

# Autonomous Navigation using Gravity Gradient Measurements

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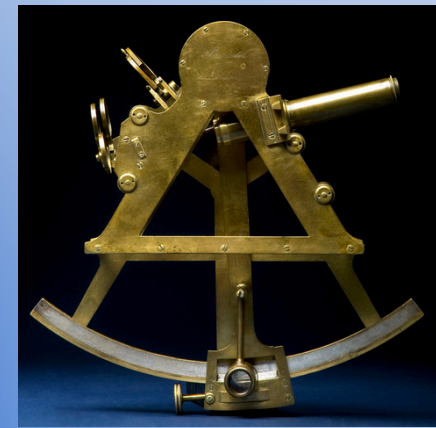
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Student Research Symposium





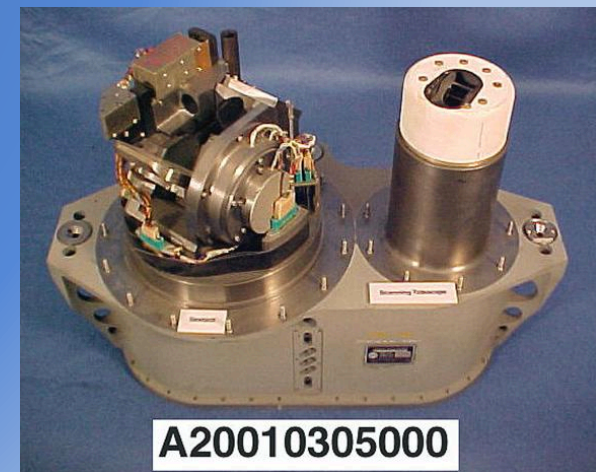
The art of navigation was first developed with the need to explore sea. Earliest records show that navigation is older than 1000 B.C.



Where?

When?

On 21<sup>st</sup> Dec 1968, with the launch of Apollo 8 mission, we pioneered Space Navigation.



# Satellite Navigation Systems

## Global Navigation Satellite System (GNSS)

Operational

In Development

1. GPS (USA)
2. G L O N A S S (Russia)

1. Galileo (EU)
2. Compass (China)

## Regional Navigation Satellite System (RNSS)

Operational

In Development

1. NAVIC (India)
2. B e i D o u (China)

1. QZSS (Japan)

## Current GNSS

1. Strong Dependence on Ground-Based Infrastructure ⇒ Low Accuracy
2. Range Limitation, Constant Maintenance Requirement, & Continuous Tracking ⇒ Unsuitable for Beyond Earth Exploration Missions

## Autonomous Navigation

1. Self-Contained & Passive System ⇒ Enhanced Accuracy
2. Autonomous, Resistant to Signal Blockage & Spoofing ⇒ Suitable for Beyond Earth Exploration Missions

GPS/STST

Onboard Optical  
Systems

IMU

Magnetometer  
Measurement Gradient

Conventional  
Space Navigation  
Techniques



Gamma Ray  
Photons

Autonomous  
Navigation

Starlight  
Refraction

Star  
Tracker

Delta-DOR

Doppler

X-ray  
Pulsars

Gravity  
Gradient

Conventional  
Space  
Navigation



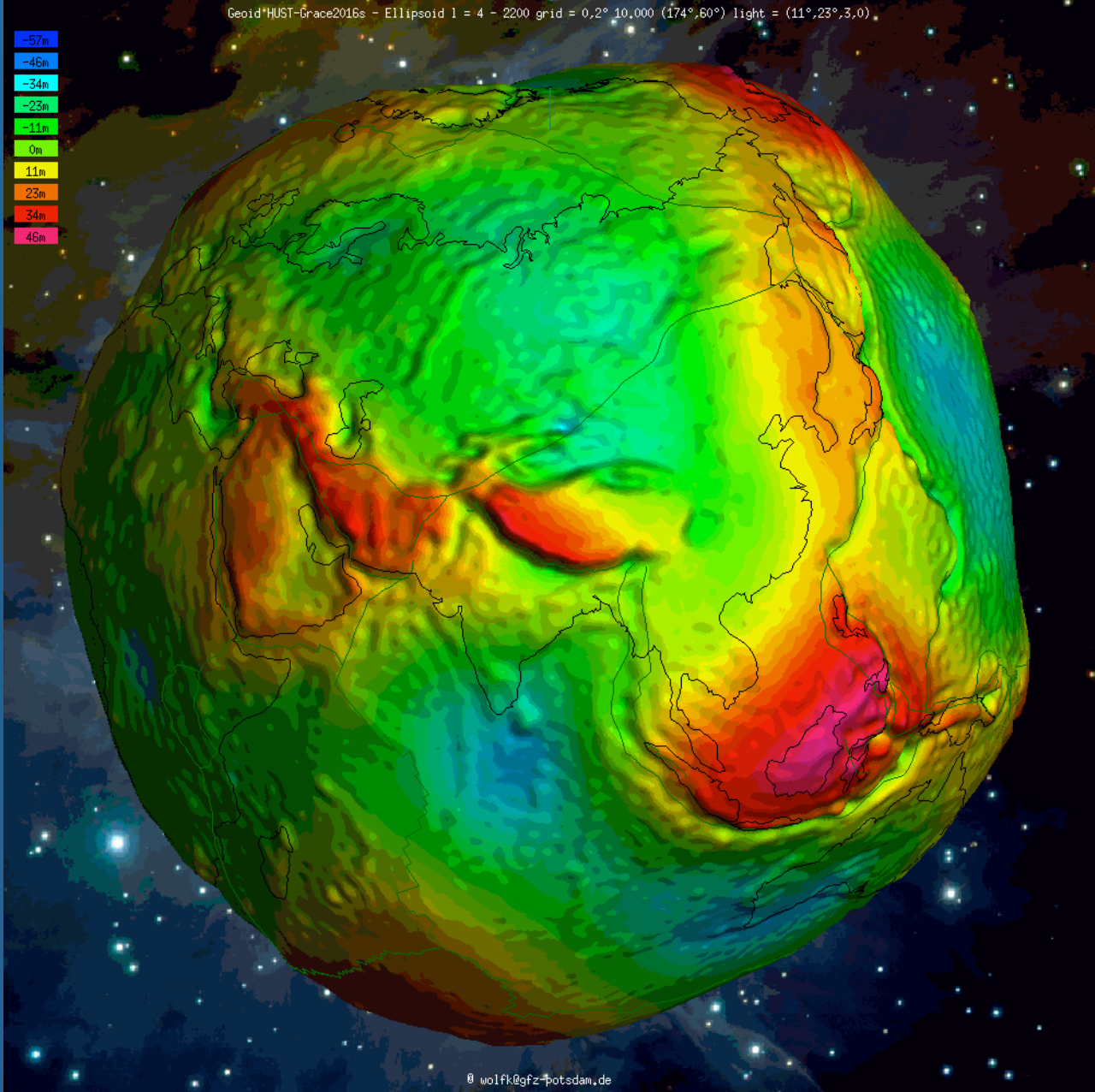
Gravity  
Gradiometry



Autonomous  
Space  
Navigation

The Gravity Gradiometry has been in use since mid 20th century, mostly for Marine Navigation & the survey of Mineral/Oil Fields.

However, the space application of the Gravity Gradiometer has been very limited.



Source- International Center for Global Earth Models (ICGEM), the model used is HUST-Grace2016s, with Orion Nebula in the background.

The Gravity Gradient Tensor ( $\nabla g$ ) is defined as the second order derivative of the gravitational potential  $U$ :

$$\nabla g_{ij} = \partial^2 U / \partial r_i \partial r_j, \quad i, j = X, Y, Z$$

$r$  is Position vector

$$\nabla g = \begin{bmatrix} \nabla g_{XX} & \nabla g_{XY} & \nabla g_{XZ} \\ \nabla g_{XY} & \nabla g_{YY} & \nabla g_{YZ} \\ \nabla g_{XZ} & \nabla g_{ZY} & \nabla g_{ZZ} \end{bmatrix} \text{ (Cesare S., 2008)}$$



Artist's view of the GOCE satellite (image credit: ESA-AOES MediaLab)



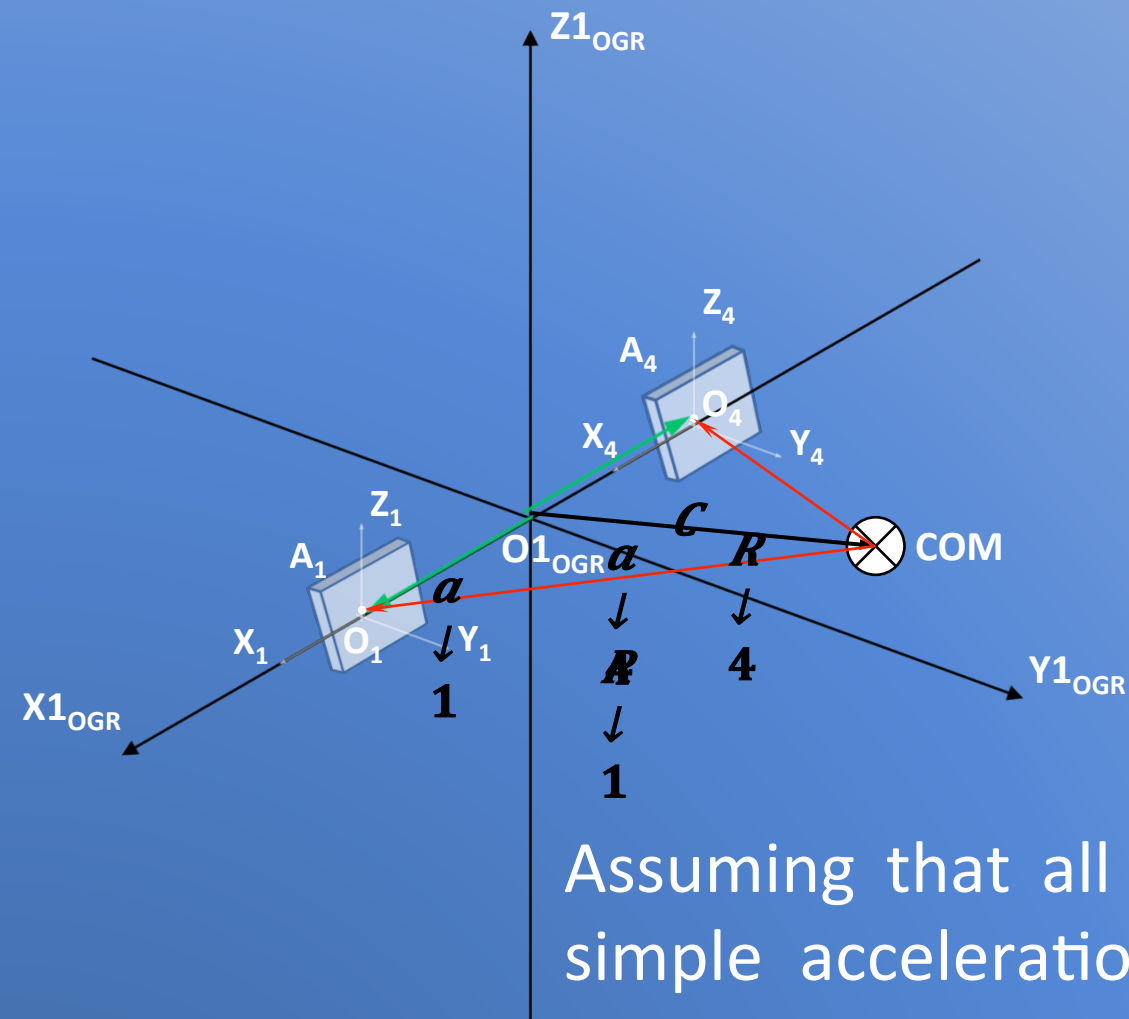
# History of Gravity Gradiometer Instruments(Richeson J.A., 2008)

Gradiometer	Developer	Noise, 1- $\sigma$ Eö	Data Rate,sec
Rotating Accel. GGI	Bell Aerospace/Textron	2(Lab.),10 (Air)	10
Rotating Torque GGI	Hughes Research Lab	0.5(Goal)	10
Floated GGI	Draper Lab	1(Lab.)	10
Falcon AGG	LM/BHP Billiton	3	Post Survey
ACVGG	Lockheed Martin(LM)	1	1
3D FTG	LM/Bell Geospace	5	Post Survey
FTGeX	LM/ARKeX	10(Goal)	1
UMD SGG (Space)	Univ. of Maryland	0.02(Lab.)	1
UMD SAA (Air)	Univ. of Maryland	0.3(Lab.)	1
UWA OQR	Univ. of Western Australia	1(Lab.)	1
Exploration GGI	ARKeX	1(Goal)	1
HD-AGG	Gedex/UMD/UWA	1(Goal)	1
Electrostatic GGI	European Space Agency	0.001(Goal)	10
Cold Atom Interfer.	Stanford Univ./JPL	30(Lab.)	1



1 Accelerometer pair      3 Isostatic X-frame      5 Intermediate tray  
2 Ultra-stable carbon-carbon structure      4 Panel regulated by heaters      6 Electronic panel structure

**Illustration of EGG system onboard GOCE (image credit:ESA,ONERA)**



The objective is to use 6 accelerometers arranged on a distance of 1 meters, on three mutually perpendicular baselines, as shown in the figure. (Cesare S., 2008)

Assuming that all perturbations, except drag are negligible. A simple acceleration Measurement Model (ECI frame) can be defined as:-

$$a \downarrow i = a \downarrow grav (r \downarrow Sc) - a \downarrow grav (r \downarrow Sc + R \downarrow i) + a \downarrow drag (r \downarrow Sc, V \downarrow Sc) + \omega \times (\omega \times R \downarrow i) + (\omega \times R \downarrow i) + 2\omega \times R \downarrow i + R \downarrow i$$

The accelerometer model can now be written as-:

$$a_{\downarrow i} = -(\nabla g - [\Omega \uparrow \Omega] - [\Omega])R_{\downarrow i} + 2[\Omega]R_{\downarrow i} + R_{\downarrow i} + D$$

where term  $(-\nabla g) R_{\downarrow i} = a_{\downarrow grav}(r_{\downarrow Sc}) - a_{\downarrow grav}(r_{\downarrow Sc} + R_{\downarrow i})$ ,

$[\Omega] = \begin{bmatrix} 0 & -\omega_{\downarrow Z} & \omega_{\downarrow Y} \\ \omega_{\downarrow Z} & 0 & -\omega_{\downarrow X} \\ -\omega_{\downarrow Y} & \omega_{\downarrow X} & 0 \end{bmatrix}$  is the cross-product matrix, and

$D$  is the acceleration due to non-gravitational forces, like Atmospheric Drag.

Assuming ideal case the 3 OAGRFs are coincident, we get:  $C_{\downarrow 1} = C_{\downarrow 2} = C_{\downarrow 3} = C$

The vectors  $R_{\downarrow i}$  and its derivatives can thus be expressed as-:

$$R_{\downarrow i} = A_{\downarrow i} - C, \quad R_{\downarrow i} = -C, \quad R_{\downarrow i} = -C$$

Rewriting the equation for  $a_{\downarrow i}$ , we get-:

$$a_{\downarrow i} = -(\nabla g - [\Omega \uparrow \Omega] - [\Omega]) (A_{\downarrow i} - C) + 2[\Omega](-C) - C + D$$

$$\Rightarrow a_{\downarrow i} = -(\nabla g - [\Omega \uparrow \Omega] - [\Omega]) A_{\downarrow i} + (\nabla g - [\Omega \uparrow \Omega] - [\Omega]) C - 2[\Omega]C - C + D$$

To isolate the Perturbation (Drag) and Gravity Gradient Tensor, we define following two modes-: (Cesare S., 2008)

1. Common-Mode Acceleration measured by the accelerometers  $A_{\downarrow i}$ ,  $A_{\downarrow j}$  -:

$$a_{\downarrow c,ij} = 1/2 (a_{\downarrow i} + a_{\downarrow j})$$

$$\Rightarrow a_{\downarrow c,ij} = -(\nabla g - [\Omega \uparrow \Omega] - [\Omega]) A_{\downarrow c,ij} + (\nabla g - [\Omega \uparrow \Omega] - [\Omega]) C - 2[\Omega]C - C + D$$

where  $A_{\downarrow c,ij} = 1/2 (A_{\downarrow i} + A_{\downarrow j})$

To isolate the Perturbation (Drag) and Gravity Gradient Tensor, we define following two modes-: (Cesare S., 2008)

2. Differential-Mode Acceleration measured by the accelerometers  $A_{\downarrow i}$ ,  $A_{\downarrow j}$  -:

$$a_{\downarrow d,ij} = 1/2 (a_{\downarrow i} - a_{\downarrow j})$$

$$\Rightarrow a_{\downarrow d,ij} = -(\nabla g - [\Omega^2] - [\Omega]) A_{\downarrow d,ij}$$

where  $A_{\downarrow d,ij} = 1/2 (A_{\downarrow i} - A_{\downarrow j})$

Now, if the accelerometer  $A \downarrow i$ ,  $A \downarrow j$  belong to the same OAG ( $ij = 14, 25, 36$ ), then  $A \downarrow c, ij = 0$ , and  $A \downarrow d, ij = A \downarrow i$

1. Common-Mode Accel.  $\Rightarrow a \downarrow c, ij = (\nabla g - [\Omega \uparrow \Omega] - [\Omega])C - 2[\Omega]C - C + D$
2. Differential-Mode Accel.  $\Rightarrow a \downarrow d, ij = -(\nabla g - [\Omega \uparrow \Omega] - [\Omega])A \downarrow i$

Assuming  $c=0$ , i.e. COM of the Spacecraft is coincident with the center of all 3 OAGs.

Thus, ignoring terms  $(\nabla g - [\Omega \uparrow \Omega] - [\Omega \downarrow])C$ ,  $2[\Omega]C$ ,  $C$ , we get-:

$$a \downarrow d, ij = -(\nabla g - [\Omega \uparrow \Omega] - [\Omega \downarrow])A \downarrow i \qquad a \downarrow c, ij = D$$

Hence, using the common-mode, the non-gravitational force like drag, can be measured, while using the differential-mode, the GGT can be measured.



Results have been obtained for an Orbit defined as-:

Altitude = 400 km.

Eccentricity = 0.01

Inclination =  $\pi/6$  rad.

Right Ascension of the Ascending Node =  $\pi/6$  rad.

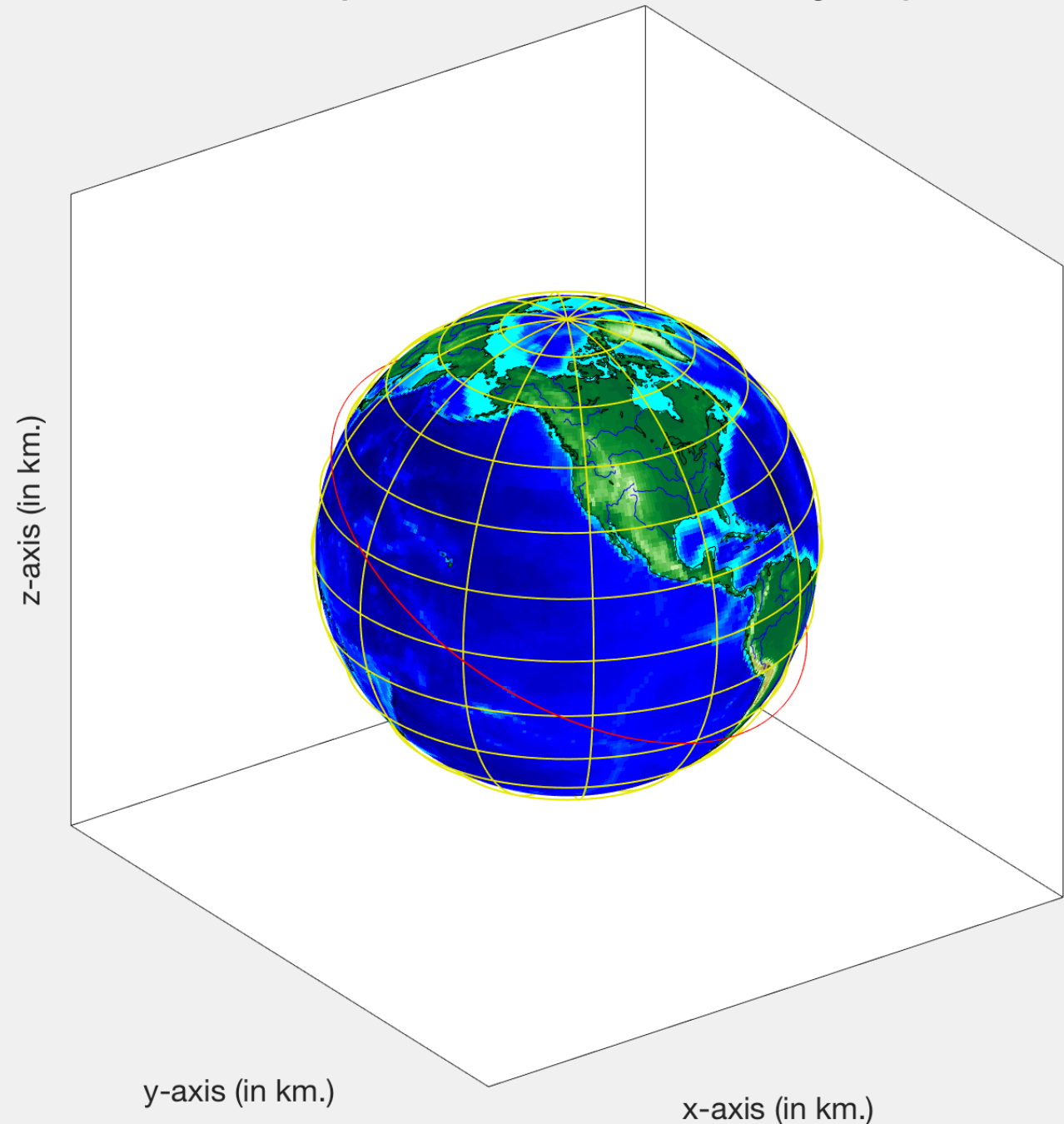
Argument of Periapsis =  $\pi/2$  rad.

True Anomaly = 0 rad.

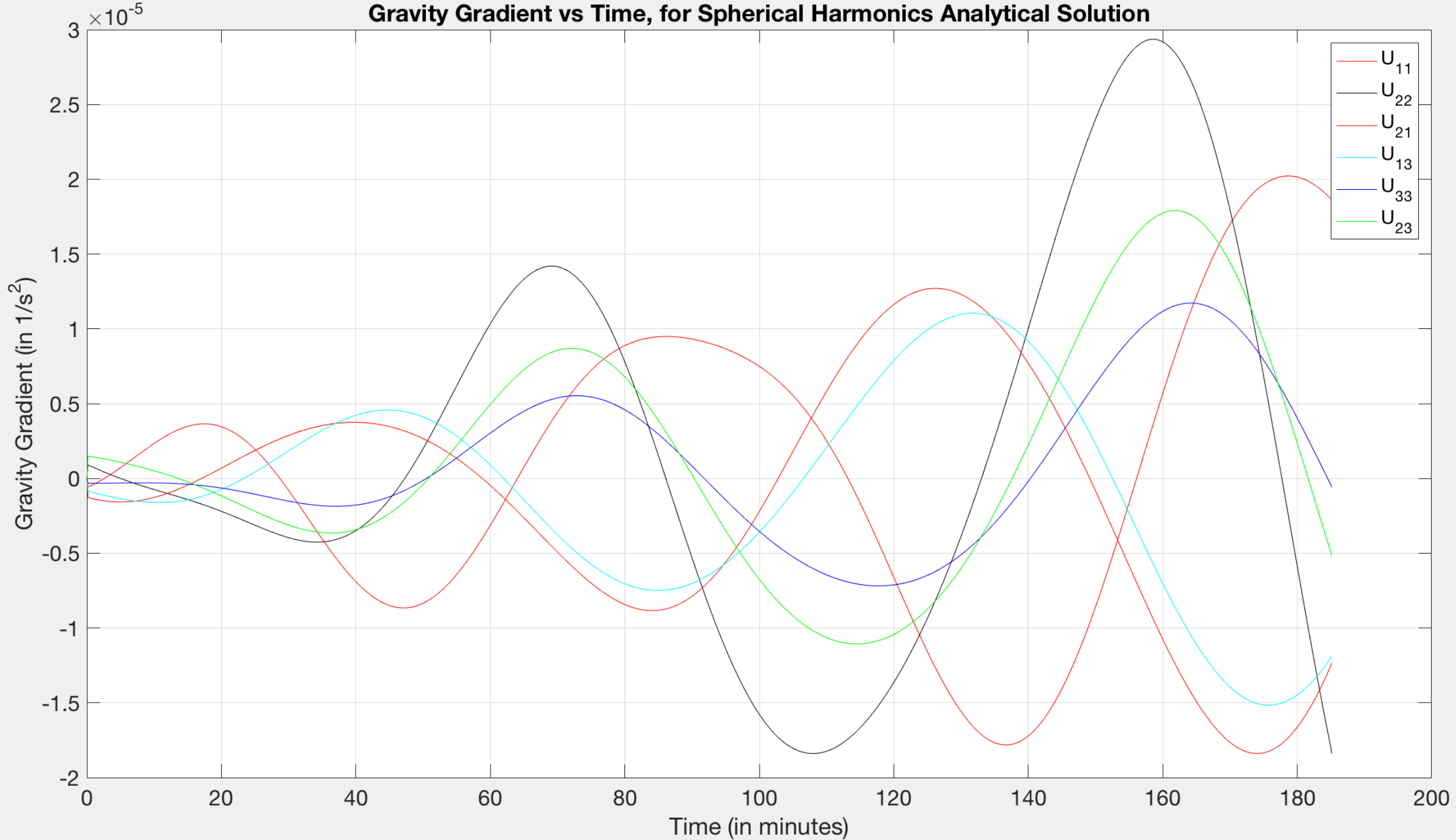
True Anomaly = 0 rad.

Results have been shown for an ideal Gravity Gradiometer Measurement Model, using 3x3 Spherical Harmonics Gravity Model

Simulated Orbit for Spherical Harmonics Model, using Analytical method



# Gravity Gradient vs Time, for Spherical Harmonics Analytical Solution



However, we can never have perfect measurements.

Hence, there is always a need for-:



Future work includes-:

- i. Formulate the Measurement Model with appropriate error model,
- ii. Implement Kalman Filter for Orbit Determination, and
- iii. Complete Covariance Analysis using techniques like Monte Carlo or Linear Covariance analysis
- iv. Identify various Error Sources, and determine the contribution of each.

# Backup Slide

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1960s-70s	Rotating Accel. GGI	Bell Aerospace/Textron	2(Lab.),10 (Air)	10
1960s-70s	Rotating Torque GGI	Hughes Research Lab	0.5(Goal)	10
1960s-70s	Floated GGI	Draper Lab	1(Lab.)	10
March'94	Falcon AGG	LM/BHP Billiton	3	Post Survey
	ACVGG	Lockheed Martin(LM)	1	1
	3D FTG	LM/Bell Geospace	5	Post Survey
2005	FTGeX	LM/ARKeX	10(Goal)	1
	UMD SGG (Space)	Univ. of Maryland	0.02(Lab.)	1
	UMD SAA (Air)	Univ. of Maryland	0.3(Lab.)	1
	UWA OQR	Univ. of Western Australia	1(Lab.)	1
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