



Update on Improving Launch Vibration Environments for CubeSats

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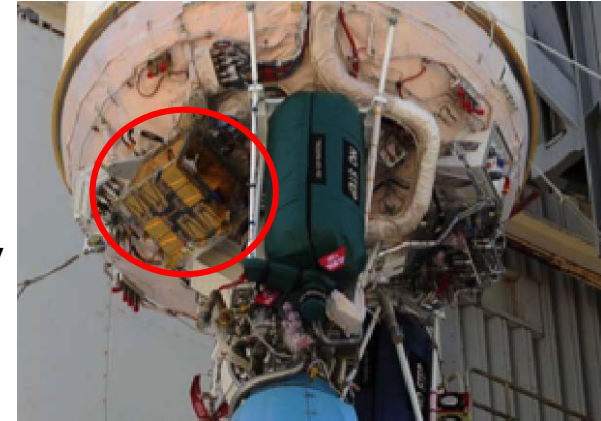
California Polytechnic State University, San Luis Obispo

Small Satellite Conference, Logan, Utah

August 8th, 2018

CubeSat Launch Environments

- CubeSat launch environments are typically bounded by random vibration environmental loads
 - Shock, acoustic, and quasi-static environments are typically considered non-damaging and only rarely require testing
 - Environments are defined at the payload dispenser interface
 - Actual CubeSat interface levels are not typically defined
- This is different from typical primary spacecraft environmental loads
 - Bounding environments: vibroacoustics, quasi-static loads, sine vibration
 - Environments are defined at the primary spacecraft interface



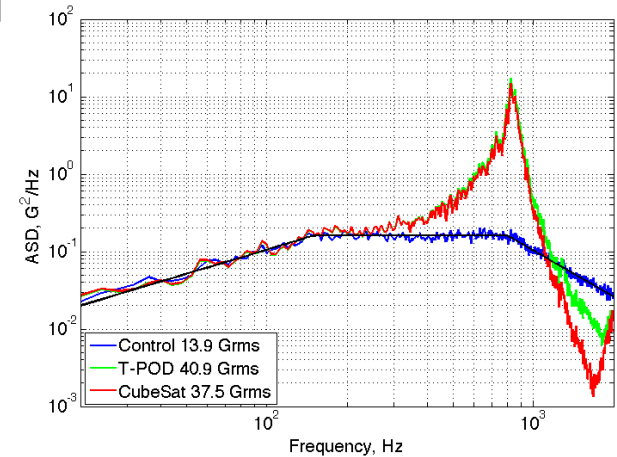
Credit: ULA



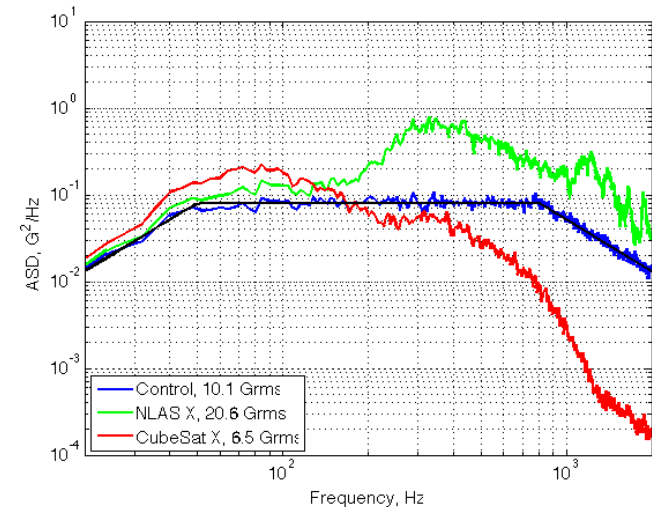
Credit: ULA

Review from Last Year

- Actual levels experienced by CubeSat vary due to a number of factors:
 - Launch vehicle/test specification
 - Dispenser and constraint method
 - Isolation implementation
- Free-constraint dispenser response is often 2-3 times higher than input levels, but CubeSat levels remain 1:1 or less
- Internal isolation demonstrated on the 3U P-POD
 - Consists of damping material embedded in dispenser to CubeSat interface contact points (rails)
 - Internally isolated CubeSat levels ranged from $3.7 G_{rms}$ to $4.4 G_{rms}$
 - Similar results expected with the 6U NLAS



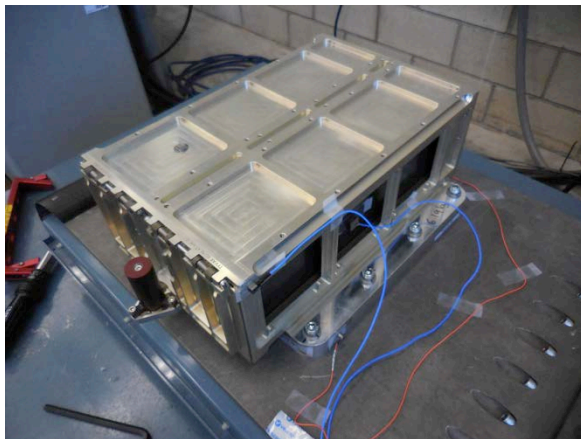
Dispenser and CubeSat Response almost 1:1!



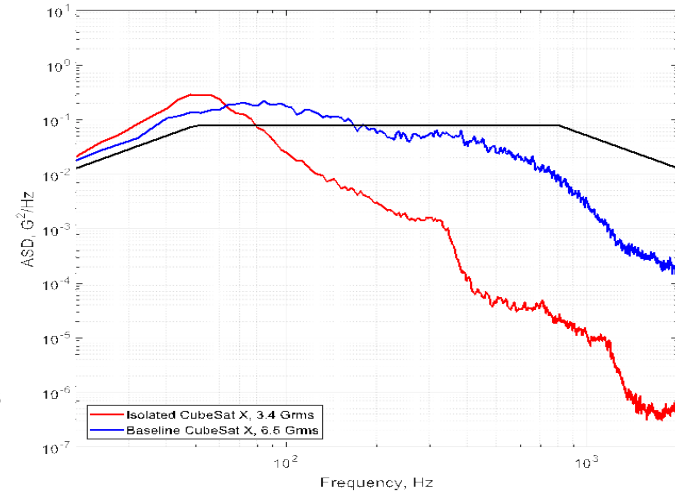
CubeSat Response in NLAS X-Axis

6U Isolation Testing Results

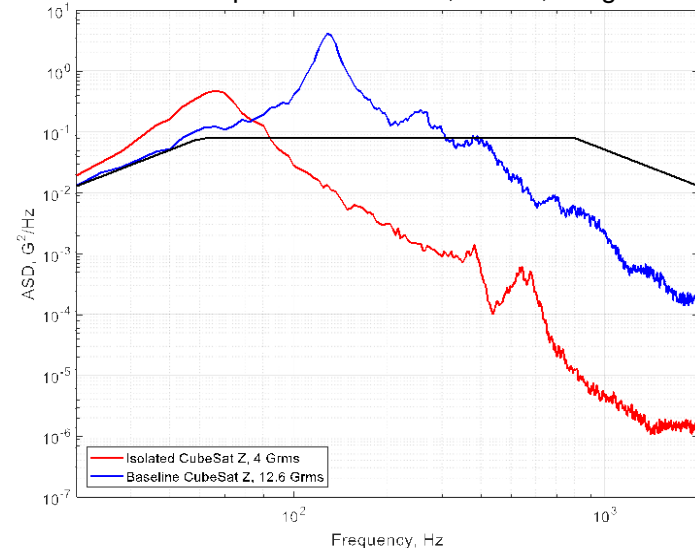
- After isolation incorporation, reduced environments were measured in all axis
 - Overall G_{rms} levels reduced by 17% - 71%
 - GEVS CubeSat response overall level ranged from 3.1 G_{rms} to 4.0 G_{rms}
 - Performance is sensitive to input spectrum. Better performance at higher frequency loading
 - Low first mode (between 50-60Hz)



Test Setup



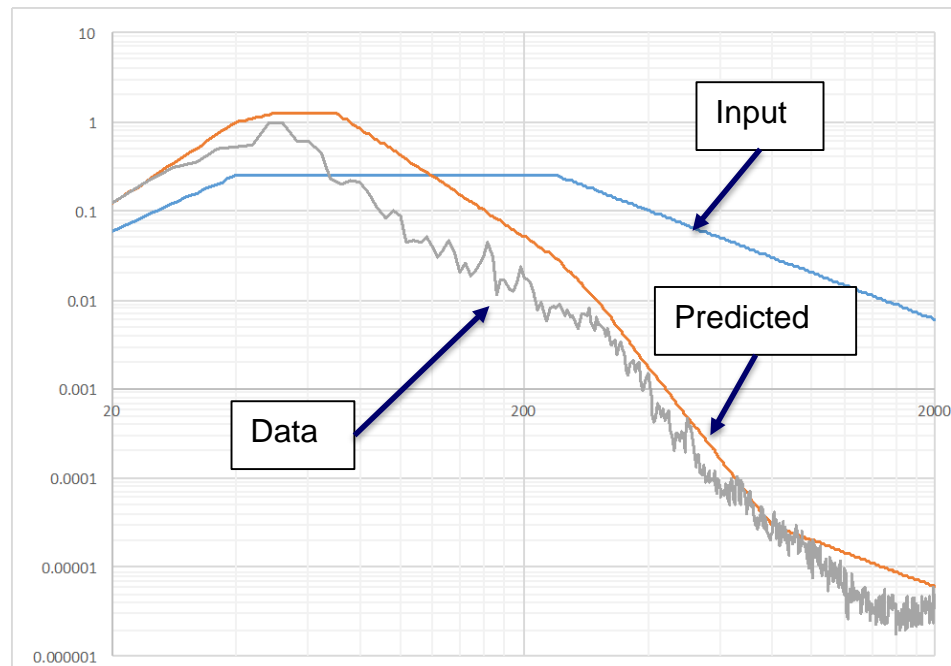
Sample Data – X Axis, GEVS, 14kg



Sample Data – Z Axis, GEVS, 14kg

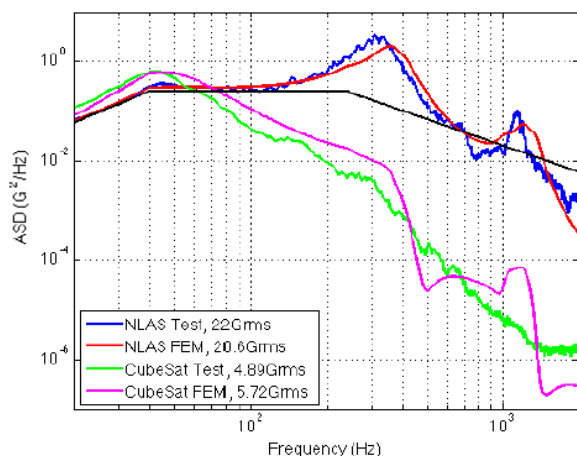
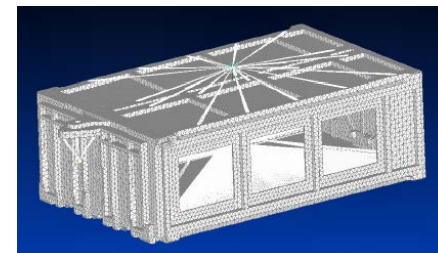
6U Payload Transfer Function

- Analyzing data sets for the 6U testing, a transfer function was developed which can be used to estimate payload environments for a variety of launch vehicle inputs
 - To leverage this capability, simply multiply the launch vehicle input by the transfer function to obtain the estimated payload environment
 - Enables rapid evaluation of environment, no need for complex analytical models.
- Low frequency amplification is seen as a result of the isolators. Roll off begins at 60-70 Hz and reduces vibe inputs by a factor of 10-100x starting at ~200Hz

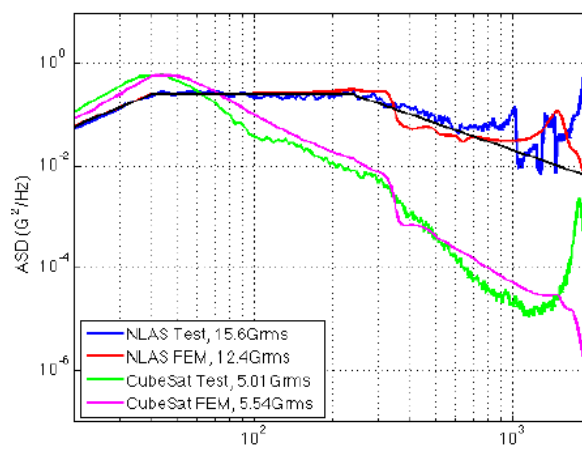


6U Finite Element Modeling

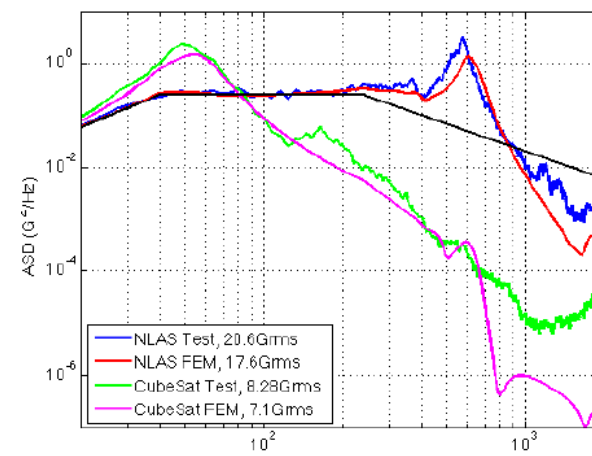
- A finite element modeling approach was used to investigate the ability to perform complex predictions
 - CubeSat is modeled as point mass at CG to simulate CubeSat simulator used in test
 - CubeSat is tied to dispenser using spring/damper elements
- Analytical response of CubeSat is extracted in PSD format and compared to measured response
 - Tuned model correlates to test data
 - Divergences in high frequencies due to mass model modes and not perfectly capturing high frequency dynamics when using point mass assumption



X-Axis



Y-Axis



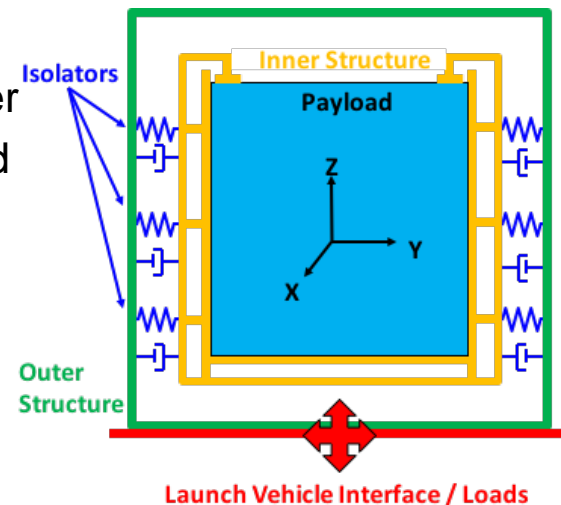
Z-Axis

12U Implementation

- Tyvak's 12U Rail Based Dispenser
 - Designed around internal isolation
- Retracting Rails allow for easier payload analysis
 - Contacts payload while integrated to reduce rail-to-rail free play
 - Analyzable boundary condition for payload developers
- Isolated Internal Structure
 - The 12U dispenser is unique in that it isolates the payload from the external dispenser structure through a unique load path approach
 - Utilizes bushings instead of constrained damping layer
 - Creates an analyzable boundary condition for payload developers



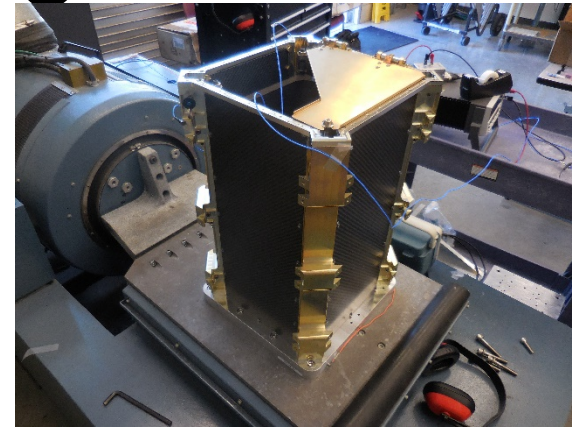
Credit: Tyvak



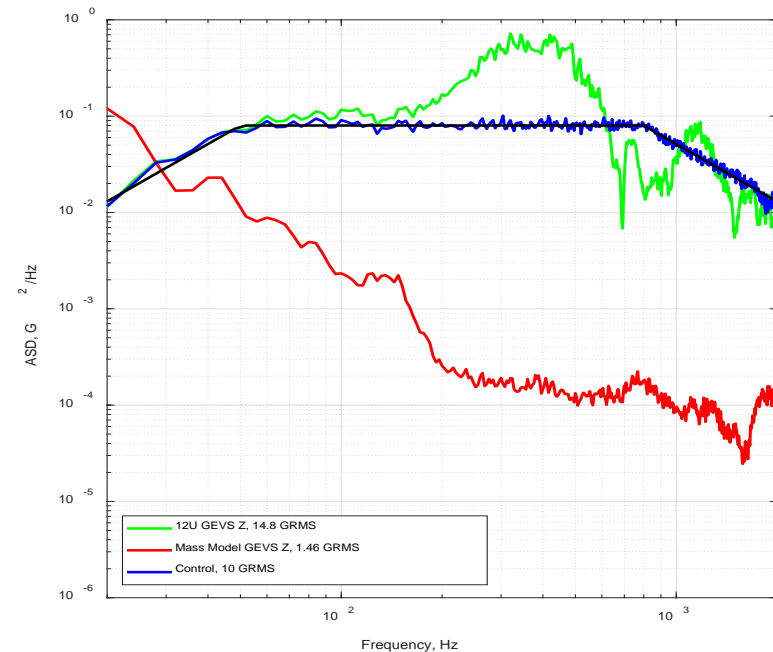
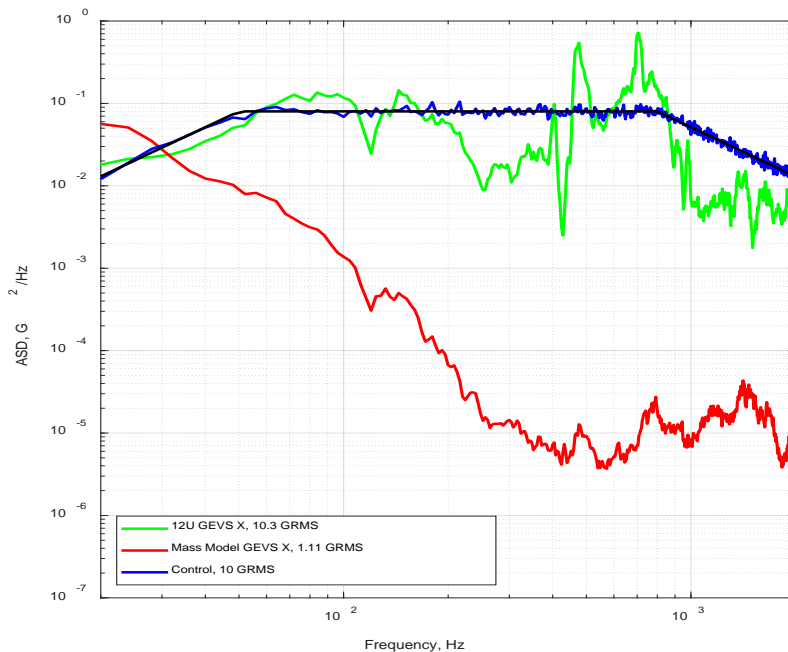
Internal Structure is Isolated from External
Credit: Tyvak

12U Isolation Testing Results

- Isolated design effectively reduces payload environments in all axis
 - Overall gRMS levels reduced by 77% - 93%
 - Low first mode (between 20 – 25 Hz)

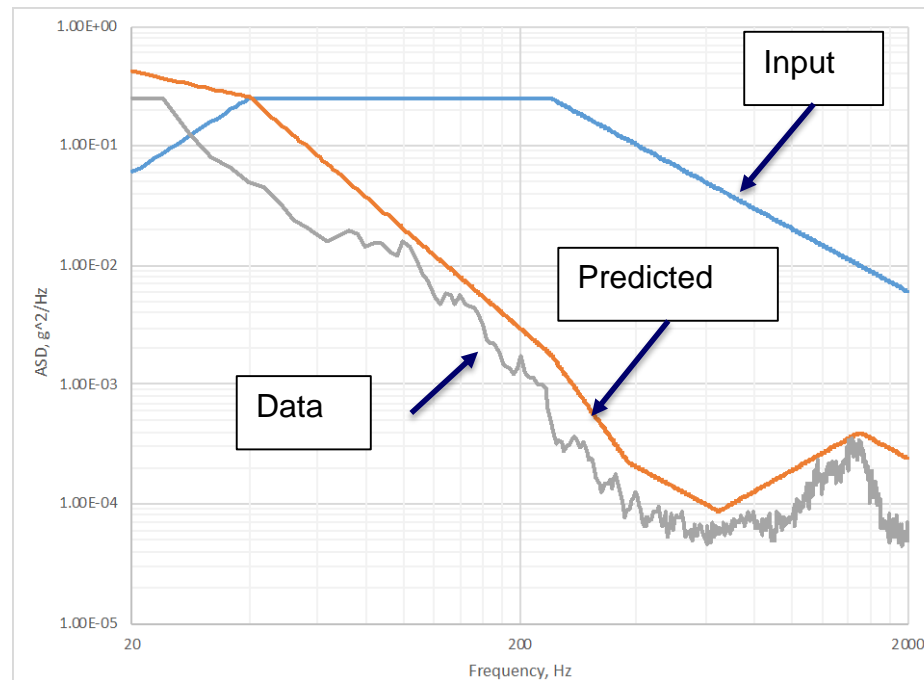


Test Setup



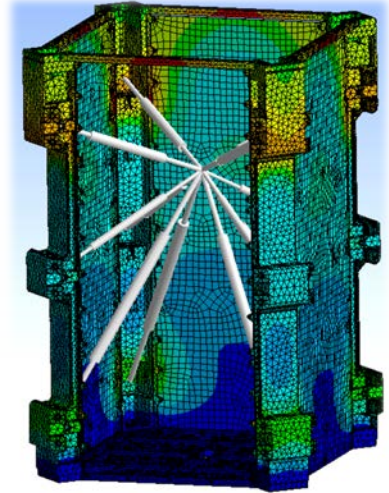
12U Payload Transfer Function

- Analyzing data sets for the 12U testing, a transfer function was developed which can be used to estimate payload environments for a variety of launch vehicle inputs
 - To leverage this capability, simply multiply the launch vehicle input by the transfer function to obtain the estimated payload environment
 - Enables rapid evaluation of environment, no need for complex analytical models.
- Low frequency amplification is seen as a result of the isolators. Attenuation begins at ~40Hz and reduces vibe inputs by a factor of 10-100x starting at 100Hz

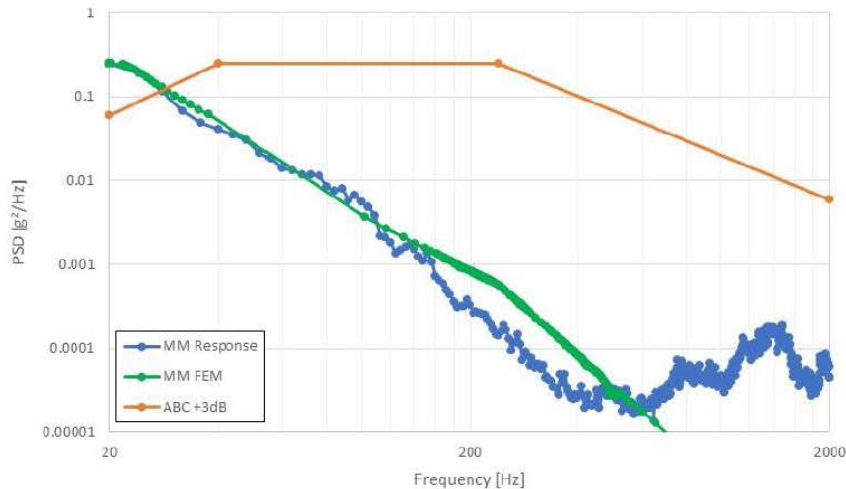


12U Finite Element Modeling

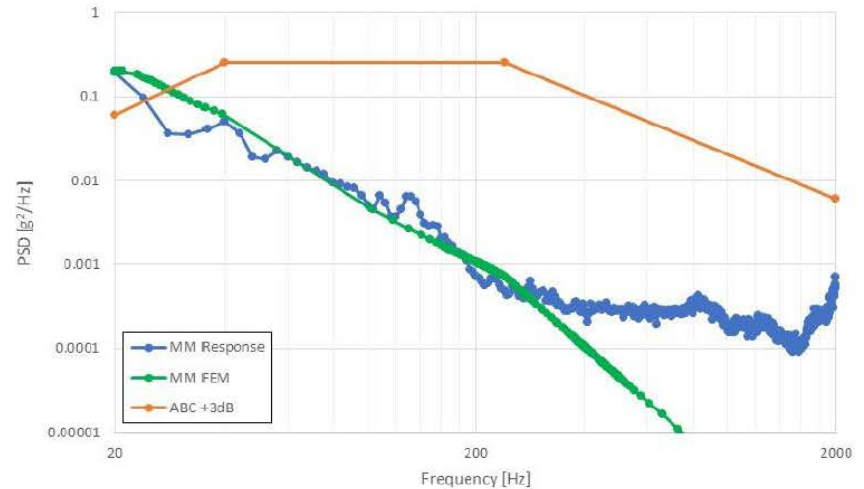
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Config 1, 25kg, ABC MPE +3dB, X

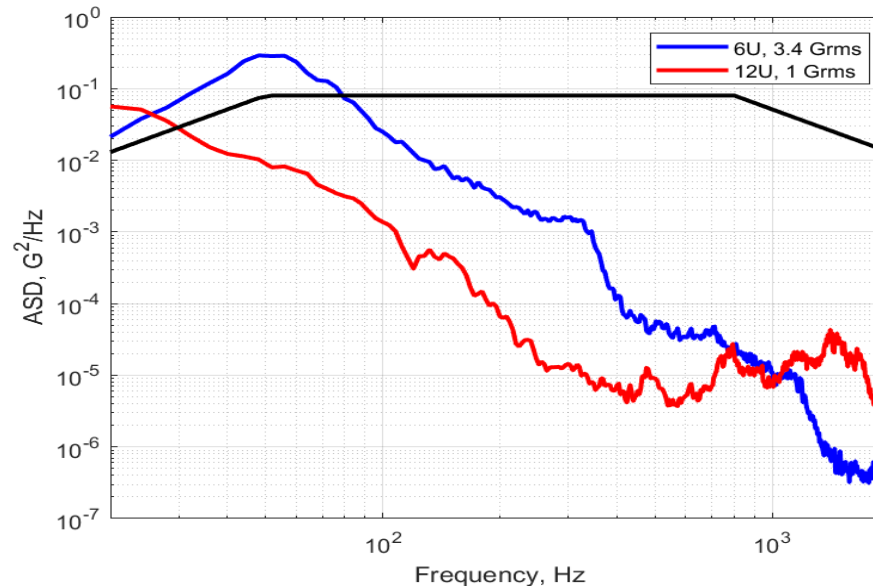


Config 1, 25kg, ABC MPE +3dB, Z



Conclusion and What's Next

- Internal isolation can be successfully implemented in multiple ways
 - 6U – modified rail type dispenser, constrained layer of damping material
 - 12U – built around bushing isolation system (dramatically improved results)
- Two methods for predicting loads exist
 - Compiling known test data to synthesize enveloping transfer functions
 - High fidelity FEMs to generate accurate response for a CubeSat
- Lower CubeSat loads, lower mass dispenser
- Dispenser is hard-mounted, less mass for coupled loads analysis



X-Axis Comparison of 6U to 12U Response