ST
STI=ST
C CHECK EXTREMES
EMX=ST-SMAX
LA EMX
SKP
J .30
SMA=ST
JHX=L*YRO+J-1
KHX=K
J .33
30 EMN=SMIN-ST
LA EMN
SKP
J .33
SMIN=ST
JMN=L*YRO+J-1
KMN=K
33 RETURN

C IFF=2 PRINT RES DATA
70 JR=L*YRO+J-1
WRITE(6,102)(BASID(L),L=1,10),JR
102 FORMAT(1X10A4,15///10X,22HRESERVOIR DATA (AC=FT))
WRITE(6,103)(V(L),L=1,6)
103 FORMAT(/4XSHMONTH,7(7X3))
WRITE(6,104)(ROUT(1,K,1),K=1,6)
WRITE(6,105)(ROUT(2,K,1),K=1,6)
WRITE(6,106)(ROUT(3,K,1),K=1,6)
WRITE(6,107)(ROUT(4,K,1),K=1,6)
WRITE(6,108)(ROUT(1,K,2),K=1,6)
WRITE(6,109)(ROUT(2,K,2),K=1,6)
WRITE(6,110)(ROUT(3,K,2),K=1,6)
WRITE(6,103)(V(L),L=7,13)
WRITE(6,104)(ROUT(1,K,1),K=7,13)
WRITE(6,105)(ROUT(2,K,1),K=7,13)
WRITE(6,106)(ROUT(3,K,1),K=7,13)
WRITE(6,107)(ROUT(4,K,1),K=7,13)
WRITE(6,108)(ROUT(1,K,2),K=7,13)
WRITE(6,109)(ROUT(2,K,2),K=7,13)
WRITE(6,110)(ROUT(3,K,2),K=7,13)
104 FORMAT(/2X8HSTORAGE ,/2X8HAT EDM ,7F10.0)
105 FORMAT(/2X8HCHANGE ,/2X8HIN STOR ,7F10.0)
106 FORMAT(/2X8HEVAP ,/2X8HVOLUME ,7F10.0)
107 FORMAT(/2X8HPRECIP ,/2X8HVOLUME ,7F10.0)
108 FORMAT(/2X8H ,/2X8HINFLOW ,7F10.0)
109 FORMAT(/2X8H ,/2X8HOUTFLOW ,7F10.0)
110 FORMAT(/2X8HEVAP ,/2X8H(INCHES),7F10.0)
C J=NYR WRITE EXTREMES
JE=NYR-J
LA JE
A /0
OCT 027410
J .75
WRITE(6,120)J,SMAX,V(KHX),JHX
120 FORMAT(/10X15HMAX STORAGE FOR,13,7H YEARS=,F10.0,5HAC=FT,2X3,15)
121 FORMAT(/10X15HMIN STORAGE FOR,13,7H YEARS=,F10.0,5HAC=FT,2X3,15)
75 LA JRES
A /0
OCT 027410
J .99
WRITE(6,125)
125 FORMAT(1M1)
99 RETURN
END

C RESERVOIR OPERATION OUTPUT ARRAY ALLOCATOR
SUBROUTINE RSDUT(L,K,N,DH,DA,ROUT)
DIMENSION ROUT(4,13,2)
ROUT(L,K,N)=DH
ROUT(L,13,N)=ROUT(L,13,N)+DA
RETURN
END

C RESERVOIR SURFACE AREA ALGORITHM = SUBROUTINE AREA
SUBROUTINE AREA(SI,AR,RES)
DIMENSION RES(10)
IF(SI.LT.0.0)GOTO10
IF(SI.LT.RES(8))GOTO1
C2=RES(10)
AR=RES(9)+SI**C2
J .12
1 C2=RES(7)
AR=RES(6)+SI**C2+RES(5)
J .12
10 AR=RES(5)
12 RETURN
END

```

Figure B. 6. (cont'd)

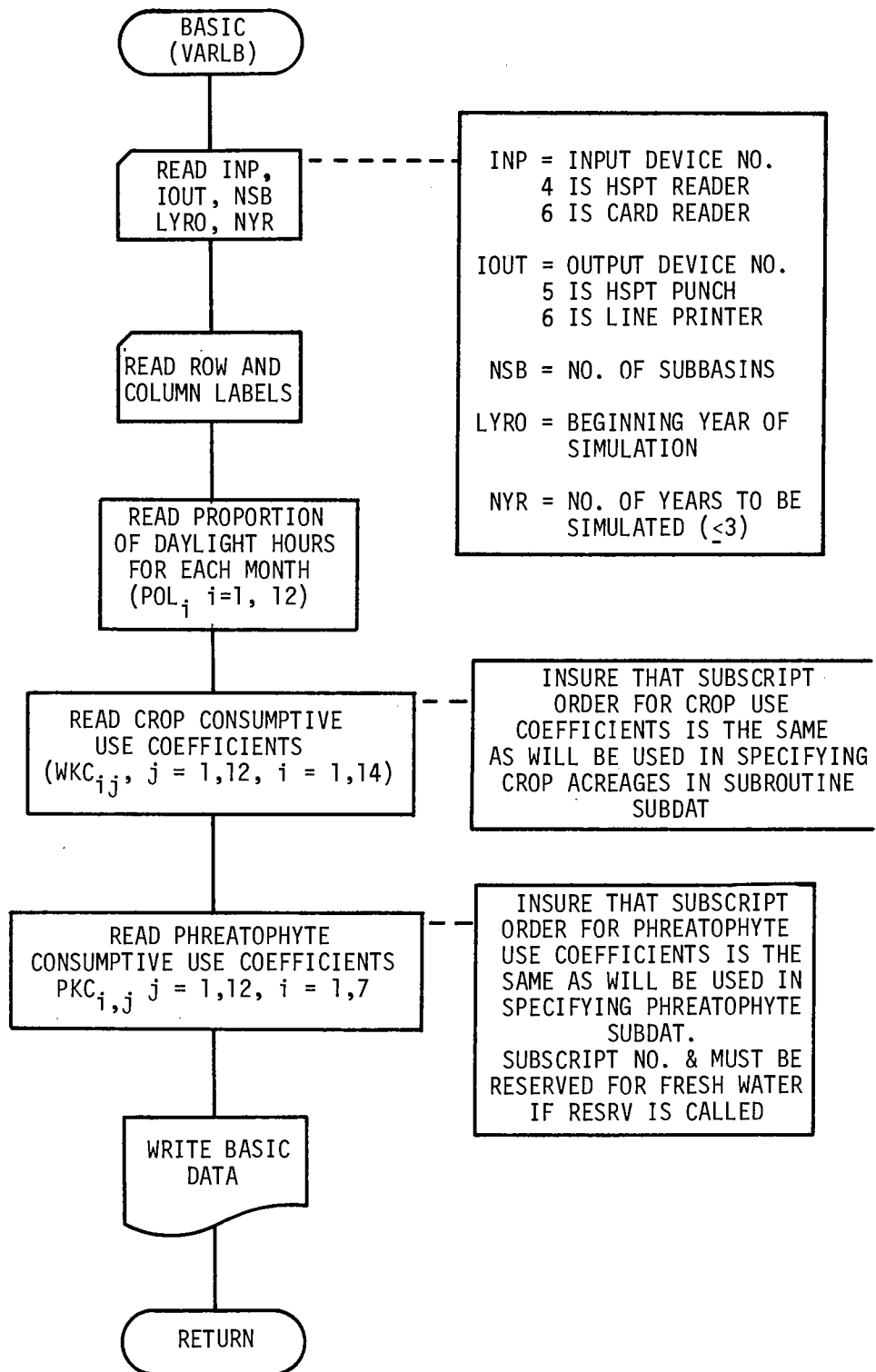


Figure B.8. Flow chart of subroutine BASIC.

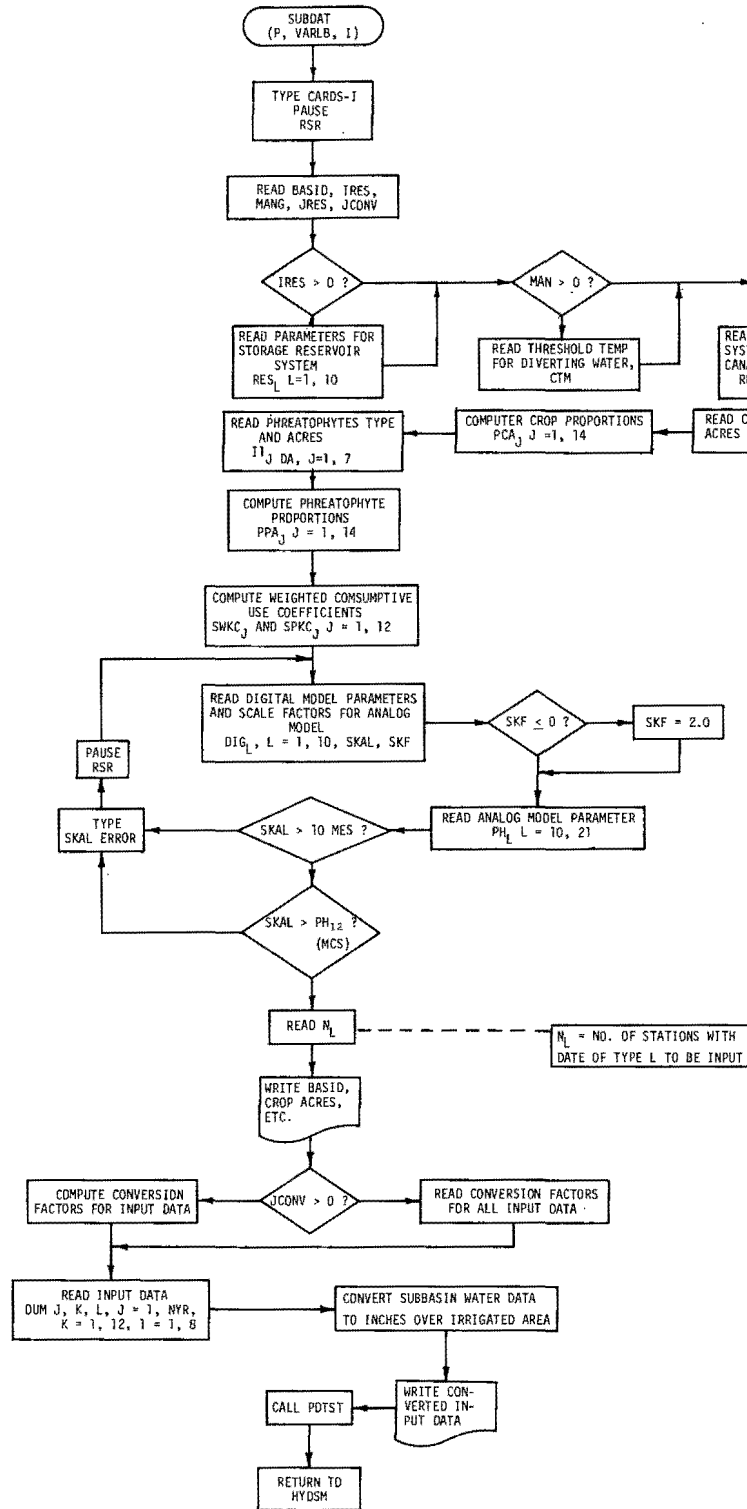


Figure B.9. Flow chart of subroutine SUBDAT.

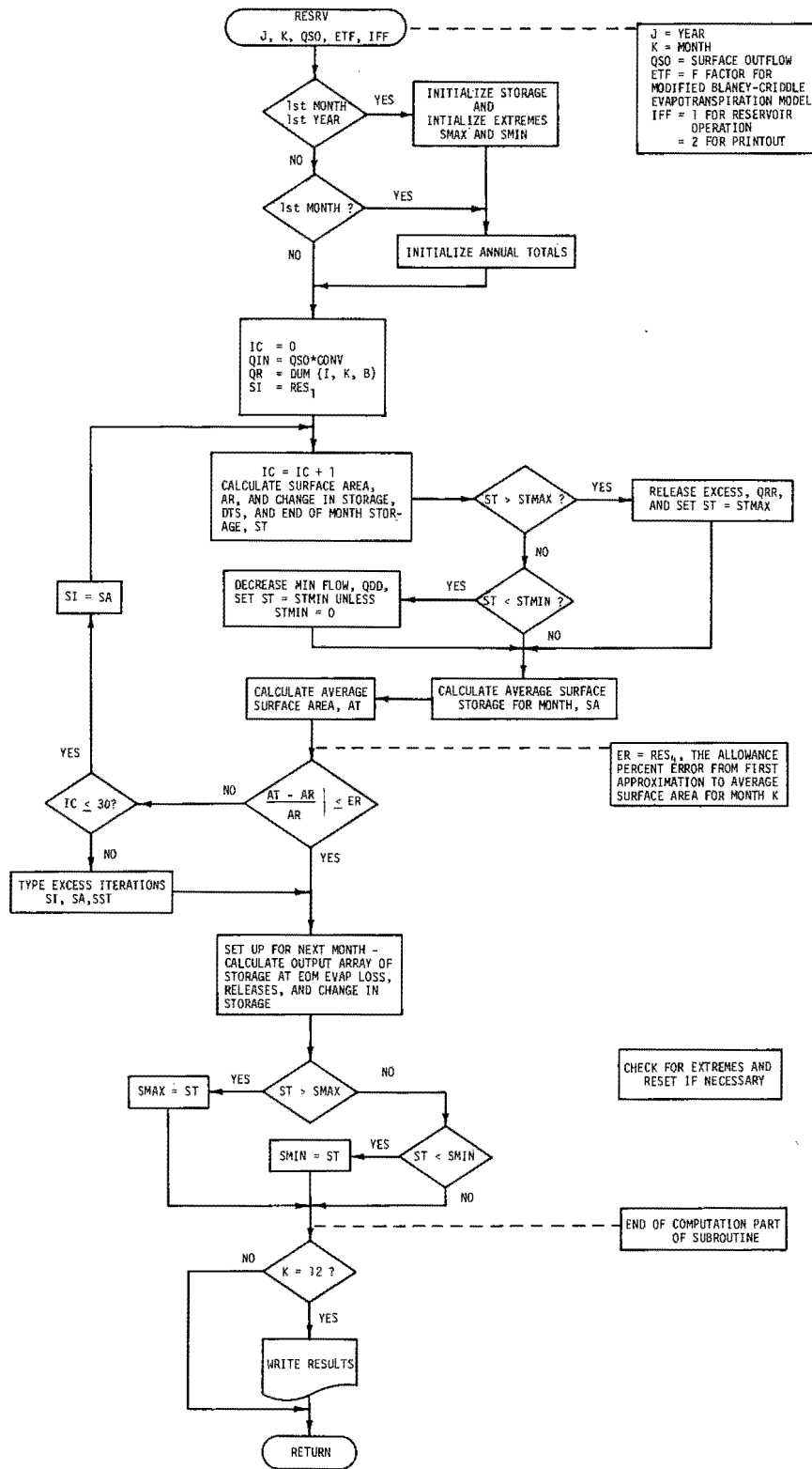


Figure B.10. Flow chart of subroutine RESRV.

APPENDIX C

MODIFIED INPUT DATA,
MODEL COEFFICIENTS, AND
OUTPUT DATA

APPENDIX C

MODIFIED INPUT DATA, MODEL COEFFICIENTS, AND OUTPUT DATA

This appendix includes modified input data, model variable values for each subbasin, and model output for each subbasin. The first printout page lists the modified input data and the coefficients for the subbasin. Modified data includes the input data from Appendix A but in a scaled and summed, where necessary, form. The next three printout pages list the subbasin outputs for the three modeled years. Four printout pages are listed on one page of text in this appendix. The modified input data and the output data for one subbasin occupies one page of text.

The modified input data pages list the name of the subbasin on the first line and indicate the use of program options on the second line. The third and fourth lines list the acreages of the crops in the subbasin according to the land use table and the total crop acreage. The fifth and sixth lines give the fraction of the total crop acreage for each crop. The seventh line lists a conversion factor for converting inches over the total crop area to acre-feet. The

eighth line lists acreage for each phreatophyte. The ninth line gives the total phreatophyte acreage. Lines ten and eleven list the fraction of total phreatophyte acreage for each phreatophyte and the conversion factor from inches over the phreatophyte acreage to acre-feet. Lines twelve and thirteen give weighted values for crop and phreatophyte consumptive use coefficients. Lines fourteen and fifteen are the verified values of the model variables. The next twenty-four lines represent the input data for the years of modeling, in this case 1954, 1955, and 1956. The input data beginning with number one are temperature, precipitation, streamflow for correlation purposes, canal diversion, gaged outflow, gaged river inflow, groundwater inflow, and reservoir storage or a dummy variable for any desired data. The last two groups of data are the calculated and actual potentiometer settings. The variables listed on the output data printouts are defined in Appendix B and are given here in units of acre-feet. The variables are given for each month and an annual summary or average.

EVANSTON												
0	0	0	0	0	0	0	0	0	0	0	0	0
2599.	8823.	19835.	314.	0.	0.	0.	0.	0.	0.	0.	0.	31571.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
08232.	27946.	62826.	00994.	00000.	00000.	00000.	00000.	00000.	00000.	00000.	00000.	00000.
00000.	00000.	00000.	00000.	00000.	00000.	00000.	00000.	00000.	00000.	00000.	00000.	00000.
32030.916	632.	609.	3523.	261.	2434.	0.	0.	0.	0.	0.	0.	0.
7459.	08472.	08164.	47231.	03499.	32631.	00000.	00000.	00000.	00000.	00000.	00000.	00000.
621.58325	.35	.06	.80	.01	1.07	1.10	1.04	1.00	.92	.82	.75	.69
	.81	.90	.99	1.04	1.07	1.10	1.12	1.13	1.12	1.10	1.03	.92
	.90	.38	1.00	.00	.78	.79	.00	32.00	24.00	1.59	20.00	2.00
	10.00	7.00	11.00	.20	.00	.00	.00	.00	.00	2.50	2.00	.00
1 1954	22.18	24.28	24.78	48.88	49.78	54.88	55.28	59.38	53.78	43.88	34.48	17.48
1 1955	12.28	14.78	29.38	34.28	47.38	54.98	62.18	63.00	52.18	42.00	22.98	20.48
1 1956	20.28	10.78	28.28	35.58	46.38	55.98	62.88	50.98	53.18	39.78	22.38	16.68
2 1954	.69	.34	.75	.14	.78	1.43	1.11	1.60	.70	.80	1.42	.73
2 1955	.57	.81	.49	.19	1.29	1.15	1.37	1.15	1.28	.40	.82	1.00
2 1956	1.21	.35	.87	.39	2.32	.87	.71	.38	.82	.94	.14	.83
3 1954	.18	.21	.33	1.12	.54	.77	.87	.82	.82	.82	.86	.86
3 1955	.08	.08	.07	1.47	.78	.71	.86	.83	.81	.82	.86	.41
3 1956	.24	.18	.97	.82	1.41	.24	.18	.08	.81	.82	.83	.85
4 1954	.08	.08	.00	4.00	14.00	13.00	4.23	1.29	.95	1.00	.00	.00
4 1955	.08	.08	.00	14.94	15.81	4.27	2.10	1.06	1.08	.00	.00	.00
4 1956	.08	.08	.00	8.00	7.99	17.00	6.52	1.96	.81	1.19	.00	.00
5 1954	1.52	1.47	2.77	5.59	10.63	2.75	.29	.01	.88	.86	.39	.83
5 1955	1.00	.91	1.12	5.38	12.31	9.26	.16	.08	.88	1.12	.99	2.98
5 1956	2.27	1.83	5.06	6.43	22.85	15.72	.89	.82	.00	.89	.94	1.84
6 1954	1.26	1.25	1.55	5.20	16.46	7.73	3.84	1.20	1.17	1.07	.98	.96
6 1955	.92	.82	.93	3.33	16.33	15.22	3.29	1.87	1.19	1.21	1.83	1.86
6 1956	1.29	1.87	2.33	4.95	26.43	22.18	4.86	1.68	.88	1.17	1.04	1.65
7 1954	.08	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
7 1955	.08	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
7 1956	.08	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1954	.08	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1955	.08	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1956	.08	.08	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

POTS 18 THRU 24 SHOULD BE SET AS FOLLOWS
 .10000 .01275 .03871 .54999 .01000
 .00000 .00000 .02380 .50000 .00000
 .10000 .00000 .00000 .00000 .79999

POTS 19 THRU 24 ARE SET AS FOLLOWS
 .10000 .01275 .03871 .54999 .00994
 .00000 .00000 .02374 .49975 .00000
 .10015 .00000 .00000 .00000 .79988

EVANSTON												
VAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
TEMP	22.10	24.22	24.78	48.60	40.78	54.88	54.88	54.88	54.88	54.88	54.88	54.88
PPT	1.45	1.02	2.85	3.65	5.81	5.88	5.88	5.88	5.88	5.88	5.88	5.88
PRV	1815.33	594.51	1973.18	368.32	2892.11	3762.28	3762.28	3762.28	3762.28	3762.28	3762.28	3762.28
QUNG	3323.99	3388.99	4097.99	13691.99	43322.98	20339.99	20339.99	20339.99	20339.99	20339.99	20339.99	20339.99
QUNG	388.87	1233.27	3225.36	5228.42	1199.78	1611.99	1611.99	1611.99	1611.99	1611.99	1611.99	1611.99
QCNL	.00	.00	.00	10523.99	36823.98	34201.00	34201.00	34201.00	34201.00	34201.00	34201.00	34201.00
QSIT	3490.89	4259.89	6942.17	13998.39	28618.47	6528.77	6528.77	6528.77	6528.77	6528.77	6528.77	6528.77
QIGS	.00	1135.46	3613.36	8404.77	16848.65	16758.96	16758.96	16758.96	16758.96	16758.96	16758.96	16758.96
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	5990.48	5757.53	4117.33	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNMT	.00	1135.46	3613.36	4117.32	.00	.00	.00	.00	.00	.00	.00	.00
ETPH	221.98	274.58	381.18	924.90	1837.67	2426.85	2426.85	2426.85	2426.85	2426.85	2426.85	2426.85
ETP	637.78	848.33	1308.78	3434.08	7748.16	18347.55	18347.55	18347.55	18347.55	18347.55	18347.55	18347.55
ET	629.46	809.31	1342.43	3449.22	7746.30	18369.51	18369.51	18369.51	18369.51	18369.51	18369.51	18369.51
MS	5988.36	6352.48	8684.80	13728.24	22085.66	28426.79	28426.79	28426.79	28426.79	28426.79	28426.79	28426.79
DP	571.85	552.38	528.27	475.31	423.92	386.11	386.11	386.11	386.11	386.11	386.11	386.11
OTO	4088.83	4785.90	7399.46	14413.51	28955.40	68590.80	68590.80	68590.80	68590.80	68590.80	68590.80	68590.80
OGO	77.07	64.23	64.23	38.53	38.53	51.38	51.38	51.38	51.38	51.38	51.38	51.38
QSD	3930.95	4781.73	7335.22	14374.97	28916.95	6808.92	6808.92	6808.92	6808.92	6808.92	6808.92	6808.92
QGAG	3999.99	3889.99	7309.99	14719.99	29999.99	7249.99	7249.99	7249.99	7249.99	7249.99	7249.99	7249.99
DIFF	-89.83	811.73	25.22	-348.01	948.98	-441.47	-441.47	-441.47	-441.47	-441.47	-441.47	-441.47
VAR	JLY	AUG	SEP	OCT	NOV	DEC	ANN					
TEMP	65.28	59.39	53.70	43.80	34.40	17.40	40.82					
F	5.78	5.69	4.51	3.41	2.27	1.09	43.16					
PPT	2920.31	4269.46	1841.64	2341.51	3735.90	1922.56	27035.07					
QRV	6012.99	3178.99	3090.99	2820.99	2578.99	2528.99	110287.89					
QUNG	159.57	60.82	41.86	55.29	134.29	126.39	13395.31					
QCNL	11128.99	3353.99	2499.99	2638.99	.00	.00	181212.92					
QSIT	90.86	-816.36	237.80	834.38	2275.90	2486.90	68825.86					
QIGS	7149.33	5499.18	2791.64	3341.29	3735.90	.00	68558.58					
QGLI	.00	.00	.00	.00	.00	.00	.00					
SNW	.00	.00	.00	.00	.00	.00	.00					
SNMT	.00	.00	.00	.00	.00	.00	.00					
ETPH	3852.85	2864.47	1945.06	1842.13	437.39	188.88	16397.23					
ETP	15229.57	18789.18	6739.48	3308.81	1359.18	526.85	68108.89					
ET	15222.63	18720.21	6789.25	3320.76	1374.55	552.38	62137.25					
MS	20361.33	15171.44	11259.75	11311.14	13874.85	13161.00	13161.00					
DP	341.73	237.65	211.96	134.88	89.92	64.23	3883.87					
OTO	334.80	-786.54	393.69	912.08	2299.46	2492.17	72893.26					
OGO	64.23	25.69	77.07	51.38	51.38	54.23	68.88					
QSD	289.77	-732.23	282.61	868.78	2248.89	2427.94	71425.26					
QGAG	786.99	36.88	.00	172.99	1825.99	2191.99	89334.93					
DIFF	-498.22	-770.23	282.61	667.70	1222.89	235.84	2898.31					

OBJ# .695
 OBA# .794

EVANSTON												
VAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
TEMP	12.23	14.77	20.38	34.20	47.38	54.98	54.98	54.98	54.98	54.98	54.98	54.98
F	.80	.98	1.66	3.07	4.77	5.59	5.59	5.59	5.59	5.59	5.59	5.59
PPT	1499.62	2131.84	1269.14	499.87	3393.88	3225.55	3225.55	3225.55	3225.55	3225.55	3225.55	3225.55
QRV	2449.90	2171.99	2460.99	8774.99	48232.97	40862.90	40862.90	40862.90	40862.90	40862.90	40862.90	40862.90
QUNG	130.34	116.12	153.25	7845.86	1635.79	1485.19	1485.19	1485.19	1485.19	1485.19	1485.19	1485.19
QCNL	.00	.00	.00	38963.99	41594.98	41594.98	41594.98	41594.98	41594.98	41594.98	41594.98	41594.98
QSIT	2450.80	2121.33	2308.97	16818.24	34206.85	23304.98	23304.98	23304.98	23304.98	23304.98	23304.98	23304.98
QIGS	.00	.00	.00	7339.84	17440.98	18831.54	18831.54	18831.54	18831.54	18831.54	18831.54	18831.54
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	3428.19	5551.23	6840.38	.70	.00	.00	.00	.00	.00	.00	.00	.00
SNMT	.00	.00	.00	8639.67	.70	.00	.00	.00	.00	.00	.00	.00
ETPH	122.54	166.79	313.27	681.81	1615.69	2437.11	2437.11	2437.11	2437.11	2437.11	2437.11	2437.11
ETP	352.07	515.31	1075.64	2234.47	6806.92	18394.72	18394.72	18394.72	18394.72	18394.72	18394.72	18394.72
ET	366.11	526.69	1091.93	2267.36	6840.83	18392.63	18392.63	18392.63	18392.63	18392.63	18392.63	18392.63
MS	12881.38	12293.88	11214.79	18346.88	26983.59	28987.68	28987.68	28987.68	28987.68	28987.68	28987.68	28987.68

RANDOLPH										
0	0	0	1							
1916.	5518.	40025.	1213.	0.	0.	0.	0.	0.	48674.	
0.	0.	0.	0.	0.	0.	0.	0.	0.		
.03930.	.11337.	.02234.	.02492.	.00000.	.00000.	.00000.	.00000.	.00000.		
.00000.	.00000.	.00000.	.00000.	.00000.	.00000.	.00000.	.00000.	.00000.		
\$4056.000										
854.	2146.	705.	608.	2073.	0.	0.	0.	0.		
0475.										
.13052	.33127.	.11614	.09389	.32015	.00000.	.00000.	.00000.	.00000.		
539.58325										
.54	.65	.79	.92	1.00	1.13	1.07	1.01	.92	.82	.75
.89	1.02	1.19	1.29	1.32	1.32	1.32	1.31	1.29	1.24	1.13
1.30	.45	1.00	.00	.50	.02	.00	32.00	26.30	1.00	20.00
10.00	1.40	14.00	.00	.00	40.00	1.00	.00	.20	.30	2.50
1 1904	21.00	19.00	27.00	41.00	50.00	54.70	64.00	59.00	42.00	34.70
1 1905	7.00	11.50	19.70	35.00	47.60	54.40	62.10	62.00	52.20	42.00
1 1906	19.30	18.00	27.30	39.00	50.50	58.00	64.00	57.10	52.50	42.30
2 1904	.93	.47	1.82	.19	1.05	1.04	1.00	2.17	.05	1.21
2 1905	.70	1.10	.67	.26	1.75	1.07	1.05	1.57	1.74	.54
2 1906	1.64	.48	.09	.53	3.14	.92	.06	.51	.03	1.27
3 1904	5.85	5.71	7.92	8.43	12.50	9.76	7.42	5.59	4.69	4.04
3 1905	3.90	3.30	3.95	4.46	14.10	9.00	6.57	5.42	4.47	4.43
3 1906	5.67	4.67	8.43	20.10	29.20	19.00	15.50	12.20	19.10	9.00
4 1904	.00	.00	.00	2.00	15.50	3.59	1.05	.46	.38	.00
4 1905	.00	.00	.00	5.00	20.00	11.60	3.00	.52	.32	.00
4 1906	.00	.00	.00	3.00	15.00	12.00	6.00	.45	.52	.00
5 1904	1.20	1.30	2.53	2.87	.81	.91	1.15	.11	.09	.15
5 1905	.61	.55	.49	2.04	1.09	2.29	.44	.45	.18	.11
5 1906	2.31	1.92	7.39	4.20	9.99	7.00	.68	.35	.13	.20
6 1904	1.34	1.31	2.29	4.55	8.44	2.45	.67	.42	.29	.38
6 1905	.93	.84	1.03	4.10	10.39	7.05	.90	.60	.30	.37
6 1906	1.94	1.57	4.56	5.05	16.98	11.65	1.54	.73	.45	.55
7 1904	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
7 1905	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
7 1906	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1904	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1905	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1906	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

POTS 18 THRU 24 SHOULD BE SET AS FOLLOWS
 .10000 .31007 .17057 .69999 .00000
 .00000 1.00000 .11904 .50000 .02500
 .10000 .00000 .19999 .29999 .79999

POTS 18 THRU 24 ARE SET AS FOLLOWS
 .09997 .31078 .17797 .69958 .00000
 .00000 .09835 .11877 .49989 .02496
 .09948 .00000 .19995 .29974 .79968

RANDOLPH											1954													
											VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC	ANN
											TEMP	21.00	19.00	27.00	41.00	50.00	54.70							
											F	1.43	1.33	2.29	3.76	5.00	5.07							
											PPT	3772.07	1906.31	4137.11	770.83	4298.79	7886.63							
											QRV	5461.99	5349.99	9328.98	18459.97	34244.94	9905.98							
											QUNG	474.55	463.19	7202.98	2770.71	1814.00	791.73							
											QCML	.00	.00	.00	6112.00	62667.00	14961.00							
											QSIT	5729.19	5591.44	16085.89	16497.00	4900.70	1000.70							
											DIGS	.00	.00	13267.04	8594.78	32549.39	14421.10							
											QGLI	.00	.00	.00	.00	.00	.00							
											SNW	11397.35	13303.07	4173.74	.00	.00	.00							
											SNMT	.00	.00	13267.04	4173.74	.00	.00							
											ETPH	207.35	221.74	444.07	1079.21	1007.36	2524.92							
											ETP	957.07	1000.00	2226.00	5752.89	12250.83	16261.33							
											ET	772.38	772.38	2119.10	5822.57	12259.10	16259.64							
											MS	7406.95	6674.17	17853.92	20065.09	40065.09	39104.35							
											DP	49.51	49.51	49.51	59.41	59.41	59.41							
											QTO	5703.75	5525.50	16061.60	16437.89	4931.30	1903.59							
											QGO	1227.89	1148.67	3267.77	3366.70	1009.45	853.55							
											QSD	4475.85	4378.03	12793.92	13071.09	3801.91	1810.00							
											QGAG	4000.99	5669.99	10299.98	8429.98	2099.99	2099.99							
											DIFF	-414.13	-1293.15	2493.84	4641.18	571.91	-1600.95							
											VAR	JLY	AUG	SEP	OCT	NOV	DEC	ANN						
											TEMP	64.00	59.00	52.00	42.50	34.70	13.10	40.21						
											F	6.71	5.66	4.43	3.32	2.29	.82	42.71						
											PPT	6084.00	8001.31	3853.19	4907.75	7787.51	4815.43	58163.00						
											QRV	3533.99	1721.99	1176.99	1550.99	2300.99	3456.99	95607.78						
											QUNG	601.91	453.40	390.67	370.39	340.00	335.40	15227.02						
											QCML	4258.79	1946.67	1541.27	.00	.00	.00	93207.90						
											QSIT	-1600.96	-1542.63	-971.72	981.00	2228.32	3659.39	53313.80						
											DIGS	8000.45	9677.61	4546.77	4987.75	7787.51	.00	103752.42						
											QGLI	.00	.00	.00	.00	.00	.00	.00						
											SNW	.00	.00	.00	.00	.00	.00	4015.43						
											SNMT	.00	.00	.00	.00	.00	.00	17440.79						
											ETPH	3845.40	2642.00	1851.81	946.39	420.47	130.99	16591.37						
											ETP	23483.17	16526.21	9959.17	4686.04	2100.14	610.99	95902.25						
											ET	23498.26	16546.61	9991.46	4693.71	2110.10	653.55	95506.09						
											MS	23775.52	16683.49	11457.01	11734.27	17436.02	16804.27	16804.27						
											DP	49.51	59.41	59.41	49.51	49.51	59.41	653.55						
											QTO	-1623.98	-1564.57	-1019.83	970.42	2198.32	3624.25	52910.12						
											QGO	-455.50	-455.78	-277.26	435.78	752.57	1192.22	1192.22						
											QSD	-1166.47	-1128.86	-732.77	534.78	1445.74	2435.97	40975.89						
											QGAG	609.99	479.99	895.99	627.99	888.99	1810.99	35020.89						
											DIFF	-1778.47	-1600.86	-1128.77	-93.27	556.74	618.97	1472.99						

OBJ= 2.351
 OBA= .363

RANDOLPH											1955													
											VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC	ANN
											TEMP	7.00	11.50	19.70	35.00	47.00	54.40							
											F	.51	.77	1.63	3.15	4.00	5.54							
											PPT	3163.67	4461.99	2717.51	1054.55	7090.00	6367.91							
											QRV	3700.99	3442.99	4190.99	10629.97	42153.92	28621.95							
											QUNG	316.36	207.69	320.42	7540.79	1143.00	778.75							
											QCML	.00	.00	.00	20200.00	81119.00	47049.59							
											QSIT	4031.17	3582.54	4194.44	14302.17	5044.44	5736.31							
											DIGS	.00	.00	.00	24538.56	43602.28	27540.23							
											QGLI	.00	.00	.00	.00	.00	.00							
											SNW	7179.11	11640.71	14358.23	.22	.00	.00							
											SNMT	.00	.00	.00	14358.00	.22	.00							
											ETPH	74.19	128.14	316.96	862.59	1740.40	2490.00							
											ETP	342.43	613.00	1589.20	3556.81	10783.95	16039.40							
											ET	376.28	653.55	1604.17	3564.84	10823.26	16041.79							
											MS	14447.79	15853.85	14209.27	35192.92	56819.64	56819.64							
											DP	59.41	49.51	39.60	49.51	99.02	5129.41							
											QTO	3980.74	3529.23	4198.90	14298.98	5080.80	10813.35							
											QGO	1148.67	1168.47	911.01	2931.09	1089.25	2237.92							
											QSD	2832.07	2858.75	3247.98	11387.89	4000.54	8575.42							
											QGAG	2479.99	2279.99	1999.99	8299.98	4429.99	9339.98							
											DIFF	352.07	76.76	1247.97	3067.90	-429.44	-734.55							
											VAR	JLY	AUG	SEP	OCT	NOV	DEC	ANN						
											TEMP	62.10	62.00	52.20	42.80	25.70	26.40	37.33						
											F	6.45	6.02	4.38	3.33	1.89	1.66	30.99						

COKEVILLE

Table with 10 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP) and 10 rows of data.

Table with 10 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP) and 20 rows of data.

POTS 10 THRU 24 SHOULD BE SET AS FOLLOWS
.05000 .02500 .25000 .52300 .00952
.00900 .02300 .16666 .50000 .14205
.05000 .00000 .00000 .07000 .03999

POTS 10 THRU 24 ARE SET AS FOLLOWS
.04925 .02463 .24945 .52325 .00959
.00000 .02337 .16595 .49969 .14239
.05047 .05944 .07928 .06935 .03947

COKEVILLE

1954

Table with 10 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP) and 10 rows of data.

Table with 10 columns (VAR, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and 10 rows of data.

OBJ= 0.372
OBA= 1.000

COKEVILLE

1955

Table with 10 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP) and 10 rows of data.

Table with 10 columns (VAR, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and 10 rows of data.

DRJ= 13.579
OBA= .186

COKEVILLE

1956

Table with 10 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP) and 10 rows of data.

Table with 10 columns (VAR, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and 10 rows of data.

OBJ= 47.028
OBA= -.027

BEAR LAKE										
	0	1								
8959.	12347.	20121.	10098.	42.	0.	0.	0.	0.	51513.	
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	
.17358	.23922	.30984	.19544	.00001	.00000	.00000	.00000	.00000		
.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000	.00000		
34301.083										
21283.	7307.	3100.	2030.	6030.	0.	0.	0.	0.		
42356.										
.50247	.17251	.07318	.00223	.10958	.00000	.00000	.00000			
33520.066										
.51	.08	.71	.08	1.00	1.14	.08	.08	.78	.71	.57
1.29	1.37	1.46	1.52	1.53	1.53	1.53	1.53	1.51	1.40	1.43
.20	.40	1.00	.00	.24	.08	35.00	31.00	1.53	20.00	1.00
10.00	2.50	6.00	.40	.00	.00	.00	.00	.00	2.50	3.50
1 1954	21.70	25.43	28.80	43.63	52.13	55.48	67.73	62.46	85.66	44.00
1 1955	15.00	13.20	28.23	33.76	49.46	56.18	64.13	65.39	54.59	44.26
1 1956	24.00	13.40	27.23	41.16	52.00	59.16	65.63	61.60	55.93	44.03
2 1954	2.23	.52	1.78	.36	1.48	1.90	.47	.55	1.16	1.54
2 1955	1.04	1.85	.00	1.40	1.49	1.54	.94	2.08	2.41	.73
2 1956	2.08	.62	.23	.09	3.11	.82	.58	.62	.22	1.15
3 1954	5.03	5.76	8.00	12.53	28.26	17.43	12.14	8.00	7.09	6.84
3 1955	5.32	4.61	5.09	8.04	29.60	20.50	15.09	18.22	7.78	7.37
3 1956	8.01	6.30	8.20	22.63	49.23	41.06	18.92	12.58	9.62	8.87
4 1954	.00	.00	.00	.00	15.61	8.01	2.61	1.60	1.35	.00
4 1955	.00	.00	.00	.00	16.05	12.74	4.41	1.22	2.30	.00
4 1956	.00	.00	.00	.00	15.08	18.15	7.02	3.90	3.05	1.00
5 1954	1.12	1.19	2.31	2.41	8.58	9.75	10.08	12.23	6.65	1.62
5 1955	1.35	1.26	.83	4.19	2.05	6.97	17.44	9.99	8.15	2.00
5 1956	2.94	1.59	3.59	6.57	8.34	8.28	16.31	13.13	6.25	2.35
6 1954	.71	.72	.50	.86	12.00	12.53	17.81	13.84	7.34	1.90
6 1955	.71	.57	.66	1.04	5.61	9.49	19.28	9.27	9.34	1.50
6 1956	1.56	1.23	2.62	2.59	7.00	11.17	17.68	13.45	6.63	2.33
7 1954	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
7 1955	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
7 1956	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1954	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1955	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1956	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

POTS 10 THRU 24 SHOULD BE SET AS FOLLOWS
 .10000 .10000 .10000 .29999 .02000
 .00000 .00000 .06666 1.00000 .00000
 .10000 .00000 .00000 .00000 .79999

POTS 10 THRU 24 ARE SET AS FOLLOWS
 .09997 .09985 .09979 .29974 .01965
 .00000 .00000 .00597 .90945 .00000
 .09997 .00000 .00000 .00000 .79943

BEAR LAKE											1954										
	JAN	FEB	MAR	APR	MAY	JUN															
VAR	21.78	25.43	28.80	43.63	52.13	55.48															
TEMP	1.43	1.70	2.39	3.92	5.26	5.65															
F	0.91	1.41	2.23	3.56	5.11	5.83															
PPT	3093.97	3123.87	2163.98	3719.97	5589.61	53931.61															
QRTV	7050.33	5945.81	7019.36	17682.98	29576.15	17998.26															
QUNG	.00	.00	.00	.00	.00	.00															
QCNL	8176.00	8591.66	5463.18	12106.32	41039.94	38336.67															
QSIT	.00	.00	.00	.00	.00	.00															
QIGS	.00	.00	.00	.00	.00	.00															
QGGL	16258.08	18494.66	25806.49	2092.58	30.11	.22															
SNW	1965.40	2478.13	3720.16	5295.63	16771.84	19811.13															
SNMT	947.23	1321.10	2207.60	6622.04	14562.63	17931.53															
ETP	1018.50	1323.08	2025.14	8546.93	14627.48	17935.17															
MS	14133.92	12831.84	10626.69	25984.20	25884.20	25884.20															
DP	1722.11	1407.09	861.05	388.52	805.55	4641.30															
QTO	9026.64	7935.52	6247.91	12411.81	41740.24	42005.82															
QGO	21.00	21.00	42.00	31.50	21.00	42.00															
QBO	9807.64	7917.52	6205.00	12300.31	41719.24	42863.82															
QGAG	4839.96	5159.96	9949.63	10369.92	36939.73	41939.70															
DIFF	4067.67	2757.55	-3744.02	2018.38	4779.50	924.10															
VAR	67.73	62.46	55.66	44.00	36.50	19.46															
TEMP	7.84	5.99	4.67	3.43	2.40	1.22															
F	2021.50	2365.59	4902.25	7053.77	5692.40	7784.95															
PPT	76621.45	59551.57	31577.77	8180.94	3202.97	4582.90															
QRTV	12531.67	9083.88	7318.72	6854.20	6193.55	5636.13															
QUNG	11226.82	6881.73	5808.48	.00	.00	.00															
QCNL	51950.39	41023.25	20569.55	6934.36	5528.24	5468.61															
QSIT	6512.86	5118.28	7311.83	7053.77	5692.48	.00															
QIGS	.00	.00	.00	.00	.00	.00															
QGGL	.00	.00	.00	.00	.00	.00															
SNW	.00	.00	.00	.00	.00	.00															
SNMT	.22	.00	.00	.00	.00	.00															
ETP	32712.40	24859.51	16264.35	8180.78	3865.28	1750.48															
MS	25539.72	17581.66	10298.01	4748.10	2206.90	871.10															
DP	2760.62	8715.57	5103.33	3591.23	2194.64	903.05															
QTO	7739.00	4853.26	6394.91	9786.64	13545.69	12684.83															
MS	8421.55	8096.03	4906.92	1827.12	63.60	-325.52															
QRTV	68284.46	49038.22	25191.19	6673.57	5523.36	8633.62															
QUNG	73.50	42.00	31.50	42.00	21.00	42.00															
QGO	6218.00	46906.21	25159.65	6631.56	5476.85	6012.82															
QBO	69189.58	52609.63	28619.00	7006.95	3689.67	6190.95															
QGAG	69189.58	52609.63	28619.00	7006.95	3689.67	6190.95															
DIFF	-8978.55	-3813.41	-3460.14	1622.61	1481.88	1621.06															

OBJ= 10,153
 OBA= .132

BEAR LAKE											1955										
	JAN	FEB	MAR	APR	MAY	JUN															
VAR	15.86	13.20	28.23	33.76	49.46	56.18															
TEMP	.99	.88	1.67	3.03	4.99	5.72															
F	4473.12	7957.00	4258.07	6021.51	6408.61	6623.66															
PPT	3072.97	2465.98	2844.97	4513.96																	

SODA										
VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	ANN
TEMP	13.80	13.90	21.30	34.75	49.30	55.40	64.20	71.10	78.10	85.80
PPT	.91	.93	1.76	3.12	4.97	5.65	7.00	8.30	9.60	11.00
ORIV	1123.74	1281.24	1227.00	2487.00	3629.50	5489.50	7549.50	9629.50	11709.50	13789.50
QUNG	7172.59	6597.66	4896.67	19322.31	12965.63	32846.76	48965.63	64896.76	80846.76	96796.76
QCNL	5405.62	4644.83	5295.41	18249.21	7885.71	8179.45	8179.45	8179.45	8179.45	8179.45
OSIT	12462.22	11113.34	9840.60	37894.22	19452.03	32411.51	32411.51	32411.51	32411.51	32411.51
QDGS	.00	.00	.00	5706.03	4377.10	11371.42	11371.42	11371.42	11371.42	11371.42
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	1562.91	2764.16	3991.24	752.29	4.77	.01	.01	.01	.01	.01
ETPH	119.90	129.34	261.40	477.29	1399.50	1937.62	1937.62	1937.62	1937.62	1937.62
ETP	181.00	217.13	490.02	1079.23	3798.66	5371.86	5371.86	5371.86	5371.86	5371.86
MS	4298.62	4079.81	3598.91	7765.45	7765.45	7765.45	7765.45	7765.45	7765.45	7765.45
OP	19.70	19.70	19.70	19.70	382.35	1643.75	1643.75	1643.75	1643.75	1643.75
QTO	12431.02	11097.00	9819.93	37056.56	19781.78	34000.83	34000.83	34000.83	34000.83	34000.83
QGO	37.84	18.92	37.84	18.92	37.84	37.84	37.84	37.84	37.84	37.84
QSO	12393.18	11078.17	9792.09	37037.64	19743.94	33962.99	33962.99	33962.99	33962.99	33962.99
QGAG	12965.83	14471.62	12839.39	34468.62	21035.00	37299.77	37299.77	37299.77	37299.77	37299.77
DIFF	-872.65	-3393.44	-3057.29	2577.81	-1291.05	-3336.77	-3336.77	-3336.77	-3336.77	-3336.77

POTS 10 THRU 24 SHOULD BE SET AS FOLLOWS
 1.0000 2.5000 2.5000 2.3999 0.0000
 0.0000 0.0000 1.6000 4.1600 0.0000
 1.0000 0.0000 0.0000 0.0000 0.9999

POTS 10 THRU 24 ARE SET AS FOLLOWS
 0.9997 62475 24957 23956 0.0000
 0.0000 0.0000 1.6500 4.1600 0.0000
 1.0000 0.0000 0.0000 0.0000 0.9992

SODA										
VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	ANN
TEMP	19.30	24.00	28.25	43.50	51.80	54.85	62.85	68.85	74.85	82.85
PPT	1.27	1.66	2.34	3.91	5.23	5.56	6.81	8.06	9.31	10.56
ORIV	6367.97	6482.91	11425.90	11839.37	38885.55	43688.66	58688.66	73688.66	88688.66	103688.66
QUNG	6120.37	8941.99	15774.28	13059.33	7078.45	7648.52	8218.59	8788.66	9358.73	9928.80
QCNL	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
OSIT	12332.12	13194.14	24653.15	24025.28	43088.33	46448.22	59888.33	73288.44	86688.55	100088.66
QDGS	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	3409.90	4050.52	3103.22	64.43	.24	.00	.00	.00	.00	.00
ETPH	102.21	230.77	346.69	873.41	1588.49	1884.36	2588.49	3288.62	3988.75	4688.88
ETP	253.27	367.40	649.91	1974.91	4311.82	5188.74	6068.66	6948.58	7828.50	8708.42
MS	3634.38	3949.73	7580.47	7761.50	6539.53	7785.45	8971.37	10157.29	11343.21	12529.13
OP	19.70	19.70	19.70	19.70	19.70	19.70	19.70	19.70	19.70	19.70
QTO	12317.49	13168.93	24829.22	24398.48	45741.24	46981.84	58881.95	70782.06	82682.17	94582.28
QGO	28.38	47.30	47.30	47.30	37.84	37.84	37.84	37.84	37.84	37.84
QSO	12289.11	13121.83	24782.51	24351.17	45703.39	46923.79	58823.90	70724.01	82624.12	94524.23
QGAG	13988.85	13793.44	24218.99	25471.89	46242.51	47013.87	58914.98	70816.09	82717.20	94618.31
DIFF	-1609.73	-871.81	2563.52	-1120.71	-539.11	-2790.87	-2790.87	-2790.87	-2790.87	-2790.87

OBJ# 25.764
 DBA# .649

SODA										
VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	ANN
TEMP	13.80	13.90	21.30	34.75	49.30	55.40	64.20	71.10	78.10	85.80
PPT	.91	.93	1.76	3.12	4.97	5.65	7.00	8.30	9.60	11.00
ORIV	1123.74	1281.24	1227.00	2487.00	3629.50	5489.50	7549.50	9629.50	11709.50	13789.50
QUNG	7172.59	6597.66	4896.67	19322.31	12965.63	32846.76	48965.63	64896.76	80846.76	96796.76
QCNL	5405.62	4644.83	5295.41	18249.21	7885.71	8179.45	8179.45	8179.45	8179.45	8179.45
OSIT	12462.22	11113.34	9840.60	37894.22	19452.03	32411.51	32411.51	32411.51	32411.51	32411.51
QDGS	.00	.00	.00	5706.03	4377.10	11371.42	11371.42	11371.42	11371.42	11371.42
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	1562.91	2764.16	3991.24	752.29	4.77	.01	.01	.01	.01	.01
ETPH	119.90	129.34	261.40	477.29	1399.50	1937.62	1937.62	1937.62	1937.62	1937.62
ETP	181.00	217.13	490.02	1079.23	3798.66	5371.86	5371.86	5371.86	5371.86	5371.86
MS	4298.62	4079.81	3598.91	7765.45	7765.45	7765.45	7765.45	7765.45	7765.45	7765.45
OP	19.70	19.70	19.70	19.70	382.35	1643.75	1643.75	1643.75	1643.75	1643.75
QTO	12431.02	11097.00	9819.93	37056.56	19781.78	34000.83	34000.83	34000.83	34000.83	34000.83
QGO	37.84	18.92	37.84	18.92	37.84	37.84	37.84	37.84	37.84	37.84
QSO	12393.18	11078.17	9792.09	37037.64	19743.94	33962.99	33962.99	33962.99	33962.99	33962.99
QGAG	12965.83	14471.62	12839.39	34468.62	21035.00	37299.77	37299.77	37299.77	37299.77	37299.77
DIFF	-872.65	-3393.44	-3057.29	2577.81	-1291.05	-3336.77	-3336.77	-3336.77	-3336.77	-3336.77

OBJ# 65.334
 DBA# .369

SODA										
VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	ANN
TEMP	18.90	13.00	26.80	41.15	51.80	59.00	66.80	73.60	80.40	87.20
PPT	1.24	.87	2.22	3.70	5.23	6.81	8.39	9.97	11.55	13.13
ORIV	14892.30	8172.61	16873.97	29931.77	39130.89	38596.65	47896.65	56796.65	65696.65	74596.65
QUNG	5405.63	5265.49	14780.72	18347.06	13561.14	11893.66	10216.66	8539.66	6862.66	5185.66
QCNL	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
OSIT	19739.40	13336.67	31245.78	47529.18	46590.20	48998.20	51396.20	53794.20	56192.20	58590.20
QDGS	.00	.00	3919.48	6233.45	8435.11	8176.89	8176.89	8176.89	8176.89	8176.89
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	7758.70	8643.70	9221.30	169.12	.05	.00	.00	.00	.00	.00
ETPH	158.85	121.43	328.90	749.63	1588.49	2262.96	2947.43	3631.90	4316.37	5000.84
ETP	246.02	203.65	616.55	1695.03	4311.62	6273.84	8136.06	10000.30	11864.54	13728.78
MS	269.16	212.85	634.63	1705.82	4324.21	6283.31	8142.41	10001.51	11860.61	13719.71
OP	476.90	130.08	382.35	2731.50	4324.21	3819.65	3819.65	3819.65	3819.65	3819.65
QTO	20179.12	13405.44	31569.50	50216.03	50878.26	44757.35	44757.35	44757.35	44757.35	44757.35
QGO	37.84	18.92	37.84	28.38	37.84	28.38	37.84	28.38	37.84	28.38
QSO	20141.28	13368.52	31531.66	50187.85	50840.42	44728.97	44728.97	44728.97	44728.97	44728.97
QGAG	21149.94	16368.22	33713.47	46621.89	50966.78	43093.01	43093.01	43093.01	43093.01	43093.01
DIFF	-1606.66	-2981.69	-2181.81	1565.76	-120.35	1635.95	1635.95	1635.95	1635.95	1635.95

OBJ# 91.265
 DBA# 3.826

DNEIDA										
N	0	0	1							
11673.	5361.	2367.	7927.	36.	1471.	1363.				
0.	0.	0.	466.	0.	0.	0.	38884.			
38443	17423	07664	25667	00115	04762	04413				
00000	00000	00000	00000	00000	00000	00000				
\$2573.666										
597.		1233.	0.	1005.	0.	0.				
2635.										
21958	00000	43492	00000	35449	00000	00000				
235.25000										
.48	.55	.63	.81	1.04	1.12	.95	.87	.77	.67	.59
.99	1.08	1.14	1.18	1.20	1.22	1.23	1.24	1.23	1.22	1.17
.40	.60	1.00	.80	.50	.82	.60	32.00	22.00	.78	20.00
10.00	4.50	7.00	.00	.50	3.00	.00	.00	.00	.00	2.50
1 1954	15.10	26.10	28.80	44.40	52.10	54.30	67.20	62.70	56.60	44.70
1 1955	13.80	15.40	23.40	36.40	49.10	55.30	64.50	65.50	55.20	46.80
1 1956	14.00	14.60	27.90	41.70	52.00	59.00	65.90	61.60	56.60	44.10
2 1954	1.46	.89	2.23	1.12	1.92	2.50	.62	1.40	1.54	.51
2 1955	.73	.79	.89	1.82	2.38	3.68	.59	2.17	1.56	1.66
2 1956	1.78	.71	.23	.79	2.46	.62	.47	.14	.33	1.25
3 1954	6.12	5.74	11.60	39.30	11.60	4.69	1.71	1.48	1.58	2.60
3 1955	3.76	3.53	4.73	23.00	42.10	26.20	3.26	3.14	1.82	1.85
3 1956	10.70	8.17	28.40	91.00	42.70	6.37	2.87	2.95	1.27	3.87
4 1954	.00	.00	.00	.00	6.40	5.10	5.30	3.30	2.40	.00
4 1955	.00	.00	.00	.00	2.80	7.50	5.50	4.90	2.60	.00
4 1956	.00	.00	.00	.00	4.70	8.00	8.00	4.80	3.10	.00
5 1954	9.38	9.44	14.72	16.18	17.49	19.12	26.75	23.96	16.80	9.25
5 1955	8.67	8.55	9.17	18.58	11.95	13.43	29.53	18.94	18.58	9.48
5 1956	13.58	18.45	17.34	27.44	23.03	14.78	26.28	24.42	15.13	9.48
6 1954	5.67	5.98	9.86	11.42	18.43	19.51	27.25	22.10	13.43	4.95
6 1955	5.18	5.76	5.18	14.32	9.83	15.29	38.31	17.45	15.87	5.76
6 1956	8.63	6.69	12.42	22.45	21.48	16.99	28.41	23.46	12.31	6.58
7 1954	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
7 1955	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
7 1956	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
8 1954	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1955	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1956	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

POTS 10 THRU 24 SHOULD BE SET AS FOLLOWS
 .10000 .03006 .05555 .34999 .02500
 .07500 .00000 .33703 .50000 .00000
 .10000 .00000 .00000 .00000 .79999

POTS 10 THRU 24 ARE SET AS FOLLOWS
 .89997 .03045 .05517 .34924 .02465
 .87427 .00000 .03717 .49969 .00000
 .89999 .00000 .00000 .00000 .79974

DNEIDA										
VAR	JAN	FEB	MAR	APR	MAY	JUN				
TEMP	15.10	26.10	28.80	44.40	52.10	54.30				
F	.99	1.74	2.39	3.99	5.26	5.33				
PPT	3757.55	2290.56	5739.27	2882.50	3577.39	6434.16				
QRV	14616.35	14377.23	25378.66	29412.85	47435.89	50215.68				
QUNG	315.81	3342.96	4807.53	2263.37	397.12	241.40				
QCNL	.00	.00	.00	.00	18471.46	13125.59				
QSIT	14661.35	17766.22	29189.84	31181.76	37278.77	41582.82				
QIGS	.00	6492.95	6828.88	3365.45	13468.33	14389.58				
QGLI	7720.99	7720.99	7720.99	7720.99	7720.99	7720.99				
SNH	5765.01	1562.62	481.01	.00	.00	.00				
SNMT	.00	6492.95	6828.88	468.94	.06	.06				
ETPH	78.01	133.98	194.54	506.85	879.35	998.85				
ETP	373.91	750.45	1173.70	3822.38	8316.98	9990.55				
ET	369.56	765.57	1168.70	3832.85	8331.74	9990.55				
MS	12593.89	18008.12	18008.12	17868.28	18033.25	18020.69				
OP	1313.22	1837.82	1112.15	1137.28	1313.22	1595.97				
OTO	23708.85	26515.88	37775.58	39773.70	46831.92	50831.35				
OGO	28.13	58.26	37.78	58.26	58.26	25.13				
QSO	23875.71	26465.53	37737.69	39723.42	45981.66	50685.21				
QGAG	24111.90	24310.78	37989.89	41647.14	45034.71	49219.34				
DIFF	-435.78	2154.76	-162.99	-1923.71	946.95	1386.87				

DNEIDA										
VAR	JULY	AUG	SEP	OCT	NOV	DEC	ANN			
TEMP	67.20	62.70	56.88	44.70	38.80	21.30	42.87			
F	6.98	6.01	4.75	3.48	2.98	1.34	45.08			
PPT	1595.67	3603.13	3963.44	1312.86	3834.76	746.38	3973.38			
QRV	78142.58	56891.19	34573.18	12753.19	11956.11	13548.80	381698.87			
QUNG	88.91	75.18	81.32	133.83	198.08	178.89	11788.62			
QCNL	13548.42	8493.09	6176.70	.00	.00	.00	87987.47			
QSIT	68316.08	58585.80	38022.86	12422.60	11893.37	14815.34	351035.87			
QIGS	7779.92	8698.99	7669.52	1312.56	3834.76	.00	78742.93			
QGLI	7720.99	7720.99	7720.99	7720.99	7720.99	7720.99	92651.98			
SNH	.00	.00	.00	.00	.00	.00	746.36			
SNMT	.00	.00	.00	.00	.00	.00	13794.84			
ETPH	1736.22	1365.84	926.28	464.41	253.78	183.55	7827.81			
ETP	14642.84	18486.29	6318.08	2789.47	1488.56	522.48	8818.88			
ET	14684.22	18438.38	6339.91	2777.24	1428.04	540.36	68872.17			
MS	13176.21	11467.14	12792.93	11366.88	13785.78	13283.03	13283.03			
OP	2829.52	2387.67	2463.07	2238.59	1815.89	1262.95	19899.41			
OTO	69833.31	60358.00	39962.20	22142.57	21149.60	22745.78	40820.93			
OGO	58.26	58.26	25.13	58.26	58.26	58.26	515.23			
QSO	69783.04	60307.73	39937.73	22892.31	21899.53	22695.51	468105.68			
QGAG	68847.31	61673.64	43241.28	23812.80	23513.69	22517.35	468838.08			
DIFF	935.74	-1365.98	-3384.22	-1728.29	-2414.15	-5724.38				

OBJ# 5.111
 OBA# -2.224

DNEIDA										
VAR	JAN	FEB	MAR	APR	MAY	JUN				
TEMP	13.80	15.40	23.40	36.40	49.10	55.30				
F	.91	1.03	1.94	3.27	4.95	5.84				
PPT	1878.77	2033.19	2059.93	4169.33	6125.32	9265.19				
QRV	13351.08	14845.81	13351.08	36864.59	29337.11	39355.95				
QUNG	193.58	181.78	1683.61	3127.20	2173.87	1939.78				
QCNL	.00	.00	.00	.00	7208.26	19382.49				
QSIT	13480.55	14948.16	14876.55	39703.12	22480.93	27768.42				
QIGS	.00	.00	2886.29	7994.21	10461.17	28846.69				
QGLI	7720.99	7720.99	7720.99	7720.99	7720.99	7720.99				
SNH	2625.13	4658.33	3636.96	12.09	.00	.00				
SNMT	.00	.00	2886.29	3824.67	12.09	.00				
ETPH	63.98	79.04	158.06	288.77	755.49	1945.38				
ETP	341.72	442.79	953.83	2178.63	7145.46	18452.64				
ET	364.43	464.96	1811.62	2218.82	7150.46	13442.95				
MS	12943.73	12491.33	14432.88	18008.12	18008.12	18020.69				
OP	786.57	377.00	113.10	6.28	6.28	314.16				
OTO	21715.38	22796.84	22456.74	47125.23	29858.55	35551.28				
OGO	58.26	58.26	25.13	58.26	58.26	58.26				
QSO	21665.04	22745.78	22431.61	47074.96	29808.28	35501.98				
QGAG	22318.08	22019.18	23613.33	47824.47	38787.00	34573.18				
DIFF	-853.04	726.59	-1181.71	-749.50	-978.72	927.90				

DNEIDA										
VAR	JULY	AUG	SEP	OCT	NOV	DEC	ANN			
TEMP	64.50	65.58	55.28	46.80	28.68	25.30	39.89			
F	6.78	6.28	4.63	3.58	1.88	1.80	42.47			
PPT	1286.63	5584.65	4014.91	4272.28	3448.71	6287.20	52425.36			

CACHE VALLEY										
0	0	0	1	0055	50020	9489	4827	089	0	152088
52429	27563	6055	50020	9489	4827	089	0	152088		
392	0	3	683	0	275	0	0	152088		
34480	18132	8365	3298	8622	8317	8819	0	0		
8257	8088	8081	8844	8088	8018	8088	0	0		
81267.33										
7515	10663	15771	5776	7775	0	0				
52700										
14259	38188	29925	10950	14753	8088	8088				
84391.666										

0	52	59	88	1,00	1,13	1,33	1,51	1,71	1,86	1,56	1,48
.81	.89	1.01	1.10	1.14	1.18	1.18	1.19	1.18	1.13	1.03	.98
.28	.50	1.00	.00	.00	.17	.00	31.00	25.00	1.16	10.00	2.00
10.00	3.50	7.00	.00	.00	.43	.00	.00	.00	.00	2.50	3.00
1 1954	25.48	30.48	36.83	49.89	57.11	65.65	62.85	65.19	61.94	48.77	41.27
1 1955	15.48	19.08	29.26	36.27	54.79	61.25	69.69	71.57	80.29	49.83	31.98
1 1956	30.48	20.48	37.04	47.19	57.37	64.31	71.17	67.39	82.85	47.40	31.48
2 1954	1.70	.82	2.95	.92	1.06	1.07	.31	.22	1.42	.88	1.99
2 1955	2.95	1.84	1.00	2.11	1.08	2.27	.24	1.68	2.25	1.08	2.15
2 1956	3.03	.88	.00	.86	3.03	.89	.47	.23	.21	1.48	.71
3 1954	6.83	5.78	6.68	12.53	28.28	17.43	12.14	8.80	7.09	6.84	8.00
3 1955	5.32	4.61	5.09	8.04	29.08	28.50	15.00	18.22	7.78	7.37	8.49
3 1956	8.01	6.30	8.26	22.63	49.23	41.88	18.92	12.55	9.62	8.87	7.13
4 1954	.00	.00	.00	.00	9.80	5.00	8.48	3.48	1.50	.00	.00
4 1955	.00	.00	.00	.00	4.00	5.80	8.00	3.00	2.50	.00	.00
4 1956	.00	.00	.00	2.00	8.00	13.00	18.00	5.00	2.50	.00	.00
5 1954	5.11	5.37	6.53	7.40	5.34	4.44	4.06	4.02	3.82	3.80	4.00
5 1955	4.36	3.86	6.73	9.07	10.00	6.54	4.27	3.85	4.00	4.27	5.14
5 1956	6.88	5.87	9.31	12.53	14.67	8.51	4.36	4.64	3.78	4.88	5.81
6 1954	3.11	2.96	4.37	5.99	6.48	5.27	6.19	5.62	4.12	2.88	2.84
6 1955	2.70	2.56	2.86	6.12	7.12	5.20	7.08	4.41	4.45	3.61	3.53
6 1956	4.52	3.40	5.52	10.32	18.85	8.85	8.00	6.02	4.16	3.25	3.87
7 1954	.43	.43	.43	.43	.43	.43	.43	.43	.43	.43	.43
7 1955	.43	.43	.43	.43	.43	.43	.43	.43	.43	.43	.43
7 1956	.43	.43	.43	.43	.43	.43	.43	.43	.43	.43	.43
8 1954	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1955	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1956	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

POTS 10 THRU 24 SHOULD BE SET AS FOLLOWS
 .0000 .05102 .07142 .09999 .00000
 .0000 .02158 .04781 .50000 .00000
 .1000 .00000 .00000 .00000 .39999

POTS 10 THRU 24 ARE SET AS FOLLOWS
 .09997 .05035 .07035 .09958 .00000
 .00000 .02117 .04699 .49957 .00000
 .09936 .00000 .00000 .00000 .39959

CACHE VALLEY 1954

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	26.40	30.48	35.83	49.89	57.11	60.85
F	1.74	2.03	2.97	4.49	5.78	6.15
PPT	21534.46	10367.21	37389.82	11653.94	12160.83	24954.84
ORIV	39489.87	37499.88	55459.82	75939.76	81885.75	66759.74
QUNG	21786.07	32357.66	23738.28	26146.50	60864.43	37534.57
CNCL	.00	.00	.00	.00	124139.64	69670.31
QSIT	50326.35	67466.86	75117.96	92115.54	60393.21	46217.85
DIGS	8847.54	24942.27	48727.19	13111.22	74246.80	59789.88
QGIL	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95
SNW	27381.81	12825.94	1407.37	10.08	.01	.00
SNMT	8847.54	24942.27	11358.57	1457.28	19.07	.01
ETPH	1889.58	2391.47	4072.13	11972.71	19491.85	23251.31
ETP	3083.46	4086.43	6904.56	25125.15	5528.82	65524.46
ET	3123.53	4113.17	8890.52	25251.16	52543.44	65556.19
MS	43822.28	64635.57	88728.98	76727.66	68724.06	82897.40
OP	92.77	77.31	61.85	806.85	2876.12	4638.91
QTO	81233.67	71583.00	80805.82	98128.51	68501.31	56138.87
QGO	61.85	123.70	61.85	123.70	123.70	61.85
QBO	61171.82	71439.29	79943.96	98094.81	68377.88	56869.82
QGAG	64749.79	68189.76	64897.75	83781.71	67849.79	56249.82
OIFF	-3577.96	3329.58	-4153.77	4243.89	727.61	-188.88
VAR	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	62.85	68.19	61.84	48.77	41.27	25.82
F	6.53	6.54	5.12	3.60	2.72	1.82
PPT	3926.87	2766.81	17987.60	8813.78	25207.98	15034.16
ORIV	78489.75	71208.78	52288.82	36579.88	36079.88	34179.89
QUNG	20142.62	18950.32	15267.92	14298.67	19296.87	13673.82
CNCL	18709.98	43888.92	19888.99	.00	.00	.00
QSIT	37743.88	38878.54	38503.31	48798.28	44827.89	45889.21
DIGS	44462.32	24321.28	27488.18	6813.78	25287.98	2395.81
QGIL	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95
SNW	.00	.00	.00	.00	.00	.00
SNMT	.00	.00	.00	.00	.00	.00
ETPH	26533.23	29614.09	19732.94	18886.32	4972.65	1944.50
ETP	59795.42	58516.39	34262.81	18866.32	7794.88	2972.32
ET	59888.39	58527.64	32888.89	13036.41	7437.72	2999.83
MS	87189.92	33462.83	28343.07	23349.20	41209.83	48714.21
OP	5721.32	5535.77	4283.28	2875.10	1287.97	348.18
QTO	48778.46	49898.24	47984.53	48778.46	59828.83	51885.81
QGO	123.70	154.83	123.70	123.70	123.70	154.83
QBO	48866.75	49543.61	47788.82	48866.75	58471.39	51461.83
QGAG	51589.83	59829.84	48499.85	48219.85	50131.84	731556.87
OIFF	-2663.08	-1386.22	-719.82	426.90	-321.43	1329.18

DBJ* .451
 DBA* -1.248

CACHE VALLEY 1955

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	15.48	19.58	29.26	38.27	54.79	61.25
F	1.88	1.31	2.42	3.44	5.53	6.24
PPT	25968.02	23307.80	12887.33	26728.06	21281.11	28754.83
ORIV	34319.89	32719.89	36349.88	77559.76	90249.71	85989.79
QUNG	11456.33	9927.38	45542.71	41231.33	85716.18	61377.85
CNCL	.00	.00	.00	.00	58689.32	57882.99
QSIT	44614.82	41186.97	78633.80	112967.87	113845.07	75053.43
DIGS	.00	.00	43227.18	56825.18	48668.17	57262.18
QGIL	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95
SNW	39487.16	62715.05	32155.27	2258.22	5.82	.00
SNMT	.00	.00	43227.18	29887.84	2252.49	5.82
ETPH	1151.40	1549.29	3258.99	5823.20	17566.16	23812.71
ETP	1915.48	2833.27	5526.07	12228.18	47393.31	67288.96
ET	1948.34	2859.64	5335.77	12262.19	47394.25	67292.42
MS	38796.79	36183.53	73882.45	88726.98	88726.98	78815.17
OP	-154.63	-218.48	-154.03	92.77	1932.88	5393.82
QTO	49791.82	46203.59	83778.81	119323.28	128246.68	85885.29
QGO	123.70	81.95	154.83	61.85	123.70	123.70
QBO	49886.32	48141.74	83624.17	118261.40	128118.98	85541.59
QGAG	55289.82	49223.85	85261.73	114999.85	115339.64	82919.73
OIFF	-5622.51	-3882.18	-1637.56	3261.76	4777.33	2621.85
VAR	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	69.49	71.57	60.29	49.83	31.99	30.54
F	7.24	6.87	5.06	3.88	2.18	1.92
PPT	3848.15	21281.11	28581.49	13688.71	27234.75	52062.72
ORIV	89889.73	85963.82	56419.82	36139.88	44829.85	65649.79
QUNG	32495.50	22888.21	16753.88	19878.89	13975.86	46975.86
CNCL	101338.65	38801.99	31668.32	.00	.00	27684.25
QSIT	37824.67	25566.15	38182.06	43346.35	55924.89	118325.79
DIGS	53789.48	49282.18	44335.65	13688.71	27234.75	34876.57
QGIL	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95
SNW	.00	.00	.00	.00	17192.14	17192.14
SNMT	.00	.00	.00	.00	34876.57	118252.92
ETPH	33691.21	33484.88	19157.37	19864.41	2881.00	2299.96
ETP	76445.28	69564.86	33283.53	17825.21	4516.88	3515.87
ET	76480.25	69594.26	33245.58	17813.43	4546.13	3556.50
MS	58889.82	30879.71	41951.25	37889.00	80638.62	88726.98
OP	7344.9					

TREMONTON										
	0	0	1							
17803,	13758,	1158,	16645,	6513,	8612,	72,				67587,
2093,	P,	507,	217,	0,	217,	0,				
26340,	28344,	11713,	24827,	89636,	12742,	80106,				
83896,	84880,	80750,	80800,	80321,	80800,	80800,				
\$5632,254	374,	3892,	4525,	2698,	9506,	0,				0,000
20735,										
44900,	14897,	21881,	12999,	45881,	80800,	80800,				
\$1729,583										
.44	.50	.56	.71	.98	1.08	.95	.87	.78	.72	.53
.81	.95	1.09	1.16	1.18	1.18	1.18	1.18	1.13	1.04	.91
.30	.55	1.00	.80	.40	.11	.00	35.00	28.00	1.11	20.00
10.00	1.00	6.00	.80	.80	24.00	17.00	.03	.04	.00	2.50
1 1954	29.68	32.95	37.70	58.75	59.55	62.35	75.15	78.25	62.45	58.58
1 1955	15.78	21.35	31.35	44.00	55.48	63.28	72.05	73.38	61.35	58.15
1 1956	31.40	21.05	38.35	49.45	59.75	66.50	74.55	68.75	65.00	58.80
2 1954	1.33	.58	1.87	.45	.84	1.03	.34	.17	1.99	.49
2 1955	2.28	1.64	.76	1.21	1.32	2.10	1.12	1.77	1.11	.40
2 1956	2.85	.38	.11	1.16	2.08	.62	.35	.00	.04	.98
3 1954	1.21	1.02	1.20	2.22	5.01	3.09	2.15	1.56	1.25	1.17
3 1955	.94	.81	.90	1.42	5.20	5.06	2.67	1.81	1.38	1.15
3 1956	1.42	1.11	1.45	4.81	8.74	7.43	3.35	2.23	1.70	1.57
4 1954	.08	.08	.08	.50	.80	9.00	10.18	10.18	6.08	2.70
4 1955	.08	.08	.08	.80	5.80	7.80	10.80	9.18	7.70	3.30
4 1956	.08	.08	.08	.80	6.80	10.40	10.50	10.48	7.90	4.00
5 1954	13.00	12.87	16.46	18.52	5.51	3.75	1.33	1.23	3.64	7.81
5 1955	11.35	10.10	17.11	22.67	17.39	9.91	1.29	1.84	2.92	8.13
5 1956	23.17	14.12	22.10	29.40	28.85	7.94	1.36	2.48	2.88	8.31
6 1954	12.14	13.04	15.96	17.22	12.36	10.24	9.39	9.26	8.83	8.86
6 1955	10.34	9.26	16.16	21.47	21.02	15.16	9.83	8.92	9.24	9.91
6 1956	20.86	13.37	22.29	28.90	33.44	14.88	10.01	10.65	8.85	10.78
7 1954	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
7 1955	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
7 1956	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1954	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1955	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
8 1956	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00

POTS 10 THRU 24 SHOULD BE SET AS FOLLOWS
 .10P00 .62500 .25000 .29999 .00000
 .00000 .59999 .18686 .50000 .42499
 .19000 .83800 .84000 .85000 .79999

POTS 10 THRU 24 ARE SET AS FOLLOWS
 .89967 .62475 .24957 .29986 .80000
 .00000 .59954 .16607 .49993 .42486
 .89997 .80978 .83979 .84949 .79968

TREMONTON										
	JAN	FEB	MAR	APR	MAY	JUN				
VAR	29.68	32.95	37.70	58.75	59.55	62.35				
TEMP	1.95	2.20	3.12	4.56	6.81	6.35				
F	7519.05	3294.86	18532.30	2534.51	4759.25	5829.37				
ORIV	68420.01	73480.70	89338.21	97815.81	69640.81	57730.40				
QUNG	2851.16	4289.46	1769.22	1436.35	3188.66	1917.38				
QCNL	.00	.00	.00	2816.12	55196.03	58698.24				
QSIT	78449.82	76554.83	89698.54	91711.59	33557.39	21765.85				
QIGS	5249.46	9139.67	13682.87	4229.81	35117.22	33709.00				
OGLI	.00	.00	.00	.00	.00	.00				
SNW	8521.17	2676.36	145.79	.15	.02	.00				
SNMT	5249.66	9139.67	2550.56	145.63	.15	.00				
ETPH	821.34	1095.42	1999.67	5188.86	8833.45	18002.62				
ETP	1477.98	1888.32	3383.46	18433.98	23982.70	29740.42				
ET	1512.58	1997.58	3382.64	18422.96	23898.55	29728.81				
MS	33358.97	33345.22	33345.22	27198.70	33349.22	33345.22				
DP	82.50	2227.59	7054.88	7714.90	1768.07	3973.92				
QTO	78755.60	78763.48	98556.78	99279.40	35256.54	25603.83				
QGO	3528.15	4125.18	4125.18	4878.18	1925.08	1375.05				
QSO	68855.45	74038.31	92431.59	95209.21	33331.47	24228.57				
QGAG	73220.01	72490.01	92750.00	104200.00	31840.00	21140.00				
DIFF	-6364.55	2148.29	-318.41	-8990.79	2291.47	3888.58				

	JULY	AUG	SEP	OCT	NOV	DEC	ANN
VAR	75.15	70.25	62.45	58.50	43.20	29.10	59.29
TEMP	7.71	6.74	5.24	3.93	2.85	1.83	52.65
PPT	1914.96	957.48	11208.17	2787.96	9321.37	6167.31	66826.59
ORIV	52930.00	52198.00	49760.00	49910.00	53303.01	53402.00	767694.62
QUNG	1335.49	968.00	779.90	730.40	660.00	1293.99	21131.07
QCNL	56885.71	56885.71	37172.84	15287.07	6758.69	3717.28	285329.82
QSIT	7187.78	9421.25	21992.92	37935.58	48800.53	51782.99	568162.12
QIGS	33202.09	32244.61	31653.23	11151.85	13038.65	3777.98	225575.81
OGLI	.00	.00	.00	.00	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00	.00
SNMT	.00	.00	.00	.00	.00	.00	.00
ETPH	15790.48	12449.61	8191.91	4341.01	2240.18	868.48	17132.25
ETP	41264.72	30116.27	17848.01	9025.93	3734.64	1426.87	74235.31
ET	41279.32	30168.83	17848.28	9047.90	3767.68	1467.56	17442.97
MS	25314.87	27418.71	33345.22	33345.22	33345.22	33303.97	33303.97
DP	4455.19	873.77	453.77	5857.75	5362.73	6737.79	46353.30
QTO	11558.51	9955.44	22275.98	43644.42	53269.85	58397.58	684889.25
QGO	713.03	685.02	1237.55	2255.10	2005.12	3892.63	29811.32
QSO	10833.48	9350.41	21039.43	41389.33	58464.73	53384.95	575078.00
QGAG	7540.89	6970.00	29510.00	4810.00	5227.00	35528.00	584659.62
DIFF	3295.47	2380.41	528.42	-2620.67	-4805.26	-215.05	-9581.68

ORJ# 5.915
 OBA# -1.781

TREMONTON										
	JAN	FEB	MAR	APR	MAY	JUN				
VAR	31.40	21.05	38.35	49.45	59.75	66.50				
TEMP	2.87	1.41	3.18	4.45	6.83	6.78				
F	18688.07	2140.25	647.70	6533.40	11634.59	3491.89				
ORIV	117498.81	75358.01	125548.33	182821.03	188350.03	83842.01				
QUNG	7298.64	693.08	5172.39	2889.38	5415.62	4604.62				
QCNL	.00	.00	.00	.00	38299.28	58575.39				
QSIT	123908.35	75331.18	128618.68	188656.78	183795.03	44558.07				
QIGS	16923.86	.00	11323.65	7833.61	32696.08	35788.45				
OGLI	.00	.00	.00	.00	.00	.00				
SNW	9836.73	11178.98	581.08	.00	.00	.00				
SNMT	16923.86	.00	12675.98	590.20	.00	.00				
ETPH	871.29	699.81	2181.78	4853.50	3905.84	11672.87				
ETP	1567.86	1281.24	3556.23	9761.20	24098.85	34698.18				
ET	1595.07	1333.00	3692.65	9762.93	24118.57	34775.28				
MS	33345.22	33345.22	33345.22	33345.22	33345.22	33345.22				
DP	6922.80	10367.95	3437.65	4248.93	2082.59	4697.68				
QTO	178658.29	85583.79	131958.84	164759.81	165639.84	48567.14				
QGO	5288.23	4482.69	5252.73	5142.72	5142.72	2667.61				
QSO	12578.86	81101.04	126698.18	159817.06	184897.89	45899.53				
QGAG	139500.83	79548.81	124580.81	165688.83	162500.83	44728.00				
DIFF	-5121.97	1561.08	2198.09	-5982.95	-2002.92	1179.52				

	JULY	AUG	SEP	OCT	NOV	DEC	ANN
VAR	74.55	68.75	63.00	58.88	32.45	26.85	48.57
TEMP	7.75	6.60	5.29	3.96	2.14	1.69	51.37
F	1971.28	28.16	283.45	5519.60	1830.48	7490.89	57617.87
ORIV	56438.00	68838.01	48728.00	68858.00	65734.01	73720.01	118698.38
QUNG	2881.28	1381.60	1958.19	979.78	1379.99	784.30	33926.31
QCNL	59138.82	58375.39	44494.78	22529.09	5832.25	3717.28	292961.87
QSIT	18488.45	17362.13	17031.33	44827.44	62851.27	71654.45	921104.62
QIGS	34497.51	32244.61	24725.56	17918.55	4446.51	28444.58	218654.75
OGLI	.00	.00	.00	.00	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00	.00
SNMT	.00	.00	.00	.00	.00	.00	.00
ETPH	15498.52	11833.00	8274.74	4407.29	1164.89	821.33	71083.23
ETP	40504.38	28624.66	18228.75	9163.75	1942.01	1316.54	174663.68
ET	40454.28	28628.76	18274.55	9254.16	1993.83	1347.55	175141.58
MS	27308.71	31035.12	33345.22	33345.22	33358.97	33345.22	33345.22
DP	8318.10	137.58	453.77	4372.69	7384.07	3327.6	

CACHE VALLEY

	JAN	FEB	MAR	APR	MAY	JUN
VAR	16.40	19.56	29.28	38.27	54.79	81.25
TEMP	1.08	1.31	2.42	3.44	5.53	6.24
F	25966.02	23307.88	12667.33	26728.06	21281.11	28754.83
PPT	34319.89	32719.89	36349.88	77559.76	90249.71	85989.79
ORIV	11456.33	9927.38	4542.41	41231.33	85716.18	81377.85
QUNG					58689.32	57022.99
OCNL						
OSIT	44614.82	41108.97	78633.88	112967.87	113405.87	75933.43
DIGS			43227.10	58625.18	48888.17	57282.15
IGLI	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95
SNM	39407.16	62719.05	32155.27	2258.22	5.82	
SNMT			43227.10	29897.04	2252.49	5.82
ETPH	1161.48	1549.29	3258.99	5823.20	17566.16	23812.71
ETP	1915.48	2633.27	5526.07	12220.18	47393.31	87288.98
ET	1948.34	2659.84	5533.77	12282.19	47394.25	87282.42
MS	38796.79	38183.33	73882.45	88726.98	79815.17	85833.82
DP	-154.63	-216.48	-154.83	92.77	1932.88	5583.82
QTO	49791.02	46203.59	83778.61	118323.26	120240.68	85685.29
OGO	123.70	61.85	154.63	61.85	123.70	123.70
QSO	49667.32	46141.74	83024.17	118261.48	120116.98	85541.59
OGAG	55289.82	49223.85	85261.73	114999.85	115339.84	82919.73
DIFF	-5622.51	-3882.18	-1637.56	3261.76	4777.33	2621.85

VAR JULY AUG SEP OCT NOV DEC ANN

TEMP	JULY	AUG	SEP	OCT	NOV	DEC	ANN
TEMP	69.89	71.37	69.29	49.83	31.00	38.54	44.45
F	7.24	6.87	5.06	3.88	2.10	1.92	47.15
PPT	3848.15	21281.11	26591.49	13688.71	27234.75	52882.72	284508.00
ORIV	89889.73	55963.82	56419.82	36139.88	44829.85	65649.79	687881.37
QUNG	32495.50	22808.21	16733.80	15678.89	13975.88	48975.98	383331.87
OCNL	101338.65	38081.99	31688.32				88681.25
OSIT	37824.67	25568.18	38182.88	43346.35	55924.69	118325.79	776591.37
DIGS	53789.48	48282.18	44335.68	13688.71	27234.75	34878.37	420895.68
IGLI	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95	83383.39
SNM						17192.14	17192.14
SNMT						34878.37	118252.92
ETPH	33891.21	33404.88	19157.37	18664.41	2881.00	2299.96	155281.56
ETP	78445.28	65564.06	33263.53	17829.21	4518.08	3315.67	338831.00
ET	76480.25	65594.26	33245.55	17813.43	4548.13	3356.50	338238.75
MS	58689.82	38879.71	41931.25	37869.80	80830.62	68726.98	88726.98
DP	7344.94	7174.85	5535.77	3348.81	1499.91	278.33	31977.58
QTO	58440.46	38878.23	49917.88	81955.88	62656.28	115818.25	871961.37
OGO	154.63	123.70	154.63	123.70	61.85	188.55	1453.92
QSO	58285.84	37946.32	48883.24	51832.14	62894.42	115322.68	878887.87
OGAG	54189.82	48619.85	58749.88	54159.82	65124.88	108929.87	883888.88
DIFF	-3583.98	-18873.52	-1866.68	-2327.66	-2538.37	8793.81	-12588.13

POTS 10 THRU 24 SHOULD BE SET AS FOLLOWS

	JAN	FEB	MAR	APR	MAY	JUN
10000	05182	07142	09909	08080	08080	08080
08080	02150	04781	58080	08080	08080	08080
10000	08080	08080	08080	08080	39999	

POTS 18 THRU 24 ARE SET AS FOLLOWS

	JAN	FEB	MAR	APR	MAY	JUN
09997	05035	07055	09955	08080	08080	08080
08080	02117	04899	49957	08080	08080	08080
09936	08080	08080	08080	08080	39959	

CACHE VALLEY 1984

	JAN	FEB	MAR	APR	MAY	JUN
VAR	26.48	30.40	35.83	49.89	57.11	68.65
TEMP	1.74	2.03	2.97	4.49	5.76	6.18
F	21534.46	10387.21	37368.62	11653.94	12166.63	24954.64
PPT	39489.87	37499.88	85459.82	75939.76	81889.75	66769.78
ORIV	21786.07	32357.66	23738.26	26148.50	68864.43	37534.57
QUNG						
OCNL						
OSIT	59326.35	67466.86	75117.98	92115.54	88393.21	46217.85
DIGS	8847.54	24942.27	48727.19	13111.22	74248.80	59789.80
IGLI	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95
SNM	27381.91	12825.94	1487.37	18.88		
SNMT	8847.54	24942.27	11358.57	1457.28	18.87	
ETPH	1688.58	2391.47	4072.13	11972.71	19491.05	23251.31
ETP	3883.46	4088.43	6984.85	25125.15	52526.82	65624.46
ET	3123.53	4113.17	6896.52	25231.16	52543.44	65658.10
MS	43822.28	64836.57	88726.98	78727.05	88726.98	82897.48
DP	92.77	77.31	61.85	896.85	2876.12	4638.91
QTO	61233.67	71583.00	88885.82	98128.51	88881.31	56138.87
OGO	61.85	123.70	61.85	123.70	61.85	61.85
QSO	6171.82	71439.29	79943.96	98884.81	88777.98	56889.82
OGAG	64749.79	68189.78	84897.75	93781.71	87849.79	58249.82
DIFF	-3577.98	3329.50	-4153.77	4243.89	727.81	-188.88

VAR JULY AUG SEP OCT NOV DEC ANN

TEMP	JULY	AUG	SEP	OCT	NOV	DEC	ANN
TEMP	82.85	86.19	61.04	48.77	41.27	25.82	47.35
F	6.53	6.84	5.12	3.88	2.72	1.62	49.56
PPT	3926.87	2786.81	17987.60	6813.78	23287.98	15834.16	192418.85
ORIV	78489.75	71268.78	52268.82	36579.85	38879.88	34179.89	88335.58
QUNG	26142.82	18958.32	15287.92	14288.87	19296.87	13873.82	388675.81
OCNL	81878.98	43888.92	19889.90				338988.93
OSIT	37743.88	38878.54	38383.31	48287.28	45989.21	846281.67	45989.21
DIGS	44482.32	24321.28	27488.10	8813.78	25287.98	2395.81	362146.93
IGLI	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95	65383.39
SNM							13439.14
SNMT							2395.81
ETPH	26533.23	29814.09	19732.94	18886.47	4972.85	1944.58	15994.89
ETP	59795.42	58518.39	34282.91	18886.32	7794.88	2972.32	337951.31
ET	59888.39	58527.64	32888.88	13888.41	7437.72	2999.83	332784.81
MS	87419.92	33482.83	28343.77	23349.28	41289.83	48714.21	48714.21
DP	9721.32	9335.77	4283.26	2875.10	1287.67	348.18	28487.47
QTO	48776.48	49898.24	47984.53	48776.48	58626.83	51553.81	738886.75
OGO	123.70	154.63	123.70	123.70	154.63	92.77	139.82
QSO	48646.75	49543.61	47788.82	48646.75	58471.39	51461.83	731556.87
OGAG	51589.83	58929.84	48499.85	48219.85	58792.83	58131.84	734782.25
DIFF	-2863.88	-1388.22	-719.02	426.98	-321.43	1329.16	-3145.37

OBJ* .451
OBA* -.248

CACHE VALLEY 1985

	JAN	FEB	MAR	APR	MAY	JUN
VAR	16.40	19.56	29.28	38.27	54.79	81.25
TEMP	1.08	1.31	2.42	3.44	5.53	6.24
F	25966.02	23307.88	12667.33	26728.06	21281.11	28754.83
PPT	34319.89	32719.89	36349.88	77559.76	90249.71	85989.79
ORIV	11456.33	9927.38	4542.41	41231.33	85716.18	81377.85
QUNG					58689.32	57022.99
OCNL						
OSIT	44614.82	41108.97	78633.88	112967.87	113405.87	75933.43
DIGS			43227.10	58625.18	48888.17	57282.15
IGLI	5446.95	5446.95	5446.95	5446.95	5446.95	5446.95
SNM	39407.16	62719.05	32155.27	2258.22	5.82	
SNMT			43227.10	29897.04	2252.49	5.82
ETPH	1161.48	1549.29	3258.99	5823.20	17566.16	23812.71
ETP	1915.48	2633.27	5526.07	12220.18	47393.31	87288.98
ET	1948.34	2659.84	5533.77	12282.19	47394.25	87282.42
MS	38796.79	38183.33	73882.45	88726.98	79815.17	85833.82
DP	-154.63	-216.48	-154.83	92.77	1932.88	5583.82
QTO	49791.02	46203.59	83778.61	118323.26	120240.68	85685.29
OGO	123.70	61.85	154.63	61.85	123.70	123.70
QSO	49667.32	46141.74	83024.17	118261.48	120116.98	85541.59
OGAG	55289.82	49223.85	85261.73	114999.85	115339.84	82919.73
DIFF	-5622.51	-3882.18	-1637.56	3261.76	4777.33	2621.85

VAR JULY AUG SEP OCT NOV DEC ANN

TEMP	JULY	AUG	SEP	OCT	NOV	DEC	ANN
TEMP	69.89	71.37	69.29	49.83	31.00	38.54	44.45
F	7.24	6.87	5.06	3.88	2.10	1.92	47.15
PPT	3848.15	21281.11	26591.49	13688.71	27234.75	52882.72	284508.00
ORIV	89889.73	55963.82	56419.82	36139.88	44829.85	65649.79	687881.37
QUNG	32495.50	22808.21	16733.80	15678.89	13975.88	48975.98	383331.87
OCNL	101338.65	38081.99	31688.32				88681.25
OSIT	37824.67	25568.18	38182.88	43346.35	55924.69	118325.79	776591.37
DIGS	53789.48	48282.18	44335.68	13688.71	27234.75	34878.37	420895.68
IGLI	5446.95	5446.95	5446				

TREMONTON												
	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	31.43	21.05	35.35	49.45	59.75	66.50	74.55	68.75	63.00	50.89	32.45	26.85
F	2.07	1.41	3.18	4.45	6.33	6.78	7.75	6.60	5.29	3.96	2.14	1.69
PPT	16800.07	2140.25	647.70	6533.40	11638.59	3491.99	5820.01	9265.04	4308.67	5843.18	7462.72	12306.46
QRTV	117490.01	75358.71	125548.33	162821.03	188350.03	83840.01	58200.01	91242.01	122980.01	118430.03	85400.01	85400.01
QUNG	7290.64	693.00	5172.39	2689.36	5415.62	4604.60	58575.39	8389.88	5368.17	3321.99	3135.00	3135.00
QCML	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
QSIT	123900.35	73531.18	128618.69	180656.78	163795.03	44558.07	58429.56	52201.31	97956.11	122781.48	56655.03	54658.24
QIGS	16023.06	.00	11323.66	7033.61	32666.00	35708.45	.00	.00	19574.77	18052.61	24903.04	35849.27
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	9230.73	11176.98	501.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNMT	16023.06	.00	12675.98	500.20	.00	.00	.00	.00	.00	.00	.00	.00
ETPH	871.29	699.01	2101.78	4853.58	8925.94	11673.07	435.64	709.78	1474.99	3566.87	7729.63	13333.07
ETP	1407.86	1221.24	3556.23	9761.28	24098.85	34698.18	783.93	1218.36	2495.70	7173.12	20915.83	30725.60
ET	1595.07	1333.80	3662.65	9762.93	24118.57	34775.28	797.53	1333.80	2543.88	7177.81	20928.42	30718.86
MS	33345.22	32148.92	33345.22	30608.85	33358.97	33343.22	32533.94	31378.89	33345.22	33358.97	33345.22	33345.22
DP	6902.00	10367.95	3437.65	4248.93	2062.59	4697.68	3327.64	453.77	2062.59	12114.28	11927.98	5197.73
QTO	130858.29	85503.79	131930.94	164759.81	165639.84	48587.14	61657.73	52197.31	99829.42	134755.98	107502.26	59677.64
QGO	5208.25	4482.69	5252.73	5142.72	5142.72	2667.61	3190.14	2695.11	4815.17	4730.20	4427.69	3135.13
QSO	12537.88	81101.89	126698.18	159817.26	168497.69	45899.53	58467.59	49582.19	95814.25	130257.76	163074.54	56542.50
QGAG	130500.03	79540.01	124500.01	165600.03	162500.03	44720.00	63970.01	56910.01	96440.01	127700.01	97970.01	50870.00
DIFF	-5121.97	1561.08	2198.09	-5982.95	-2002.92	1179.52	-5502.42	-7407.81	-585.77	3325.74	5184.54	672.50

TREMONTON												
	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	15.70	21.35	31.35	44.00	56.48	63.20	72.05	73.38	61.35	58.15	30.60	29.82
F	1.03	1.43	2.69	3.96	5.69	6.44	7.49	7.03	5.15	3.91	1.87	48.66
PPT	12869.68	9265.04	4308.67	5843.18	7462.72	12306.46	58200.01	91242.01	122980.01	118430.03	85400.01	85400.01
QRTV	58200.01	32204.00	91242.01	122980.01	118430.03	85400.01	58200.01	91242.01	122980.01	118430.03	85400.01	85400.01
QUNG	585.20	507.10	8389.88	5368.17	3321.99	3135.00	.00	.00	.00	.00	.00	.00
QCML	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
QSIT	58429.56	52201.31	97956.11	122781.48	56655.03	54658.24	58429.56	52201.31	97956.11	122781.48	56655.03	54658.24
QIGS	.00	.00	19574.77	18052.61	24903.04	35849.27	.00	.00	.00	.00	.00	.00
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	17903.51	26568.58	11382.45	93.01	.01	.01	.00	.00	.00	.00	.00	.00
SNMT	.00	.00	19574.77	11299.43	92.99	.01	.00	.00	.00	.00	.00	.00
ETPH	435.64	709.78	1474.99	3566.87	7729.63	13333.07	783.93	1218.36	2495.70	7173.12	20915.83	30725.60
ETP	783.93	1218.36	2495.70	7173.12	20915.83	30725.60	797.53	1333.80	2543.88	7177.81	20928.42	30718.86
ET	797.53	1333.80	2543.88	7177.81	20928.42	30718.86	32533.94	31378.89	33345.22	33358.97	33345.22	33345.22
MS	32533.94	31378.89	33345.22	33358.97	33345.22	33345.22	3327.64	453.77	2062.59	12114.28	11927.98	5197.73
DP	3327.64	453.77	2062.59	12114.28	11927.98	5197.73	61657.73	52197.31	99829.42	134755.98	107502.26	59677.64
QTO	61657.73	52197.31	99829.42	134755.98	107502.26	59677.64	3190.14	2695.11	4815.17	4730.20	4427.69	3135.13
QGO	3190.14	2695.11	4815.17	4730.20	4427.69	3135.13	58467.59	49582.19	95814.25	130257.76	163074.54	56542.50
QSO	58467.59	49582.19	95814.25	130257.76	163074.54	56542.50	63970.01	56910.01	96440.01	127700.01	97970.01	50870.00
QGAG	63970.01	56910.01	96440.01	127700.01	97970.01	50870.00	-5502.42	-7407.81	-585.77	3325.74	5184.54	672.50
DIFF	-5502.42	-7407.81	-585.77	3325.74	5184.54	672.50	72.05	73.38	61.35	58.15	30.60	29.82

TREMONTON												
	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	31.43	21.05	35.35	49.45	59.75	66.50	74.55	68.75	63.00	50.89	32.45	26.85
F	2.07	1.41	3.18	4.45	6.33	6.78	7.75	6.60	5.29	3.96	2.14	1.69
PPT	16800.07	2140.25	647.70	6533.40	11638.59	3491.99	5820.01	9265.04	4308.67	5843.18	7462.72	12306.46
QRTV	117490.01	75358.71	125548.33	162821.03	188350.03	83840.01	58200.01	91242.01	122980.01	118430.03	85400.01	85400.01
QUNG	7290.64	693.00	5172.39	2689.36	5415.62	4604.60	58575.39	8389.88	5368.17	3321.99	3135.00	3135.00
QCML	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
QSIT	123900.35	73531.18	128618.69	180656.78	163795.03	44558.07	58429.56	52201.31	97956.11	122781.48	56655.03	54658.24
QIGS	16023.06	.00	11323.66	7033.61	32666.00	35708.45	.00	.00	19574.77	18052.61	24903.04	35849.27
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	9230.73	11176.98	501.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNMT	16023.06	.00	12675.98	500.20	.00	.00	.00	.00	.00	.00	.00	.00
ETPH	871.29	699.01	2101.78	4853.58	8925.94	11673.07	435.64	709.78	1474.99	3566.87	7729.63	13333.07
ETP	1407.86	1221.24	3556.23	9761.28	24098.85	34698.18	783.93	1218.36	2495.70	7173.12	20915.83	30725.60
ET	1595.07	1333.80	3662.65	9762.93	24118.57	34775.28	797.53	1333.80	2543.88	7177.81	20928.42	30718.86
MS	33345.22	32148.92	33345.22	30608.85	33358.97	33343.22	32533.94	31378.89	33345.22	33358.97	33345.22	33345.22
DP	6902.00	10367.95	3437.65	4248.93	2062.59	4697.68	3327.64	453.77	2062.59	12114.28	11927.98	5197.73
QTO	130858.29	85503.79	131930.94	164759.81	165639.84	48587.14	61657.73	52197.31	99829.42	134755.98	107502.26	59677.64
QGO	5208.25	4482.69	5252.73	5142.72	5142.72	2667.61	3190.14	2695.11	4815.17	4730.20	4427.69	3135.13
QSO	12537.88	81101.89	126698.18	159817.26	168497.69	45899.53	58467.59	49582.19	95814.25	130257.76	163074.54	56542.50
QGAG	130500.03	79540.01	124500.01	165600.03	162500.03	44720.00	63970.01	56910.01	96440.01	127700.01	97970.01	50870.00
DIFF	-5121.97	1561.08	2198.09	-5982.95	-2002.92	1179.52	-5502.42	-7407.81	-585.77	3325.74	5184.54	672.50

TREMONTON												
	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	15.70	21.35	31.35	44.00	56.48	63.20	72.05	73.38	61.35	58.15	30.60	29.82
F	1.03	1.43	2.69	3.96	5.69	6.44	7.49	7.03	5.15	3.91	1.87	48.66
PPT	12869.68	9265.04	4308.67	5843.18	7462.72	12306.46	58200.01	91242.01	122980.01	118430.03	85400.01	85400.01
QRTV	58200.01	32204.00	91242.01	122980.01	118430.03	85400.01	58200.01	91242.01	122980.01	118430.03	85400.01	85400.01
QUNG	585.20	507.10	8389.88	5368.17	3321.99	3135.00	.00	.00	.00	.00	.00	.00
QCML	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
QSIT	58429.56	52201.31	97956.11	122781.48	56655.03	54658.24	58429.56	52201.31	97956.11	122781.48	56655.03	54658.24
QIGS	.00	.00	19574.77	18052.61	24903.04	35849.27	.00	.00	.00	.00	.00	.00
QGLI	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00	.00
SNW	17903.51	26568.58	11382.45	93.01	.01	.01	.00	.00	.00	.00	.00	.00
SNMT	.00	.00	19574.77	11299.43	92							

•

†

•

•

•

•

APPENDIX D
MANAGEMENT OPPORTUNITIES

EVANSTON CASE 1 -1

1954

EVANSTON CASE 1 -1

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	22.12	24.20	24.70	48.60	49.70	54.80
F	1.45	1.62	2.05	3.65	5.01	5.58
PRT	1815.33	894.51	1973.18	368.32	2852.11	3762.29
GRIV	3323.99	3380.99	4897.99	13691.99	43322.98	20339.99
QUNG	388.67	1233.27	3225.38	5228.42	1129.78	1611.59
QCHL	.00	.00	.00	.00	9367.75	17249.33
QSIT	3712.87	4534.27	7323.35	18920.42	41956.93	15398.35
QIGS	.00	1135.46	3513.38	4485.65	4547.86	18319.43
QGLI	.00	.00	.00	.00	.00	.00
SNK	5092.48	5757.53	4117.33	.00	.00	.00
SNMT	.00	1145.46	3613.38	4117.32	.00	.00
ETPH	.00	.00	.00	.00	.00	.00
ETP	637.78	948.33	1328.79	3434.38	7740.16	10347.55
ET	523.84	899.31	1297.47	3536.58	7746.37	13315.55
MS	5092.24	6378.17	8671.23	9762.58	6689.44	8689.42
DP	552.39	525.60	599.27	475.31	411.08	346.84
OTO	4266.42	5922.89	7771.99	19333.63	42302.77	16694.14
OGO	64.23	25.69	25.69	25.69	64.23	64.23
ORO	4162.19	4984.66	7746.38	19397.94	42277.87	15633.91

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	22.12	24.20	24.70	48.60	49.70	54.80
F	1.45	1.62	2.05	3.65	5.01	5.58
PRT	1815.33	894.51	1973.18	368.32	2852.11	3762.29
GRIV	3323.99	3380.99	4897.99	13691.99	43322.98	20339.99
QUNG	388.67	1233.27	3225.38	5228.42	1129.78	1611.59
QCHL	.00	.00	.00	.00	9367.75	17249.33
QSIT	3712.87	4534.27	7323.35	18920.42	41956.93	15398.35
QIGS	.00	1135.46	3513.38	4485.65	4547.86	18319.43
QGLI	.00	.00	.00	.00	.00	.00
SNK	5092.48	5757.53	4117.33	.00	.00	.00
SNMT	.00	1145.46	3613.38	4117.32	.00	.00
ETPH	.00	.00	.00	.00	.00	.00
ETP	637.78	948.33	1328.79	3434.38	7740.16	10347.55
ET	523.84	899.31	1297.47	3536.58	7746.37	13315.55
MS	5092.24	6378.17	8671.23	9762.58	6689.44	8689.42
DP	552.39	525.60	599.27	475.31	411.08	346.84
OTO	4266.42	5922.89	7771.99	19333.63	42302.77	16694.14
OGO	64.23	25.69	25.69	25.69	64.23	64.23
ORO	4162.19	4984.66	7746.38	19397.94	42277.87	15633.91

POTS 14 THRU 24 SHOULD BE SET AS FOLLOWS

19999	01275	23571	54009	81022
20000	01400	23800	54200	81200
20001	01500	24000	54400	81400

POTS 14 THRU 24 ARE SET AS FOLLOWS

00957	01257	03543	54907	82976
00958	01000	02305	49975	80000
00942	00000	00000	00000	79937

See Appendix B for definition of the variables

EVANSTON CASE 1 -1

1955

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	12.20	14.70	21.30	34.20	47.30	54.90
F	.89	.92	1.50	3.27	4.77	5.59
PRT	1499.42	2131.84	1289.14	499.87	3393.89	3025.55
GRIV	2442.81	2171.99	2450.09	3774.99	48232.97	40862.98
QUNG	109.34	116.12	153.25	7845.06	1633.74	1485.19
QCHL	.00	.00	.00	.00	.00	14779.03
QSIT	2573.34	2268.12	2611.25	18620.26	49358.77	35932.53
QIGS	.00	.00	.00	7339.54	3394.54	8641.20
QGLI	.00	.00	.00	.00	.00	.00
SNK	3420.19	5551.23	6844.38	.73	.00	.00
SNMT	.00	.00	.00	5839.67	.70	.00
ETPH	.00	.00	.00	.00	.00	.00
ETP	752.67	515.31	1075.54	2234.47	6896.32	13394.72
ET	379.84	526.89	1045.59	2207.38	6421.37	14414.32
MS	8125.25	7517.93	6593.75	11722.22	5332.80	5533.75
DP	38.54	32.11	22.84	15.25	32.11	38.53
OTO	2569.25	2275.75	2562.12	14584.53	44443.73	35425.32
OGO	51.38	51.38	54.23	25.69	38.33	23.94
ORO	2717.66	2222.42	2517.85	15359.04	49874.75	35372.63

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	12.20	14.70	21.30	34.20	47.30	54.90
F	.89	.92	1.50	3.27	4.77	5.59
PRT	1499.42	2131.84	1289.14	499.87	3393.89	3025.55
GRIV	2442.81	2171.99	2450.09	3774.99	48232.97	40862.98
QUNG	109.34	116.12	153.25	7845.06	1633.74	1485.19
QCHL	.00	.00	.00	.00	.00	14779.03
QSIT	2573.34	2268.12	2611.25	18620.26	49358.77	35932.53
QIGS	.00	.00	.00	7339.54	3394.54	8641.20
QGLI	.00	.00	.00	.00	.00	.00
SNK	3420.19	5551.23	6844.38	.73	.00	.00
SNMT	.00	.00	.00	5839.67	.70	.00
ETPH	.00	.00	.00	.00	.00	.00
ETP	752.67	515.31	1075.54	2234.47	6896.32	13394.72
ET	379.84	526.89	1045.59	2207.38	6421.37	14414.32
MS	8125.25	7517.93	6593.75	11722.22	5332.80	5533.75
DP	38.54	32.11	22.84	15.25	32.11	38.53
OTO	2569.25	2275.75	2562.12	14584.53	44443.73	35425.32
OGO	51.38	51.38	54.23	25.69	38.33	23.94
ORO	2717.66	2222.42	2517.85	15359.04	49874.75	35372.63

VAR	JULY	AUG	SEP	OCT	NOV	DEC	ANN
TEMP	62.10	63.72	62.10	42.80	22.90	20.40	37.17
F	6.43	6.24	4.37	3.27	1.51	1.28	39.48
PRT	3674.33	3025.85	3357.57	1892.36	2157.33	4735.54	29781.86
GRIV	5974.09	4932.90	3133.90	3226.99	2729.99	4381.99	131227.87
QUNG	109.75	81.36	41.97	50.24	175.37	853.19	12744.83
QCHL	20273.47	24682.99	7418.24	1944.57	2129.77	80181.87	2129.77
QSIT	-1146.15	-4334.76	378.14	1351.00	2065.37	4425.64	113471.51
QIGS	13534.37	12374.65	5135.52	2936.82	.00	833.31	55272.71
QGLI	.00	.00	.00	.00	.00	.00	.00
SNK	.00	.00	.00	.00	2157.35	6893.02	8883.00
SNMT	.00	.00	.00	.00	.00	.00	8843.38
ETPH	.00	.00	.00	.00	.00	.00	.00
ETP	13547.73	12400.30	6244.31	7943.34	904.82	615.74	58837.26
ET	13535.00	12441.61	6238.44	7941.79	847.83	511.65	58805.14
MS	6995.34	5635.00	6534.71	9932.78	3767.97	5089.86	6869.86
DP	1194.73	42.11	32.11	38.53	32.11	32.11	359.69
OTO	-1194.73	-4354.84	340.81	1351.70	2646.41	4419.11	113227.83
OGO	25.69	25.69	77.97	51.38	64.23	51.38	552.38
ORO	-1220.39	-4382.57	259.77	1516.31	2820.17	4367.73	112674.64

EVANSTON CASE 1 - 2												
VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	22.14	24.20	24.70	44.63	49.70	54.83						
F	1.40	1.62	2.45	3.65	5.01	5.59						
PRT	1815.33	894.51	1973.18	368.32	2052.11	3752.28						
GRV	333.99	336.99	4807.77	1364.99	4322.98	2933.99						
QUNC	368.87	1233.27	3228.48	5224.42	1125.70	1611.52						
OCNL	.00	.00	.00	.60	6652.27	17177.72						
GSIT	3712.87	4534.27	7323.39	19920.42	41924.82	15424.85						
QIFS	.00	1135.46	3613.38	4485.65	4573.97	10289.74						
QGLI	.00	.00	.00	.00	.00	.00						
SNH	5996.48	5757.53	4117.33	.00	.00	.00						
SNHT	.00	1135.46	3613.38	4117.32	.00	.00						
ETPH	.00	.00	.00	.00	.00	.00						
ET	637.70	840.33	1388.70	3434.00	7740.10	10347.55						
ETP	629.45	393.31	1342.43	3442.22	7746.33	10334.42						
MS	5009.20	6378.17	8654.60	9737.47	6635.09	5536.50						
NP	452.34	488.27	488.27	488.27	417.00	346.84						
QTC	4226.49	5022.89	7797.60	19346.48	42151.61	15736.60						
QTD	24.62	64.23	64.23	25.69	36.33	64.23						
QSN	4200.73	4958.66	7733.45	19320.79	44277.27	15672.45						

EVANSTON CASE 1 - 2												
VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	22.14	24.20	24.70	44.63	49.70	54.83						
F	1.40	1.62	2.45	3.65	5.01	5.59						
PRT	1815.33	894.51	1973.18	368.32	2052.11	3752.28						
GRV	333.99	336.99	4807.77	1364.99	4322.98	2933.99						
QUNC	368.87	1233.27	3228.48	5224.42	1125.70	1611.52						
OCNL	.00	.00	.00	.60	6652.27	17177.72						
GSIT	3712.87	4534.27	7323.39	19920.42	41924.82	15424.85						
QIFS	.00	1135.46	3613.38	4485.65	4573.97	10289.74						
QGLI	.00	.00	.00	.00	.00	.00						
SNH	5996.48	5757.53	4117.33	.00	.00	.00						
SNHT	.00	1135.46	3613.38	4117.32	.00	.00						
ETPH	.00	.00	.00	.00	.00	.00						
ET	637.70	840.33	1388.70	3434.00	7740.10	10347.55						
ETP	629.45	393.31	1342.43	3442.22	7746.33	10334.42						
MS	5009.20	6378.17	8654.60	9737.47	6635.09	5536.50						
NP	452.34	488.27	488.27	488.27	417.00	346.84						
QTC	4226.49	5022.89	7797.60	19346.48	42151.61	15736.60						
QTD	24.62	64.23	64.23	25.69	36.33	64.23						
QSN	4200.73	4958.66	7733.45	19320.79	44277.27	15672.45						

POTS 14 THRU 24 SHOULD BE SPT AS FOLLOWS
 19044 21275 23571 24909 21044
 20874 22430 22838 23067 23063
 19040 22834 23075 23000 23490

POTS 14 THRU 24 ARE SPT AS FOLLOWS
 20047 21257 23544 24907 20974
 20844 22838 23066 23067 23063
 19944 20876 23075 23000 23490

EVANSTON CASE 1 - 2												
VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	19.20	14.70	24.43	34.28	47.34	54.90						
F	.85	.60	1.62	3.27	4.77	5.59						
PRT	1489.62	2131.03	1249.14	499.37	3373.85	3020.55						
GRV	2442.99	4771.37	2480.39	4774.72	4623.97	4306.98						
QUNC	107.34	116.12	133.25	7845.06	1630.79	1440.19						
OCNL	.00	777.36	1316.43	.00	.00	1772.95						
GSIT	2727.34	1952.66	2113.25	16620.25	43068.77	34602.05						
QIFS	.00	295.46	581.89	7339.34	3394.54	3771.57						
QGLI	.00	.00	.00	.00	.00	.00						
SNH	3424.19	6561.23	6940.36	.00	.00	.00						
SNHT	.00	.00	.00	.00	.00	.00						
ETPH	.00	.00	.00	.00	.00	.00						
ET	352.77	515.31	1973.64	2234.47	6006.62	10394.72						
ETP	372.54	526.67	1071.93	2328.17	6847.07	10488.98						
MS	2251.82	4076.25	5656.01	13540.38	7200.33	6480.34						
NP	57.86	34.53	14.26	25.89	19.24	32.11						
QTC	2432.44	1970.37	2176.79	15610.72	49792.14	34774.83						
QTD	64.23	64.23	64.23	25.69	36.33	64.23						
QSN	2432.17	1914.79	2162.54	14504.58	49755.87	34755.81						

EVANSTON CASE 1 - 2												
VAR	JAN	FEB	MAR	APR	MAY	JUN	JULY	AUG	SEP	OCT	NOV	DEC
TEMP	19.20	14.70	24.43	34.28	47.34	54.90						
F	.85	.60	1.62	3.27	4.77	5.59						
PRT	1489.62	2131.03	1249.14	499.37	3373.85	3020.55						
GRV	2442.99	4771.37	2480.39	4774.72	4623.97	4306.98						
QUNC	107.34	116.12	133.25	7845.06	1630.79	1440.19						
OCNL	.00	777.36	1316.43	.00	.00	1772.95						
GSIT	2727.34	1952.66	2113.25	16620.25	43068.77	34602.05						
QIFS	.00	295.46	581.89	7339.34	3394.54	3771.57						
QGLI	.00	.00	.00	.00	.00	.00						
SNH	3424.19	6561.23	6940.36	.00	.00	.00						
SNHT	.00	.00	.00	.00	.00	.00						
ETPH	.00	.00	.00	.00	.00	.00						
ET	352.77	515.31	1973.64	2234.47	6006.62	10394.72						
ETP	372.54	526.67	1071.93	2328.17	6847.07	10488.98						
MS	2251.82	4076.25	5656.01	13540.38	7200.33	6480.34						
NP	57.86	34.53	14.26	25.89	19.24	32.11						
QTC	2432.44	1970.37	2176.79	15610.72	49792.14	34774.83						
QTD	64.23	64.23	64.23	25.69	36.33	64.23						
QSN	2432.17	1914.79	2162.54	14504.58	49755.87	34755.81						

EVANSTON CASE 2 -1

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	22.10	24.20	24.70	40.60	49.70	54.80
F	1.45	1.62	2.05	3.65	5.01	5.58
PPT	453.92	223.66	493.37	92.09	513.10	940.78
DRIV	3223.99	3300.99	4097.99	13691.99	43322.97	28339.99
QUNG	388.87	1233.27	3225.36	5228.42	1129.78	1811.39
QCNL	.00	.00	.00	.00	.00	.00
OSIT	5549.19	4326.37	7037.54	18225.92	42424.98	18442.38
OIGS	.00	283.91	963.49	1121.59	1162.85	2630.68
QGLI	.00	.00	.00	.00	.00	.00
SNW	1499.85	1439.61	1029.49	.00	.00	.00
SNMT	.00	283.91	963.49	1029.49	.00	.00
ETPH	166.48	205.90	285.81	693.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2587.32
ET	157.39	202.36	335.66	876.89	1981.85	2584.11
MS	1504.83	1504.79	2190.12	2417.08	1681.21	1947.79
DP	134.99	139.30	139.08	117.24	184.39	86.72
OTO	3688.10	4448.72	7156.59	18340.95	26310.91	18587.98
GGO	6.42	5.42	5.42	9.63	9.63	22.48
QSO	3661.76	4442.30	7150.08	18341.31	26311.28	18485.49

EVANSTON CASE 2 -1

1954

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	22.10	24.20	24.70	40.60	49.70	54.80
F	1.45	1.62	2.05	3.65	5.01	5.58
PPT	453.92	223.66	493.37	92.09	513.10	940.78
DRIV	3223.99	3300.99	4097.99	13691.99	43322.97	28339.99
QUNG	388.87	1233.27	3225.36	5228.42	1129.78	1811.39
QCNL	.00	.00	.00	.00	.00	.00
OSIT	5549.19	4326.37	7037.54	18225.92	42424.98	18442.38
OIGS	.00	283.91	963.49	1121.59	1162.85	2630.68
QGLI	.00	.00	.00	.00	.00	.00
SNW	1499.85	1439.61	1029.49	.00	.00	.00
SNMT	.00	283.91	963.49	1029.49	.00	.00
ETPH	166.48	205.90	285.81	693.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2587.32
ET	157.39	202.36	335.66	876.89	1981.85	2584.11
MS	1504.83	1504.79	2190.12	2417.08	1681.21	1947.79
DP	134.99	139.30	139.08	117.24	184.39	86.72
OTO	3688.10	4448.72	7156.59	18340.95	26310.91	18587.98
GGO	6.42	5.42	5.42	9.63	9.63	22.48
QSO	3661.76	4442.30	7150.08	18341.31	26311.28	18485.49

POTS TO THRU 24 SHOULD BE SET AS FOLLOWS

10000	01275	03571	04999	01000
00000	00000	02000	00000	00000
10000	00000	00000	00000	00000

POTS TO THRU 24 ARE SET AS FOLLOWS

00000	01275	03540	04997	00000
00000	00000	02000	00000	00000
00000	00000	00000	00000	00000

EVANSTON CASE 2 -1

1955

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	12.20	14.70	20.30	34.20	47.30	54.90
F	.90	.95	1.68	3.07	4.77	5.59
PPT	374.96	532.84	322.31	124.98	848.60	750.58
DRIV	2442.99	2171.99	2460.99	8774.99	40232.97	40962.99
QUNG	130.74	116.12	153.25	7845.20	1635.79	1483.19
QCNL	.00	.00	.00	.00	.00	.00
OSIT	2491.44	2103.05	2370.35	1618.82	48057.12	38277.95
OIGS	.00	.00	.00	.00	.00	.00
QGLI	.00	.00	.00	.00	.00	.00
SNW	855.18	1388.72	1713.35	.00	.00	.00
SNMT	.00	.00	.00	1710.18	.00	.00
ETPH	91.29	125.27	234.90	451.24	1211.64	1827.31
ETP	88.93	128.84	268.94	558.70	1781.78	2599.11
ET	93.19	131.59	273.02	566.93	1785.61	2598.55
MS	2412.38	1883.88	1939.25	2881.23	2044.48	1846.18
DP	9.63	9.63	9.63	4.81	8.83	5.42
OTO	2482.93	2155.30	3379.51	16172.40	29284.41	28290.84
GGO	12.84	6.42	19.27	12.84	9.63	12.84
QSO	2472.98	2148.87	3391.23	16159.95	29274.78	28277.99

EVANSTON CASE 2 -1

1956

VAR	JAN	FEB	MAR	APR	MAY	JUN
TEMP	22.20	19.70	25.20	35.50	48.30	58.90
F	1.33	1.71	2.89	3.19	4.87	6.80
PPT	795.07	230.24	46.34	256.55	1020.17	443.74
DRIV	3617.99	2833.99	6129.99	13039.99	69355.96	93111.98
QUNG	509.54	385.51	7191.34	4372.22	2938.88	515.07
QCNL	.00	.00	.00	.00	.00	.00
OSIT	1548.54	2995.17	13029.75	15943.58	71219.14	55814.94
OIGS	126.87	133.30	1846.34	1285.56	1526.22	1275.78
QGLI	.00	.00	.00	.00	.00	.00
SNW	2519.50	2749.74	949.44	.00	.00	.00
SNMT	.00	.00	1846.34	949.41	.00	.00
ETPH	152.14	91.73	251.80	468.02	1279.70	2174.07
ETP	145.75	93.78	333.85	583.22	1797.36	3091.99
ET	138.11	91.54	335.66	581.38	1809.36	3073.22
MS	1511.28	1559.48	3073.95	3719.37	3457.70	1647.79
DP	8.83	8.83	9.63	9.63	8.83	6.03
OTO	3549.49	2987.23	13912.12	18927.84	26298.34	26310.91
GGO	9.63	12.84	6.42	12.84	9.63	22.48
QSO	3632.85	2974.38	13905.69	18914.79	26291.27	26288.43

EVANSTON CASE 2 -2

	JAN	FEB	MAR	APR	MAY	JUN
VAR	22.13	24.20	24.70	40.60	49.70	54.80
TEMP	1.45	1.62	2.05	3.65	5.01	5.58
F	453.90	223.66	453.37	92.49	513.10	940.70
PPT	3323.92	3300.99	4097.99	13691.99	43322.97	20337.99
QRTV	368.67	1233.27	3225.36	5228.42	1129.70	1611.59
QUNG	.00	.00	.00	.00	1642.23	4326.53
OCNL	3946.19	4328.37	7837.54	18226.92	42456.67	18490.86
OSIT	.00	.00	903.49	1121.50	1137.15	2582.50
QIGS	.00	.00	.00	.00	.00	.00
QGLI	1499.85	1439.61	1029.49	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00
SNMT	283.91	983.49	1029.49	.00	.00	.00
ETPH	166.49	205.90	285.81	593.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2507.32
ET	157.39	292.36	324.41	862.44	1941.76	2584.11
MS	1500.83	1594.79	2127.95	2442.78	1649.46	1659.63
DP	138.11	136.51	130.96	117.24	195.99	91.54
QTC	3671.40	4442.30	7148.86	18321.66	26318.91	18575.43
QSC	6.42	16.76	16.06	12.84	9.63	22.48
QSO	3664.97	4426.24	7130.80	18306.83	26301.22	16552.95

PPTS IN THRU 24 SHOULD BE SET AS FOLLOWS

	JAN	FEB	MAR	APR	MAY	JUN
VAR	22.13	24.20	24.70	40.60	49.70	54.80
TEMP	1.45	1.62	2.05	3.65	5.01	5.58
F	453.90	223.66	453.37	92.49	513.10	940.70
PPT	3323.92	3300.99	4097.99	13691.99	43322.97	20337.99
QRTV	368.67	1233.27	3225.36	5228.42	1129.70	1611.59
QUNG	.00	.00	.00	.00	1642.23	4326.53
OCNL	3946.19	4328.37	7837.54	18226.92	42456.67	18490.86
OSIT	.00	.00	903.49	1121.50	1137.15	2582.50
QIGS	.00	.00	.00	.00	.00	.00
QGLI	1499.85	1439.61	1029.49	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00
SNMT	283.91	983.49	1029.49	.00	.00	.00
ETPH	166.49	205.90	285.81	593.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2507.32
ET	157.39	292.36	324.41	862.44	1941.76	2584.11
MS	1500.83	1594.79	2127.95	2442.78	1649.46	1659.63
DP	138.11	136.51	130.96	117.24	195.99	91.54
QTC	3671.40	4442.30	7148.86	18321.66	26318.91	18575.43
QSC	6.42	16.76	16.06	12.84	9.63	22.48
QSO	3664.97	4426.24	7130.80	18306.83	26301.22	16552.95

PPTS 12 THRU 24 ARE SET AS FOLLOWS

	JAN	FEB	MAR	APR	MAY	JUN
VAR	22.13	24.20	24.70	40.60	49.70	54.80
TEMP	1.45	1.62	2.05	3.65	5.01	5.58
F	453.90	223.66	453.37	92.49	513.10	940.70
PPT	3323.92	3300.99	4097.99	13691.99	43322.97	20337.99
QRTV	368.67	1233.27	3225.36	5228.42	1129.70	1611.59
QUNG	.00	.00	.00	.00	1642.23	4326.53
OCNL	3946.19	4328.37	7837.54	18226.92	42456.67	18490.86
OSIT	.00	.00	903.49	1121.50	1137.15	2582.50
QIGS	.00	.00	.00	.00	.00	.00
QGLI	1499.85	1439.61	1029.49	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00
SNMT	283.91	983.49	1029.49	.00	.00	.00
ETPH	166.49	205.90	285.81	593.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2507.32
ET	157.39	292.36	324.41	862.44	1941.76	2584.11
MS	1500.83	1594.79	2127.95	2442.78	1649.46	1659.63
DP	138.11	136.51	130.96	117.24	195.99	91.54
QTC	3671.40	4442.30	7148.86	18321.66	26318.91	18575.43
QSC	6.42	16.76	16.06	12.84	9.63	22.48
QSO	3664.97	4426.24	7130.80	18306.83	26301.22	16552.95

EVANSTON CASE 2 -2

	JAN	FEB	MAR	APR	MAY	JUN
VAR	22.13	24.20	24.70	40.60	49.70	54.80
TEMP	1.45	1.62	2.05	3.65	5.01	5.58
F	453.90	223.66	453.37	92.49	513.10	940.70
PPT	3323.92	3300.99	4097.99	13691.99	43322.97	20337.99
QRTV	368.67	1233.27	3225.36	5228.42	1129.70	1611.59
QUNG	.00	.00	.00	.00	1642.23	4326.53
OCNL	3946.19	4328.37	7837.54	18226.92	42456.67	18490.86
OSIT	.00	.00	903.49	1121.50	1137.15	2582.50
QIGS	.00	.00	.00	.00	.00	.00
QGLI	1499.85	1439.61	1029.49	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00
SNMT	283.91	983.49	1029.49	.00	.00	.00
ETPH	166.49	205.90	285.81	593.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2507.32
ET	157.39	292.36	324.41	862.44	1941.76	2584.11
MS	1500.83	1594.79	2127.95	2442.78	1649.46	1659.63
DP	138.11	136.51	130.96	117.24	195.99	91.54
QTC	3671.40	4442.30	7148.86	18321.66	26318.91	18575.43
QSC	6.42	16.76	16.06	12.84	9.63	22.48
QSO	3664.97	4426.24	7130.80	18306.83	26301.22	16552.95

PPTS IN THRU 24 SHOULD BE SET AS FOLLOWS

	JAN	FEB	MAR	APR	MAY	JUN
VAR	22.13	24.20	24.70	40.60	49.70	54.80
TEMP	1.45	1.62	2.05	3.65	5.01	5.58
F	453.90	223.66	453.37	92.49	513.10	940.70
PPT	3323.92	3300.99	4097.99	13691.99	43322.97	20337.99
QRTV	368.67	1233.27	3225.36	5228.42	1129.70	1611.59
QUNG	.00	.00	.00	.00	1642.23	4326.53
OCNL	3946.19	4328.37	7837.54	18226.92	42456.67	18490.86
OSIT	.00	.00	903.49	1121.50	1137.15	2582.50
QIGS	.00	.00	.00	.00	.00	.00
QGLI	1499.85	1439.61	1029.49	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00
SNMT	283.91	983.49	1029.49	.00	.00	.00
ETPH	166.49	205.90	285.81	593.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2507.32
ET	157.39	292.36	324.41	862.44	1941.76	2584.11
MS	1500.83	1594.79	2127.95	2442.78	1649.46	1659.63
DP	138.11	136.51	130.96	117.24	195.99	91.54
QTC	3671.40	4442.30	7148.86	18321.66	26318.91	18575.43
QSC	6.42	16.76	16.06	12.84	9.63	22.48
QSO	3664.97	4426.24	7130.80	18306.83	26301.22	16552.95

PPTS 12 THRU 24 ARE SET AS FOLLOWS

	JAN	FEB	MAR	APR	MAY	JUN
VAR	22.13	24.20	24.70	40.60	49.70	54.80
TEMP	1.45	1.62	2.05	3.65	5.01	5.58
F	453.90	223.66	453.37	92.49	513.10	940.70
PPT	3323.92	3300.99	4097.99	13691.99	43322.97	20337.99
QRTV	368.67	1233.27	3225.36	5228.42	1129.70	1611.59
QUNG	.00	.00	.00	.00	1642.23	4326.53
OCNL	3946.19	4328.37	7837.54	18226.92	42456.67	18490.86
OSIT	.00	.00	903.49	1121.50	1137.15	2582.50
QIGS	.00	.00	.00	.00	.00	.00
QGLI	1499.85	1439.61	1029.49	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00
SNMT	283.91	983.49	1029.49	.00	.00	.00
ETPH	166.49	205.90	285.81	593.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2507.32
ET	157.39	292.36	324.41	862.44	1941.76	2584.11
MS	1500.83	1594.79	2127.95	2442.78	1649.46	1659.63
DP	138.11	136.51	130.96	117.24	195.99	91.54
QTC	3671.40	4442.30	7148.86	18321.66	26318.91	18575.43
QSC	6.42	16.76	16.06	12.84	9.63	22.48
QSO	3664.97	4426.24	7130.80	18306.83	26301.22	16552.95

EVANSTON CASE 2 -2

	JAN	FEB	MAR	APR	MAY	JUN
VAR	22.13	24.20	24.70	40.60	49.70	54.80
TEMP	1.45	1.62	2.05	3.65	5.01	5.58
F	453.90	223.66	453.37	92.49	513.10	940.70
PPT	3323.92	3300.99	4097.99	13691.99	43322.97	20337.99
QRTV	368.67	1233.27	3225.36	5228.42	1129.70	1611.59
QUNG	.00	.00	.00	.00	1642.23	4326.53
OCNL	3946.19	4328.37	7837.54	18226.92	42456.67	18490.86
OSIT	.00	.00	903.49	1121.50	1137.15	2582.50
QIGS	.00	.00	.00	.00	.00	.00
QGLI	1499.85	1439.61	1029.49	.00	.00	.00
SNW	.00	.00	.00	.00	.00	.00
SNMT	283.91	983.49	1029.49	.00	.00	.00
ETPH	166.49	205.90	285.81	593.49	1377.94	1819.21
ETP	159.46	212.11	327.23	858.64	1935.36	2507.32
ET	157.39	292.36	324.41	862.44	1941.76	2584.11
MS	1500.83	1594.79	2127.95	2442.78	1649.46	1659.63
DP	138.11	136.51	130.96	117.24	195.99	91.54
QTC	3671.40	4442.30	7148.86	18321.66	26318.91	18575.43
QSC	6.42	16.76	16.06	12.84	9.63	22.48

EVANSTON CASE 3 -1

Table with 12 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and multiple rows of numerical data.

POTS 10 THRU 24 SHOULD BE SET AS FOLLOWS

Table with 12 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and 3 rows of numerical data.

POTS 10 THRU 24 ARE SET AS FOLLOWS

Table with 12 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and 3 rows of numerical data.

EVANSTON CASE 3 -1

Table with 12 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and multiple rows of numerical data.

EVANSTON CASE 3 -1

Table with 12 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and multiple rows of numerical data.

EVANSTON CASE 3 -1

Table with 12 columns (VAR, JAN, FEB, MAR, APR, MAY, JUN, JUL, AUG, SEP, OCT, NOV, DEC, ANN) and multiple rows of numerical data.

